



Calhoun: The NPS Institutional Archive
DSpace Repository

Theses and Dissertations

1. Thesis and Dissertation Collection, all items

1984

An investigation into the control limitations of
a bank to turn missile in the terminal homing phase.

Anderson, Barton P.

Monterey, California. Naval Postgraduate School

<http://hdl.handle.net/10945/19403>

Downloaded from NPS Archive: Calhoun



Calhoun is the Naval Postgraduate School's public access digital repository for research materials and institutional publications created by the NPS community. Calhoun is named for Professor of Mathematics Guy K. Calhoun, NPS's first appointed -- and published -- scholarly author.

Dudley Knox Library / Naval Postgraduate School
411 Dyer Road / 1 University Circle
Monterey, California USA 93943

<http://www.nps.edu/library>

WILEY KNOX LIBRARY
NAVAL POSTGRADUATE SCHOOL
MONTEREY, CALIFORNIA 93943

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

AN INVESTIGATION INTO THE CONTROL
LIMITATIONS OF A BANK TO TURN MISSILE
IN THE TERMINAL HOMING PHASE

by

Barton P. Anderson

September 1984

Thesis Advisor:

M. D. Hewett

Approved for public release, distribution unlimited

T221691

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) An Investigation Into The Control Limitations of a Bank to Turn Missile in the Terminal Homing Phase		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis September 1984
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) 'Barton Paul Anderson		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		12. REPORT DATE September 1984
		13. NUMBER OF PAGES 205
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report)
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release, distribution unlimited		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Cruise Missile Bank-to-turn homing Proportional Navigation Guidance and Control		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The purpose of this thesis was to examine guidance and control deficiencies in a bank to turn (BTT) cruise missile with limited roll authority in the terminal homing phase of its mission. A six degree of freedom simulation of a typical BTT missile was translated into FORTRAN H from the Continuous System Modelling Program (CSMP) simulation language and run on the IBM System 370 computer. Tests were conducted with the revised		

simulation program to examine the effects of electronic countermeasures (ECM) blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. In addition to the standard attack profile involving a popout attack, several other attack profiles were tested including skid-to-turn (STT) control laws and a ballistic trajectory. Miss distances varied from 3.7 feet without ECM or glint to 85 feet with ECM operating. Susceptibility of the missile to ECM blinking varied with the blinking frequency. The largest miss distances occurred with ECM frequencies below 0.2 Hz and near 6.0 Hz. Analysis of the data showed that errors at the low frequencies were primarily caused by the bank command loop of the autopilot. Those at the higher frequency were due to the roll rate command loop. Variation of the geometry of the missile's flight profile had no significant impact upon missile accuracy except that, without a popup maneuver, the roll rate channel demonstrated a marked decrease in effectiveness. Variation of the autopilot gain in the roll rate control loop changed the frequency at which degradation occurred but actually increased its effects. Skid to turn control laws were tested however the missile was unable to produce the necessary sideforce needed to track a passive target and produced undesirable coupling in the flight controls. An attempt to use the altitude command channel to fly a ballistic profile was unsuccessful due to instabilities created in the control system. It is recommended that a popup maneuver be included in the terminal guidance of a BTT cruise missile and that further tests be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a BTT missile.

Approved for public release; distribution unlimited.

An Investigation into the Control
Limitations of a Bank to Turn Missile
in the Terminal Homing Phase

by

Earton P. Anderson
Commander, United States Navy
B.S., Wheaton College, 1970

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the

NAVAI POSTGRADUATE SCHOOL
September 1984

DU
NA
MC

ABSTRACT

The purpose of this thesis was to examine guidance and control deficiencies in a bank to turn (BTT) cruise missile with limited roll authority in the terminal homing phase of its mission. A six degree of freedom simulation of a typical BTT missile was translated into FORTRAN H from the Continuous System Modelling Program (CSMP) simulation language and run on the IBM System 370 computer. Tests were conducted with the revised simulation program to examine the effects of electronic countermeasures (ECM) blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. In addition to the standard attack profile involving a popout attack, several other attack profiles were tested including skid-to-turn (STT) control laws and a ballistic trajectory. Miss distances varied from 3.7 feet without ECM or glint to 85 feet with ECM operating. Susceptibility of the missile to ECM blinking varied with the blinking frequency. The largest miss distances occurred with ECM frequencies below 0.2 Hz and near 6.0 Hz. Analysis of the data showed that errors at the low frequencies were primarily caused by the bank command loop of the autopilot. Those at the higher frequency were due to the roll rate command loop. Variation of the geometry of the missile's flight profile had no significant impact upon missile accuracy except that, without a popup maneuver, the roll rate channel demonstrated a marked decrease in effectiveness. Variation of the autopilot gain in the roll rate control loop changed the frequency at which degradation occurred but actually increased its effects. Skid to turn control laws were tested

however the missile was unable to produce the necessary sideforce needed to track a passive target and produced undesirable coupling in the flight controls. An attempt to use the altitude command channel to fly a ballistic profile was unsuccessful due to instabilities created in the control system. It is recommended that a popup maneuver be included in the terminal guidance of a BTT cruise missile and that further tests be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a BTT missile.

TABLE OF CONTENTS

I.	INTRODUCTION	13
A.	BACKGROUND	13
B.	STATEMENT OF THE PROBLEM	13
C.	MISSION SCENARIO	14
1.	Control Configuration	14
2.	Target	14
3.	ECM Simulation	15
4.	Attack Profiles	15
D.	EXISTING WORK	15
E.	SCOPE OF TESTS	16
II.	PROGRAM DESCRIPTION	18
A.	INTEGRATION OF THE EQUATIONS OF MOTION	18
B.	PROGRAM NOMENCLATURE	18
C.	AXIS SYSTEM	18
D.	PROGRAM ARCHITECTURE	19
1.	Executive Program	19
2.	Subroutine INIT	19
3.	Subroutine MISSION	19
4.	Subroutine APILOT	20
5.	Subroutine AERO	21
6.	Subroutine TGTNAV	21
7.	Subroutine PREPAR	21
8.	Subroutine OUTPUT	22
III.	BASLINE ATTACK CONFIGURATION	23
A.	AUTOPILOT ROLL RATE COMMAND LOOP ADJUSTMENT	23
B.	BASLINE PROGRAM	24

IV.	FREQUENCY SCAN TESTS	25
A.	ERROR FUNCTIONS	25
B.	ECM PHASING	26
C.	BASELINE TEST RESULTS	26
1.	ECM Frequency Scans	26
2.	Effects of Glint	27
D.	ALTERNATE CONFIGURATION FREQUENCY SCAN RESULTS	28
1.	Mission Profile	28
2.	Frequency Scan Results	29
3.	Skid To Turn Guidance Results	32
4.	Ballistic Trajectory	33
V.	CONCLUSIONS	34
A.	BASELINE CONFIGURATION TESTS	34
B.	ALTERNATE ATTACK PROFILE CONFIGURATIONS	34
C.	SKID TO TURN CONTROL	36
D.	BALLISTIC ATTACK PROFILE	36
VI.	RECOMMENDATIONS	37
APPENDIX A:	FIGURES	38
APPENDIX B:	COMPUTER DATA OUTPUT	123
APPENDIX C:	PROGRAM NOMENCLATURE	142
APPENDIX D:	COMPUTER PROGRAM LISTING	145
APPENDIX E:	SUBROUTINE MISSN1 LISTING	195
APPENDIX F:	SUBROUTINE MISSN2 LISTING	200
	LIST OF REFERENCES	204
	INITIAL DISTRIBUTION LIST	205

LIST OF TABLES

I.	Missile Attack Profile Test Configurations	17
II.	Simulation Variables Held Constant	17
III.	Error Function Variables	25
IV.	Maximum Miss Distances	30
V.	Autopilot Errors	31

LIST OF FIGURES

A.1	Load Factor Commands	33
A.2	Data Array LFT1	39
A.3	Data Array LFT2	40
A.4	Data Array DRG1	41
A.5	Data Array DRG2	42
A.6	Data Array DRG3	43
A.7	Data Array DRG4	44
A.8	Data Array PTCH1	45
A.9	Data Array PTCH2	46
A.10	Data Array SID1	47
A.11	Data Array SID2	48
A.12	Data Array SID3	49
A.13	Data Array DFEC1	50
A.14	Data Array DREC2	51
A.15	Data Array DREC3	52
A.16	Data Array ITRL1	53
A.17	Data Array ITRL2	54
A.18	Data Array ITRL3	55
A.19	CSMP Data (Roll Rate) - KROLLR = 0.1	56
A.20	CSMP Data (Controls) - KROLLR = 0.1	57
A.21	CSMP Data (Roll Rate) - KROLLR = 0.5	58
A.22	CSMP Data (Controls) - Krollr = 0.5	59
A.23	Baseline - nc ECM or GLINT - Load Factor	60
A.24	Baseline - nc ECM or GLINT - Roll Rate	61
A.25	Baseline - nc ECM or GLINT - Bank	62
A.26	Baseline - no ECM or GLINT - Controls	63
A.27	Baseline - no ECM or GLINT - Altitude	64
A.28	Baseline - nc ECM or GLINT - Geo Plot	65

A.29	Baseline with GLINT & ECM - Load Factor	66
A.30	Baseline with GLINT & ECM - Bank	67
A.31	Baseline with GLINT & ECM - Roll Rate	68
A.32	Baseline with GLINT & ECM - Controls	69
A.33	Baseline with GLINT & ECM - ECM & GLINT	70
A.34	Baseline with GLINT & ECM - Altitude	71
A.35	Baseline with GLINT & ECM - Geo Plot	72
A.36	Mean Miss Distances - Baseline	73
A.37	Mean Miss Distances - Configuration II	74
A.38	Mean Miss Distances - Configuration III	75
A.39	Mean Miss Distances - Configuration IV	76
A.40	Autopilot Errors - Baseline	77
A.41	Autopilot Errors - Configuration II	78
A.42	Autopilot Errors - Configuration III	79
A.43	Autopilot Errors - Configuration IV	80
A.44	Tracking Errors - Baseline	81
A.45	Tracking Errors - Configuration II	82
A.46	Tracking Errors - Configuration III	83
A.47	Tracking Errors - Configuration IV	84
A.48	Baseline/ECM Freq = 0.0 Hz - Bank	85
A.49	Baseline/ECM Freq = 0.4 Hz - Bank	86
A.50	Baseline/ECM Freq = 6.0 Hz - Bank	87
A.51	Baseline/ECM Freq = 0.0 Hz - Roll Rate	88
A.52	Baseline/ECM Freq = 0.4 Hz - Roll Rate	89
A.53	Baseline/ECM Freq = 6.0 Hz - Roll Rate	90
A.54	Baseline with GLINT only - Load Factor	91
A.55	Baseline with GLINT only - Bank	92
A.56	Baseline with GLINT only - Roll Rate	93
A.57	Baseline with GLINT only - Controls	94
A.58	Conf. II Mission Set - Load Factor	95
A.59	Conf. II Mission Set - Bank	96
A.60	Conf. II Mission Set - Roll Rate	97
A.61	Conf. II Mission Set - Controls	98

A.62	Conf. II Mission Set - Altitude	99
A.63	Conf. II Mission Set - Geo Plot	100
A.64	Conf. III Mission Set - Load Factor	101
A.65	Conf. III Mission Set - Bank	102
A.66	Conf. III Mission Set - Roll Rate	103
A.67	Conf. III Mission Set - Controls	104
A.68	Conf. III Mission Set - Altitude	105
A.69	Conf. III Mission Set - Geo Plot	106
A.70	Conf. IV Mission Set - Load Factor	107
A.71	Conf. IV Mission Set - Bank	108
A.72	Conf. IV Mission Set - Roll Rate	109
A.73	Conf. IV Mission Set - Controls	110
A.74	Conf. IV Mission Set - Altitude	111
A.75	Conf. IV Mission Set - Geo Plot	112
A.76	Conf. V Mission Set - Load Factor	113
A.77	Conf. V Mission Set - Bank	114
A.78	Conf. V Mission Set - Roll Rate	115
A.79	Conf. V Mission Set - Controls	116
A.80	Conf. V Mission Set - Altitude	117
A.81	Conf. V Mission Set - Geo Plot	118
A.82	Conf. VI Mission Set - Load Factor	119
A.83	Conf. VI Mission Set - Bank	120
A.84	Conf. VI Mission Set - Roll Rate	121
A.85	Conf. VI Mission Set - Controls	122

ACKNOWLEDGEMENT

The author wishes to acknowledge Dr. Marle D. Hewett, PhD, whose encouragement and advice contributed greatly to this project.

I. INTRODUCTION

A. BACKGROUND

Bank-To-Turn (BTT) control is utilized extensively on missiles which must cruise for long ranges within the atmosphere. These missiles utilize a primary lifting surface (wing) and smaller controlling surfaces as on a conventional airplane. This method has two primary advantages. First, the wing provides lift to support the missile's weight at a relatively high efficiency thereby permitting longer ranges for a given size engine and fuel load. Second, the lift vector can be positioned by banking the missile to provide large lateral accelerations resulting in excellent turn performance. Certain BTT cruise missile configurations, however, use differential tail for roll control as opposed to ailerons and suffer from poor roll rate and acceleration performance. It is the investigation into the control limitations of a BTT cruise missile configured this way in the terminal homing phase which is the subject of this thesis.

B. STATEMENT OF THE PROBLEM

In order to provide compact storage of a BTT missile, the main wings are usually folded back and designed to snap into position as the missile emerges from its cannister at launch. Because of this feature, it is generally not feasible to install roll control devices at the extremities of the wings. Roll control is normally provided by differential actuation of the tail fins of the missile. Because of their short moment arm and small area and because the main wing has a relatively large degree of roll damping, BTT missiles are limited in their ability to roll rapidly.

Because of the need to bank the missile in order to align its lift vector in the desired direction it has been suggested that the requirement for rapid roll maneuvering in the terminal phase of flight would limit the accuracy of the missile. In addition, natural fluctuations in the position of the radar target, known as glint, and artificial fluctuations due to the presence of electronic countermeasures (ECM) might further degrade the performance of a ETT missile.

C. MISSION SCENARIO

1. Control Configuration

The missile simulated in this thesis is a hypothetical bank to turn cruise missile with limited roll control authority. Its design incorporates characteristics typical of many similar designs. The missile is equipped with a standard rudder for yaw control and stabilators for both roll and pitch control. Inner loop closures for stabilization and command are included in the simulation. Command loop closures consist of normal acceleration, bank angle, and lateral acceleration. The lateral acceleration command system can be used as a turn coordinator in the bank-to-turn mode (normal) mode or as a lateral load factor (NY) command system in a skid-to-turn mode. Outer loop closures are provided for altitude and flight path angle. The autopilot control loop design is presented in detail in [Ref. 1].

2. Target

The target is assumed to be a surface combatant ship located initially 24,000 feet due North from the missile and moving East at a constant speed of 20 knots. It is assumed that the missile seeker tracks an aim point perfectly. The aim point is located nominally 10 feet above the ship's

waterline and amidships. This aim point continually shifts as a function of ECM blinking and a random glint simulation.

3. ECM Simulation

The ECM blinker simulation shifts the radar target seen by the missile's seeker forward and aft from the true target aim point by ± 75 feet along the ships longitudinal axis at a specified frequency. The aim point is simultaneously shifted vertically ± 10 feet at the same frequency.

4. Attack Profiles

The attack profile used as a baseline for this simulation began at 50 feet of altitude at a speed of Mach 0.75. The missile tracked toward the target using proportional navigation in azimuth and altitude hold at 50 feet. At a range of 18000 feet the missile rolled to 60 degrees of bank and turned away from the target to the right until the target line of sight was offset by 10 degrees. When the offset was reached, the missile climbed to an altitude of approximately 250 feet and then dove toward the target using proportional navigation in both azimuth and elevation. This mission profile is often referred to as a popout attack.

Variations of this mission included eliminating the 10 degree offset turn and/or the climb to altitude and substituting skid-to-turn control laws for some phase of the mission. A ballistic altitude profile was also attempted.

D. EXISTING WORK

In order to examine the existence of such problems and to test several proposed solutions, a six degree of freedom simulation of a typical BTT cruise missile was produced by LCDR Kent Watterson and published in [Ref. 1]. This simulation was produced using the IBM Continuous System Modelling

Program (CSMP III) simulation language. A detailed description of this language and its constructions is presented in [Ref. 2] and [Ref. 3]. The simulation included dynamics, autopilot, guidance and mission profiles. It did not represent any specific missile but, rather, included characteristics typical of missiles configured in this way. In order to overcome limitations imposed upon the simulation program by the available computer installation, this CSMP program was rewritten in extended FORTRAN H. This allowed greater flexibility and full utilization of the DISSPLA graphics programming package available at NPS. A complete copy of the program listing is presented in Appendix D.

F. SCOPE OF TESTS

The tests conducted with the revised simulation program were limited to examining the effects of ECM blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. Alternate attack profiles using modified flight geometry and, in some cases, skid-to-turn control laws were also tested. A listing of the different flight profiles examined is presented in table I.

For all flight tests of the missile, certain parameters were held constant. A list of these values is presented in table II.

TABLE I
Missile Attack Profile Test Configurations

	OFFSET TURN	POP-UP	ROLL RATE	TURN
BASELINE	X	X	0.5	BTT
II		X	0.5	BTT
III			0.5	BTT
IV		X	0.1	BTT
V		X	0.5	STT
VI		X	0.5	*

* 90 degree bank on ballistic terminal trajectory

TABLE II
Simulation Variables Held Constant

Variable Name	Value
*****	*****
Radar Burn-Through Range	500 ft
ECM Blinker Shifts:	
Longitudinal	± 75 ft
Lateral	± 00 ft
Vertical	± 10 ft
Baseline guidance scheme:	
Offset	10 deg
Popup Altitude	100 ft
Popup Range	18000 ft
Roll rate limit	75 dps
*****	*****

II. PROGRAM DESCRIPTION

A. INTEGRATION OF THE EQUATIONS OF MOTION

This simulation uses the linear, six degree of freedom equations of flight developed by Roskam in [Ref. 5:vol 1] and modified by Hewett in [Ref. 4]. The CSMP program developed by Watterson [Ref. 1] used a variable step Runge-Kutta integration method. The FORTRAN translation program uses a

$$\text{INTEGRAL}(\text{YDOT DT}) = Y + (\text{YDOT}) * \text{DT} \quad (\text{eqn 2.1})$$

simple Eulerian integration which is given by equation 2.1. The incremental time element, DT, is fixed at 0.01 seconds and the integration period lasts for less than 30 seconds.

B. PROGRAM NOMENCLATURE

A detailed description of the nomenclature used throughout the simulation program is presented in Appendix C. The variable names used in the FORTRAN translation are, with few exceptions, the same as those used in the CSMP simulation.

C. AXIS SYSTEM

The simulation uses a right handed earth reference frame where the x-axis points North, the y-axis points East and the z-axis points down. However, altitude and vertical velocity are always given as positive upwards (i.e. ALTITUDE = -Z). For plotting the geographical track in the output routines, the axes are transformed so that the X,Y, and Z axes point East, North and upward, respectively.

D. PROGRAM ARCHITECTURE

The FORTFAN simulation program consists of an executive program which calls seven major subroutines which are briefly described as follows.

1. Executive Program

The main calling program is short and handles only three tasks. It increments the TIME variable for each integration cycle. It calls the output data storage routine, PREPAR, at the specified output interval and it controls the execution of multiple flights within a single program run changing one or more key variables between the runs.

2. Subroutine INIT

This subroutine contains a small section of executable statements which resets variables to their initial value when more than one flight is flown during a program run. Included with this subroutine is the BLOCK DATA subroutine which must be used to initialize all variables in named common areas. The majority of the BLOCK DATA subprogram is taken up with arrays listed in table form which contain the aerodynamic coefficient data for the missile. Static coefficients which are functions of one variable are shown in figures A.2 through A.9 Static coefficients which are functions of two parameters are presented in figures A.10 through A.13 Dynamic coefficients are assumed to be constant and are not presented graphically.

3. Subroutine MISSN

This subroutine dictates the mission profile. It is divided into sections which activate in sequence as the mission progresses. Each section takes the flight dynamics data for the missile, compares it with the target

acquisition data (generated in subroutine TGTNAV) and outputs vertical and horizontal acceleration commands in the geographic earth reference frame. These in turn are translated into commanded bank angle and normal load factor for the missile according to equations 2.2 and 2.3. A diagram

$$PHIC = ARCTAN (AYC/AZC) \quad (\text{eqn 2.2})$$

$$NZC = AZC \cos (PHI) + AYC \sin (PHI) \quad (\text{eqn 2.3})$$

of these vectors is given in figure A.1. Different terminal attack profiles are implemented using variations of this subroutine, MISSN1 and MISSN2, which are presented in Appendices E and F.

4. Subroutine APILOT

This subroutine takes the commanded normal load factor and bank angle and applies them to the missile autopilot system. A detailed discription of the design of the missile's autopilct is presented in reference [Ref. 1]. The output of the control system is delivered in terms of conventional airplane elevator, aileron and rudder control positions. These are mixed to obtain the commanded missile fin positions. The control limits of ± 15 degrees are applied to the fins and these controls are then unmixed to obtain the limited conventicnal control positions. The dynamics of the servc actuators that move the tail surfaces are modelled as a first order real pole. Although CSMP-III provides macros that perform the simulation of many types of transfer functions within the control system only the first order real pole transfer function was necessary for this program. It is modelled in the FORTRAN translation using subroutine REALPL, presented in the program listing in Appendix C.

5. Subroutine AEFO

Subroutine AEFO uses two table lookup routines to retrieve the aerodynamic coefficients from the data presented in figures A.2 through A.18. Linear interpolations are used to obtain values between given parameters. Error messages are printed when the input parameters are outside the bounds of the data in the lookup table and these are suppressed after about 5 successive integration cycles. AEFO completes the buildup process, uses these data to compute the forces and moments on the aircraft and then integrates the equations of motion to update all of the aircraft's flight parameters and position information.

6. Subroutine TGTNAV

The TGTNAV subroutine navigates the target vessel on a course of East at a steady speed of 20 knots. It shifts the position of the radar target relative to its real position according to the ECM and GLINT parameters. The GLINT offset is produced by multiplying the GLINT shift in each axis by a random number between -1 and 1. The GLINT offset is calculated every output interval rather than 100 times per second. The ECM offset is switched according to the sign of a sine wave which runs at the ECM blinking frequency, FREQ. These offsets are then added to the actual target position to produce the radar target position. Line of sight angles and rates are calculated from this information with the assumption that the seeker has perfect pointing capability.

7. Subroutine PREPAR

At intervals specified by the output counter, this subroutine is called and stores up to 20 variables in a large array call PTS. The output interval used for all tests

was 0.20 sec. The PTS array is passed to the output routines when the simulation run is completed. This subroutine also converts output variables from radian to degree format and, in the final attack phase, calculates four error functions. These error functions are time averaged differences between commanded variables (e.g. PANK or ROLL RATE) and their actual counterparts. These are later used to analyse the performance of the control system under various conditions.

8. Subroutine OUTPUT

OUTPUT produces 3 forms of output information. The primary data output lists the value of MISDST (the distance at which the missile passed the target at its closest approach), the value of the error functions at the end of the mission, and the ranges of all the variables stored. These data are also printed to another file followed by the full contents of the PTS array in tabular form. This gives a numerical history of all the output variables from the start to the finish of the mission. (Normally, to save disk space, this file was routed to a dummy variable. It was needed only when detailed data histories of a portion of the mission were required.)

OUTPUT also calls the necessary DISSPLA routines to print graphs of the output variables. The independent variable in six graphs is TIME. In the seventh graph the positions of the missile and the target ship are plotted in three dimensional space for each output interval. Each of the graphs in this subroutine are controlled by the setting of 7 flags in the first column of the data statement at the beginning of the routine (0 to pass over and 1 to plot).

III. BASELINE ATTACK CONFIGURATION

A. AUTOPILCT ROLL RATE COMMAND LOOP ADJUSTMENT

Initial testing of the simulation was conducted on the CSMP version of the program. The frequency of the ECM blinker was varied from 0.2 Hz to a maximum of 2.0 Hz and the roll performance of the missile was graphed. Figure A.19 shows the commanded roll rate and actual roll rate plotted against time for the duration of a thirty second flight straight toward the target at a constant altitude of 50 feet. The target's radar position was blinked at a rate of 0.4 Hz and roll rate command was limited to 75 degrees per sec. In the figure, the command oscillations increased in magnitude as the target range decreased and, after 24 seconds, the autopilot commanded the maximum rate with every shift of the target's apparent position. While the commanded roll rate remained at 75 degrees per second, the actual roll rate never exceeded 35 degrees per second. Figure A.20, which plots the fin positions as a function of time, shows that the fin servos never used more than 3 degrees (of the maximum 15) of travel in either direction. To remedy this problem, the missile autopilot roll rate command loop gain (KRCLET in the program) was increased from 0.1 to 0.5. The value of this gain had been set by Watterson [Ref. 1] using root locus based upon the perturbation equations of motion [Ref. 4] in steady state level flight. Figures A.21 and A.22 show the results of a subsequent run with the revised guidance loop. Steady state error in roll rate was significantly reduced and the full range of available flight controls (± 15 deg.) was used. This difference in the autopilot was incorporated into the baseline program and remained throughout all subsequent tests.

E. BASELINE PROGRAM

In order to provide a baseline performance record against which to examine the effects of ECM and glint and/or alternate attack profiles on the accuracy of the missile and the performance of its control system, a standard, pop-out attack with an offset turn was selected and flown and is used as a standard for comparison. The parameters which apply to this baseline are listed in table II. Figures A.23 through A.28 are a complete record of the baseline program run without any ECM or glint offsets applied to the target. Figures A.29 through A.35 are a complete record of the baseline program run with the ECM blinker operating at 0.2 HZ and the glint feature operating. The complete tabular data output from this latter run is presented in Appendix B.

IV. FREQUENCY SCAN TESTS

A. ERROR FUNCTIONS

For testing the effects of glint and ECM at various blinking frequencies against the control system of the missile, a quantitative measure of the system's effectiveness was needed. Four error functions were developed for this purpose. The time weighted difference between the commanded value and the actual value of a variable was computed according to equation 4.1. This time weighted error was summed over all of the time intervals and divided by the

$$ERR = DT * ABS(COMMAND - VARIABLE) \quad (\text{eqn 4.1})$$

total time to produce the error function for the variable. The variables for which these functions were computed are

TABLE III
Error Function Variables

VARIABLE	COMMAND VARIABLE
*****	*****
1. BANK	BANK
2. ROLL RATE	ROLRT
3. AZIMUTH LOS RATE	0.0
4. ELEVATION LOS RATE	0.0
*****	*****

listed in Table III. In the terminal phase where proportional guidance is used in both the azimuth and elevation channels, the commanded azimuth and elevation angle rates are zero to produce a constant bearing intercept.

B. ECM PHASING

At low frequency blinking rates, the phase of the ECM blinker at the start of the mission had a very large effect on the miss distance. To minimize the distortion of the data due to this effect, a phase variable was added to the ECM generator to change the phase of the blinker at the start of each run. Four runs were conducted at each frequency using values of 0.0, $\pi/2$, π , $(3/2)\pi$ for the phase variable. The data for each frequency were averaged to get mean values for the miss distance and each error function.

C. BASELINE TEST RESULTS

1. ECM Frequency Scans

Four simulated flights were conducted at each frequency from 0.0 to 30 Hz. Glint was disabled for the course of these tests. The attack profile flown was the baseline popout attack mission. A graph of the mean value of the miss distance (MISDST) versus frequency is presented in figure A.36. The data show that maximum miss distance occurs in the very low frequency range of the order of 0.2 Hz and again to a lesser degree in the vicinity of 6 Hz. Figures A.40 and A.44 are plots of the error function means against frequency for the autopilot command errors and the tracking errors respectively. These data show that the bank angle command loop is susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop is primarily responsible for the errors that occur at the higher frequencies in the range of 5 to 10 Hz. Figure A.44 also demonstrates that the time averaged tracking errors follow the same basic pattern.

Figures A.48 through A.53 demonstrate these effects in flight. Figures A.48 and A.51 show the bank angle and

roll rate performance of the baseline missile without ECM. Both variables track closely to their commanded values with the exception of a small, steady state error in the rate channel which is most evident at large commanded rates. Figures A.49 and A.50 show the effects of ECM at 0.4 and 6.0 Hz upon the bank channel. In figure A.49 significant errors exist in bank as the system cannot keep up with the large, sudden changes in commanded bank caused by the ECM shift of the target. The bracket in figure A.49 is drawn between two corresponding points to emphasize the large lag present in the channel. Roll rate tracks close to its commanded level at this frequency.

At 6.0 Hz, figures A.52 and A.53 show the opposite effect. In figure A.53 the bracket emphasizes the large lag that exists in the aircraft roll response to the rapid changes in rate command. The bank command loop at this frequency has effectively filtered out most of the high frequency input.

The results of the frequency scan tests showed that the baseline BTT cruise missile simulated by the program was more susceptible to ECM frequencies in the vicinity of 0.2 and 6.0 Hz due to the excitation of the bank and roll rate command loops respectively. If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

2. Effects of Glint

In order to isolate the effects of glint, the baseline configuration was flown without ECM or glint and again with glint only. Figure A.33 shows a trace of the random glint

displacement applied to the target's position as a function of time. Figures A.23 through A.28, which trace the missile's load factor, bank angle, roll rate and flight controls without glint, may be compared with figures A.54 through A.57 which show the same traces for the mission with glint.

The miss distance recorded without glint and an ECM phase of 0 was 3.7 feet. The distance measured with glint was 9.4 feet. Although these distances are very small compared with the miss distances achieved with ECM, the degradation induced by glint was large (154 percent) compared to the best obtainable value. Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Since the miss distances without ECM and glint were very small compared to those obtained with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

D. ALTERNATE CONFIGURATION FREQUENCY SCAN RESULTS

1. Mission Profile

Similar frequency scan profiles were flown using the MISSN1 (Appendix E) subroutine to generate the guidance commands for configurations II, III and IV. These attack profiles committed the offset turn and proceeded straight toward the target using proportional navigation in azimuth from start to finish. The popup maneuver was commenced at 15000 feet from the target. Of ranges from 20,000 to 5,000

feet which were tested, 15,000 feet produced the most consistent hits with a 200 foot popup altitude command. All subsequent tests of these missile attack configurations used 15,000 ft. popup range and a 200 ft. altitude command when the maneuver was performed.

An algorithm was added to the baseline proportional guidance scheme for the terminal phase which ensured that the missile rolled to place the nearest of the positive or negative Z-axis vectors on the direction commanded by the guidance system. This ensured that the missile would command negative load factor rather than trying to roll the missile upside down as it reached the apex of its climb. Azimuthal accelerations commanded by the guidance were still achieved by banking the missile except for configuration V.

A complete set of mission profile graphs for configurations II, III, and IV against a target with glint and ECM blinking at 0.2 Hz are presented in figures A.58 through A.75

2. Frequency Scan Results

a. Miss Distances

Each configuration was flown against the target four times per test frequency. The tests covered a range of blinker frequencies from 0.05 through 30.0 Hz. The mean miss distances recorded are graphically presented as a function of frequency in figures A.37 through A.39. The results obtained were very similar to those obtained from the baseline configuration. There were two areas of higher than normal errors, one at low frequency below 0.2 Hz and another at a higher frequency near 6.0 Hz. Table IV compares the miss distances for each of the configurations.

The maximum values that occurred for all configurations appeared at the same frequencies with one

TABLE IV
Maximum Miss Distances

CONFIGURATION	FREQ. RANGE (HZ)	LOCATION (HZ)	MAGNITUDE
BASLINE	0.20 - 20.0	≤ 0.20 6.00	≥ 45 22
II	0.05 - 21.0	≤ 0.05 6.00	≥ 75 17
III	0.10 - 30.0	≤ 0.10 5.50	≥ 75 17
IV	0.10 - 30.0	≤ 0.10 N/A	≥ 75 N/A

exception: changing the roll rate gain from 0.5 to 0.1 eliminated the maximum at the higher frequency. In addition, the magnitude of the errors did not differ significantly. (The baseline shows a smaller magnitude because the data do not extend below 0.2 Hz. while the other configurations were tested down to 0.1 and 0.05 Hz). Changing the attack geometry of the missile did not significantly alter its susceptibility to ECM jamming within the scope of these tests. Altering the gain of the roll rate command channel in the missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies. Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

b. Autopilot Errors

Figures A.40 through A.43 graphically present the error functions for both the bank angle and roll rate command loops within the autopilot. These functions are representative of the ability of the missile to follow the

commands given it by the autopilot (the higher the function, the poorer the performance). As with the baseline configuration these figures demonstrate that the bank angle loop contributed most to the errors at low frequency and the roll rate loop contributed most at the higher frequency. Table V

TABLE V
Autopilot Errors

CONFIGURATION	BANK ERROR		RATE ERROR	
	FREQ . (HZ)	MAGNI- TUDE	FREQ . (HZ)	MAGNI- TUDE
=====	=====	=====	=====	=====
BASLINE	0.4	0.22	7.0	0.19
II	0.6	0.17	8.0	0.18
III	0.5	0.18	8.0	0.27
IV	0.6	0.21	2.0	0.37

is a summary of these graphs.

Magnitude of the bank error function and the frequency at which it occurred were not significantly altered in any one of the tested configurations. Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but

increased the magnitude of the errors by more than 100 percent. This effect is reflected in the miss distance graphs (figures A.36 through A.39) in the disappearance of the distinct maximum at 6 HZ and a widening of the lower maximum (figure A.39). Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect.

c. Tracking System Errors

Errors in the tracking loops are charted in figures A.44 through A.47. These errors follow the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.

3. Skid To Turn Guidance Results

The MISSN1 subroutine was further modified to allow the lateral load factor command variable, NYC, to be set according to guidance commands rather than being kept at zero for turn coordination purposes. The commanded bank angle was set to zero in the terminal phase in order to examine the effectiveness of lateral G command. No changes to the basic dynamics of the autopilot were made. The missile was flown in this configuration against a passive target. Figures A.76 through A.81 present the full data set from this test. The missile splashed into the water 99 feet left and short of the target. Once the missile came within 5 seconds of impact, cross coupling between the rudder channel and normal load factor, roll rate and bank can be seen in the figures. Although the rudder commands were never saturated, neither could the lateral load factor control loop create enough sideforce to follow the ship's lateral drift to the right. The addition of ECM and/or glint would have

only worsened the performance of the missile in this configuration. No further tests of this configuration were conducted. The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

4. Ballistic Trajectory

Because the majority of the apparent target shift with ECM blinking occurs in the horizontal plane, an attempt was made to place the missile on a ballistic trajectory and then roll the aircraft to 90 degrees angle of bank until impact using the primary load factor to follow the ECM target and lateral load factor to maintain the ballistic trajectory. In order to fly the ballistic trajectory, the altitude hold system was driven by a commanded altitude slaved to a parabolic trajectory derived from the missile's vertical speed and range to the target according to equation

$$ALT = HMDOT * RANGE / V_H + (G/2) * (RANGE / V_T)^2 + 10 \quad (\text{eqn 4.2})$$

4.2. where HMDOT, V_H and V_T are the vertical, horizontal and total speeds of the missile. The controlling subroutine used for this mission was MISSN2 and is presented in Appendix F.

Figures A.82 through A.85 show that the addition of the dynamics of the altitude command loop made the missile's control system unstable. Oscillations to the limits occurred in normal load factor and in roll rate. Considerable cross coupling occurred between the lateral-directional and longitudinal dynamics of the missile. The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

V. CONCLUSIONS

The conclusions listed below were derived from analysis of the results of simulated flights conducted using the baseline popout attack profile configuration, three variations of the baseline attack, a skid-to-turn control configuration and a ballistic altitude trajectory.

A. BASELINE CONFIGURATION TESTS

At low frequency blinking rates, the phase of the ECM blinker had a very large effect on the miss distance.

The best obtainable performance for the baseline mission without ECM or glint was a miss distance of 3.7 feet. The addition of GLINT produced a miss distance of 9.7 feet, a degradation of 154 percent.

The bank angle command loop of the missile autopilot in the baseline configuration was especially susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop was primarily affected at the higher frequencies in the range of 5 to 10 Hz. The time averaged tracking errors also followed the same basic pattern.

If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

B. ALTERNATE ATTACK PROFILE CONFIGURATIONS

In terms of the average miss distances measured, changing the flight geometry of the missile did not signifi-

cantly alter its susceptibility to ECM jamming within the scope of these tests.

Altering the gain of the roll rate command channel in the baseline missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies.

Changing the geometry of the attack had no effect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the roll rate gain from 0.5 to 0.1 had no noticeable affect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but increased the magnitude of the errors by more than 100 percent. This effect was reflected in the miss distance data by the disappearance of the distinct maximum at 6 HZ and a widening of the lower maximum. Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect and, in this case enlarged it.

Errors in the azimuth and elevation tracking loops closely followed the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.

C. SKID TO TURN CONTROL

The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

D. BALLISTIC ATTACK PROFILE

The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

VI. RECOMMENDATIONS

Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

Since the elimination of a popup increased roll rate errors by 50 percent, a popup profile is recommended for the terminal phase of a BTT cruise missile. Further testing should be conducted to determine the effects of different popup profiles on the susceptibility of the roll rate command system to ECM blinking.

Since the miss distances without ECM and glint were very small compared to those with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

APPENDIX A
FIGURES

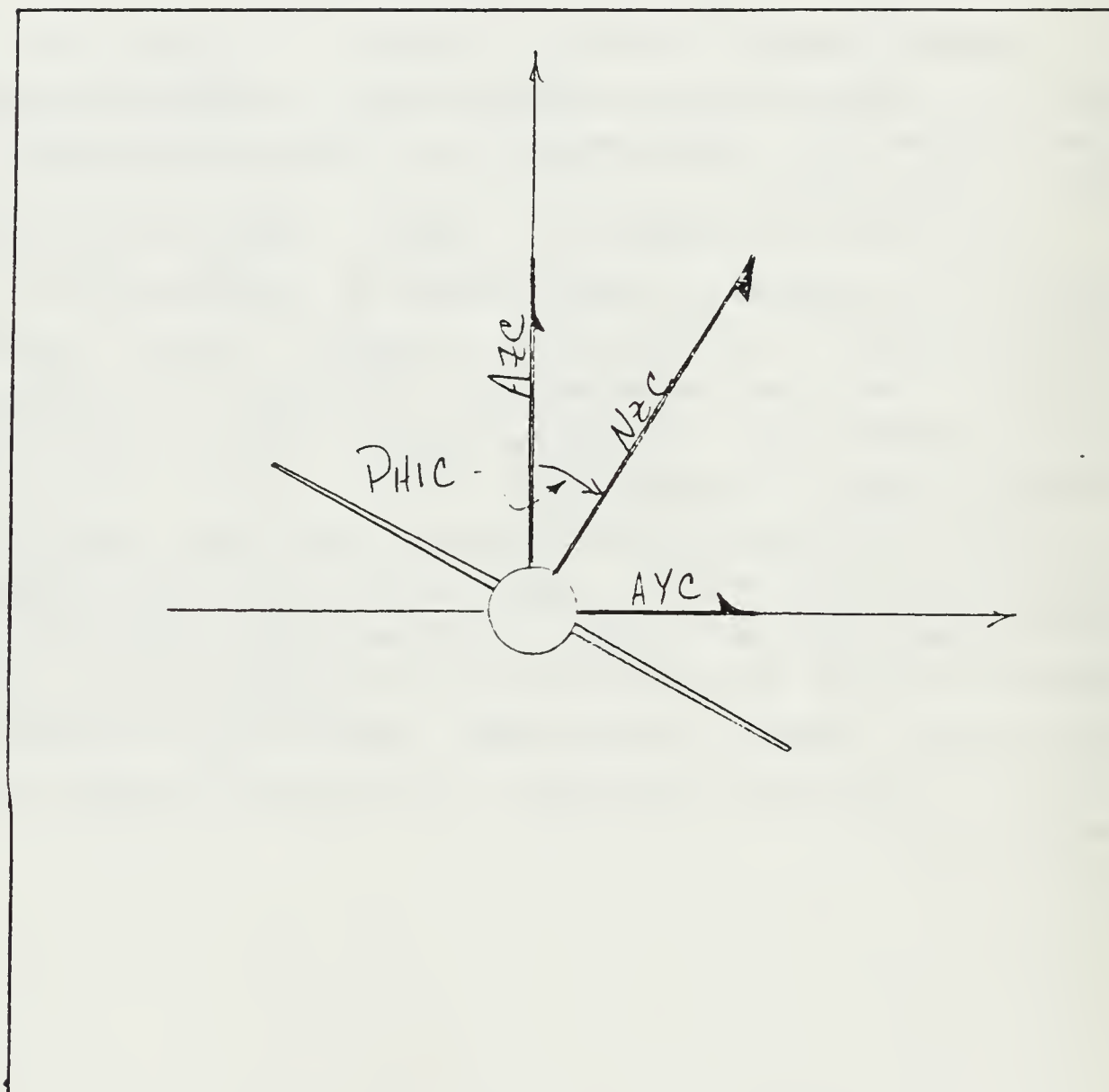


Figure A.1 Load Factor Commands.

STATIC AERODYNAMIC COEFFICIENTS

LIFT COEFFICIENT DATA

BASIC CL VS. AOA

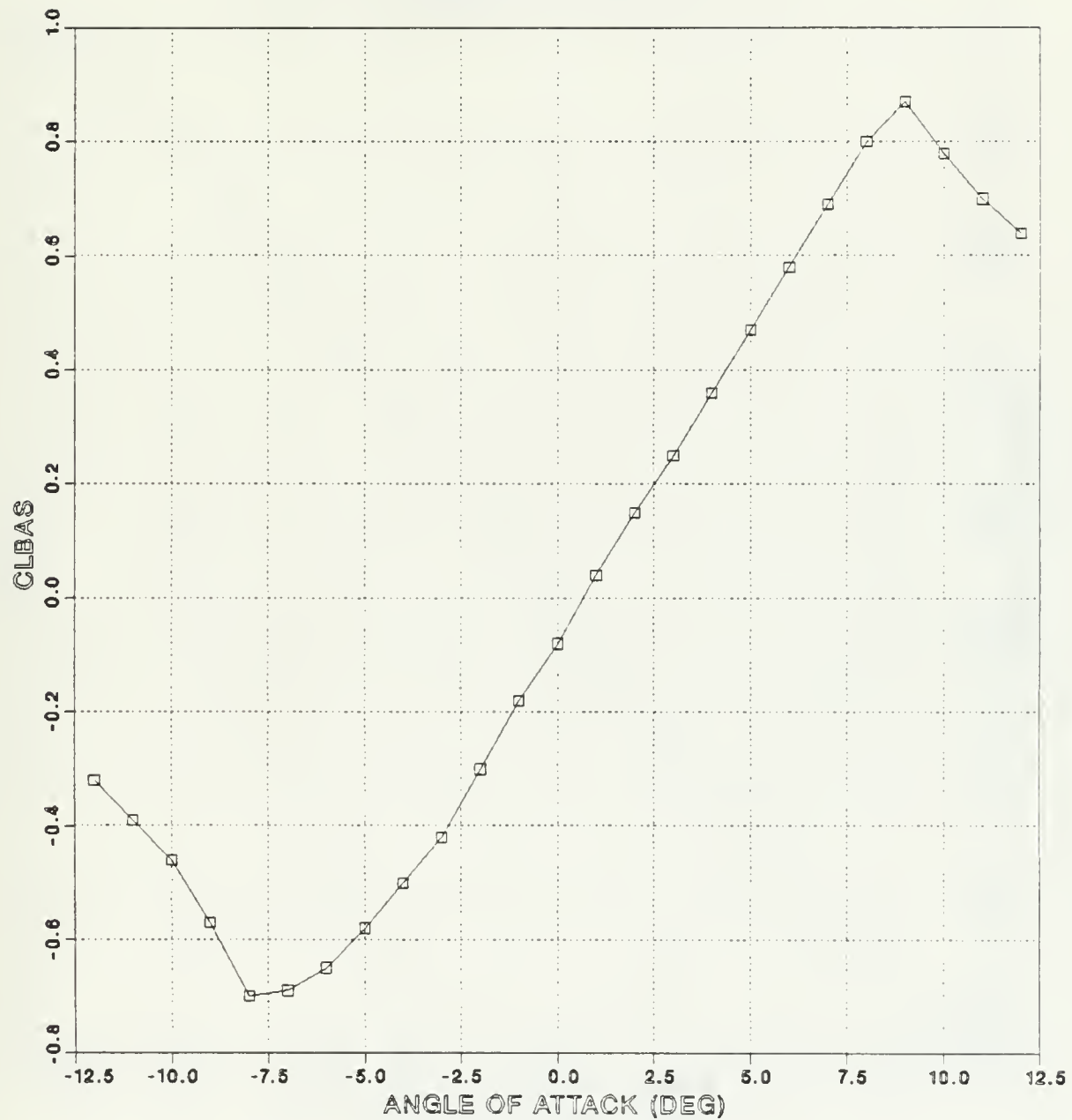


Figure A.2 Data Array LFT1.

STATIC AERODYNAMIC COEFFICIENTS

LIFT COEFFICIENT DATA

DELTA CL VS SYMMETRIC STABILATOR

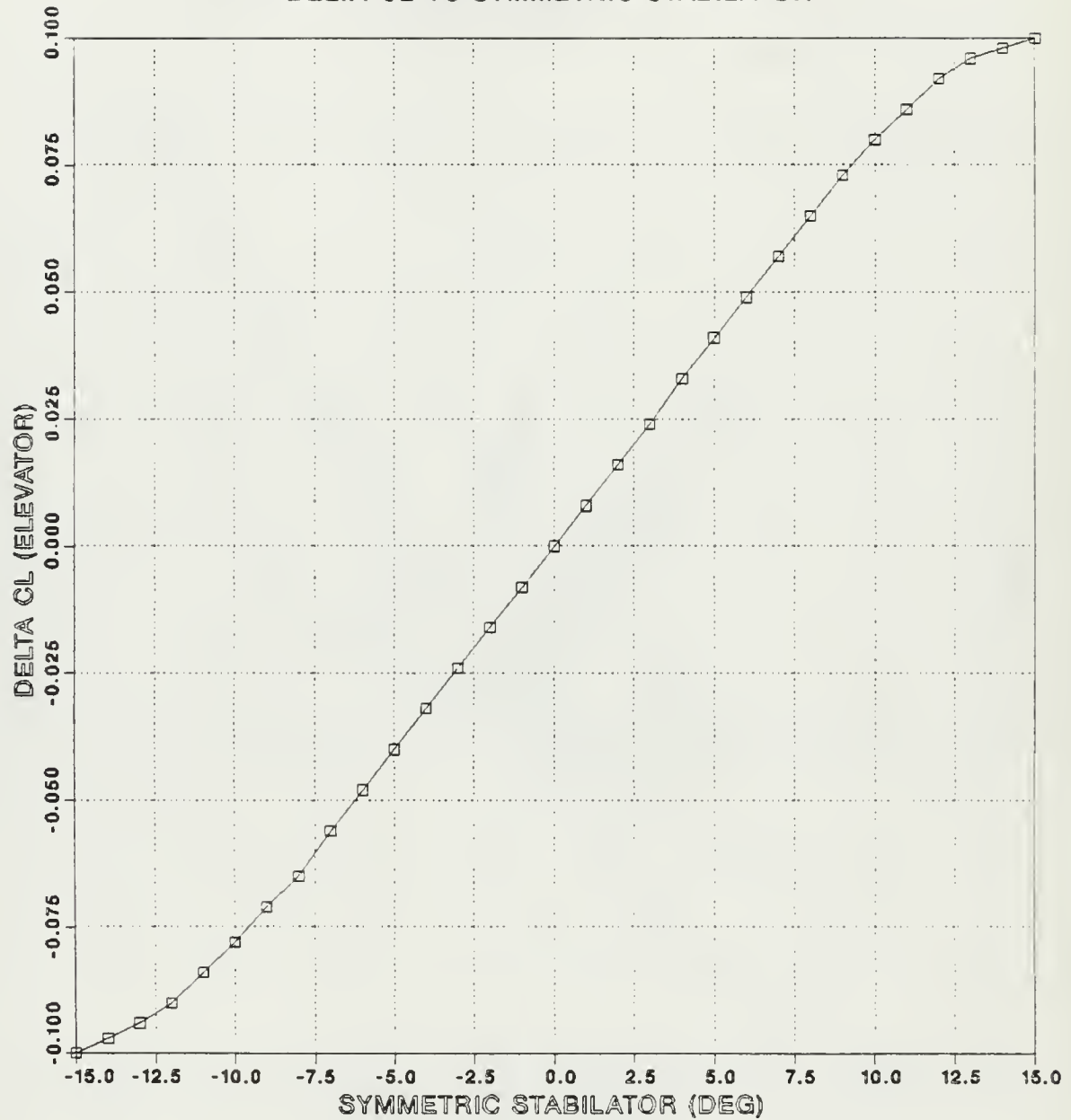


Figure A.3 Data Array LFT2.

STATIC AERODYNAMIC COEFFICIENTS

DRAG COEFFICIENT DATA

BASIC CD VS. AOA

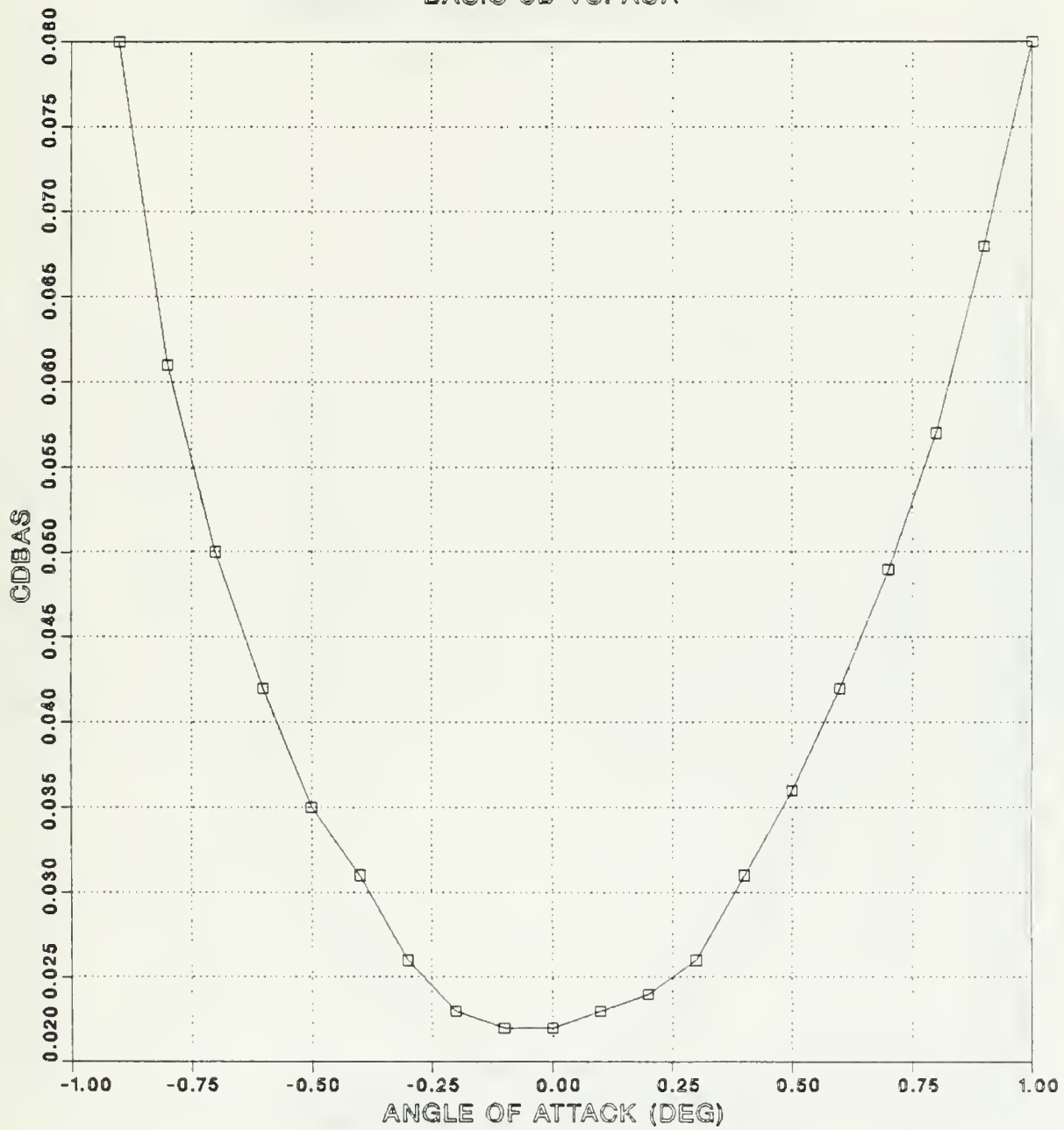


Figure A.4 Data Array DRG1.

STATIC AERODYNAMIC COEFFICIENTS

DRAG COEFFICIENT DATA

DELTA CD VS SYMMETRIC STABILATOR

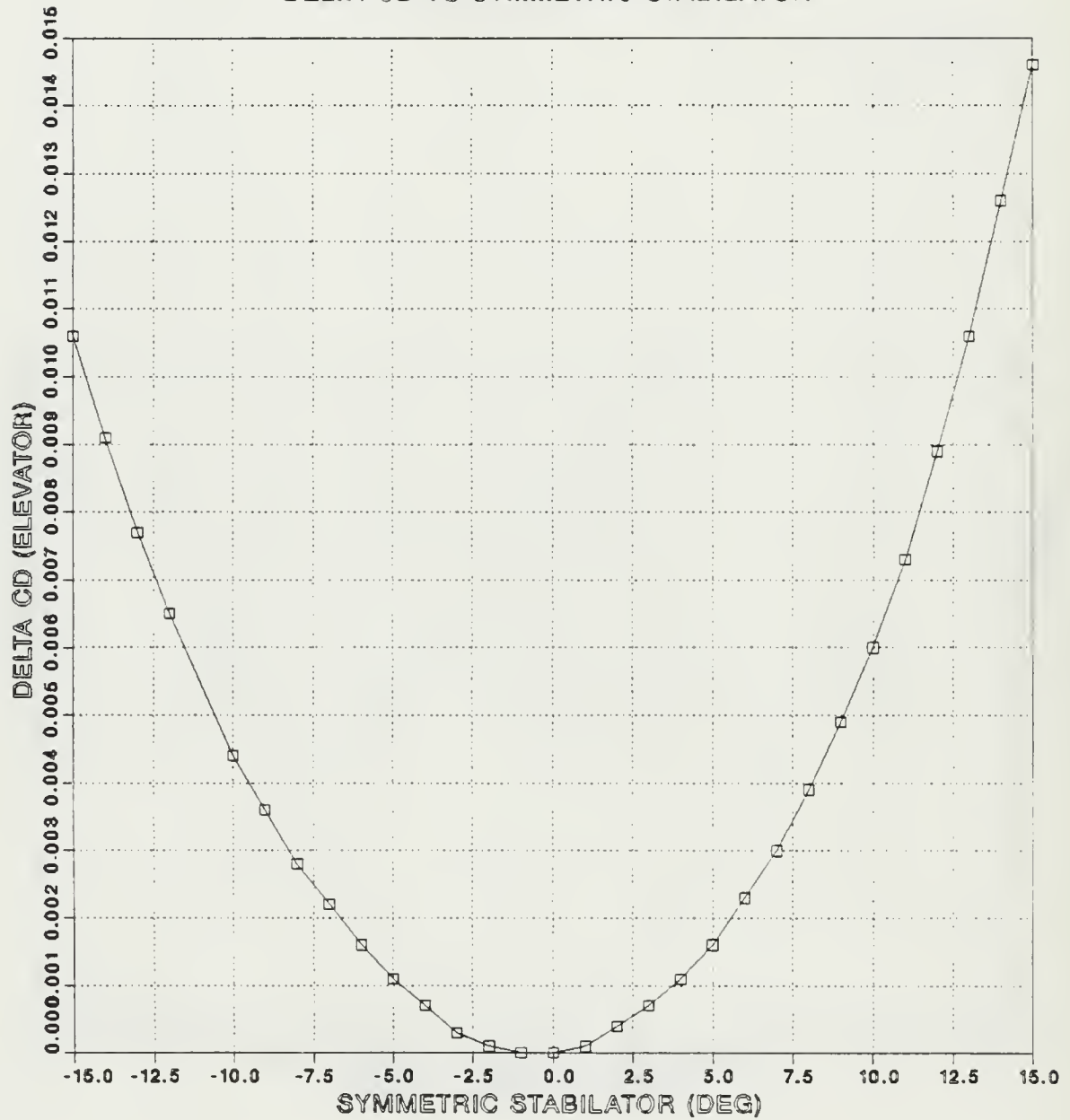


Figure A.5 Data Array DRG2.

STATIC AERODYNAMIC COEFFICIENTS

DRAG COEFFICIENT DATA

DELTA CD VS ASYMMETRIC STABILATOR

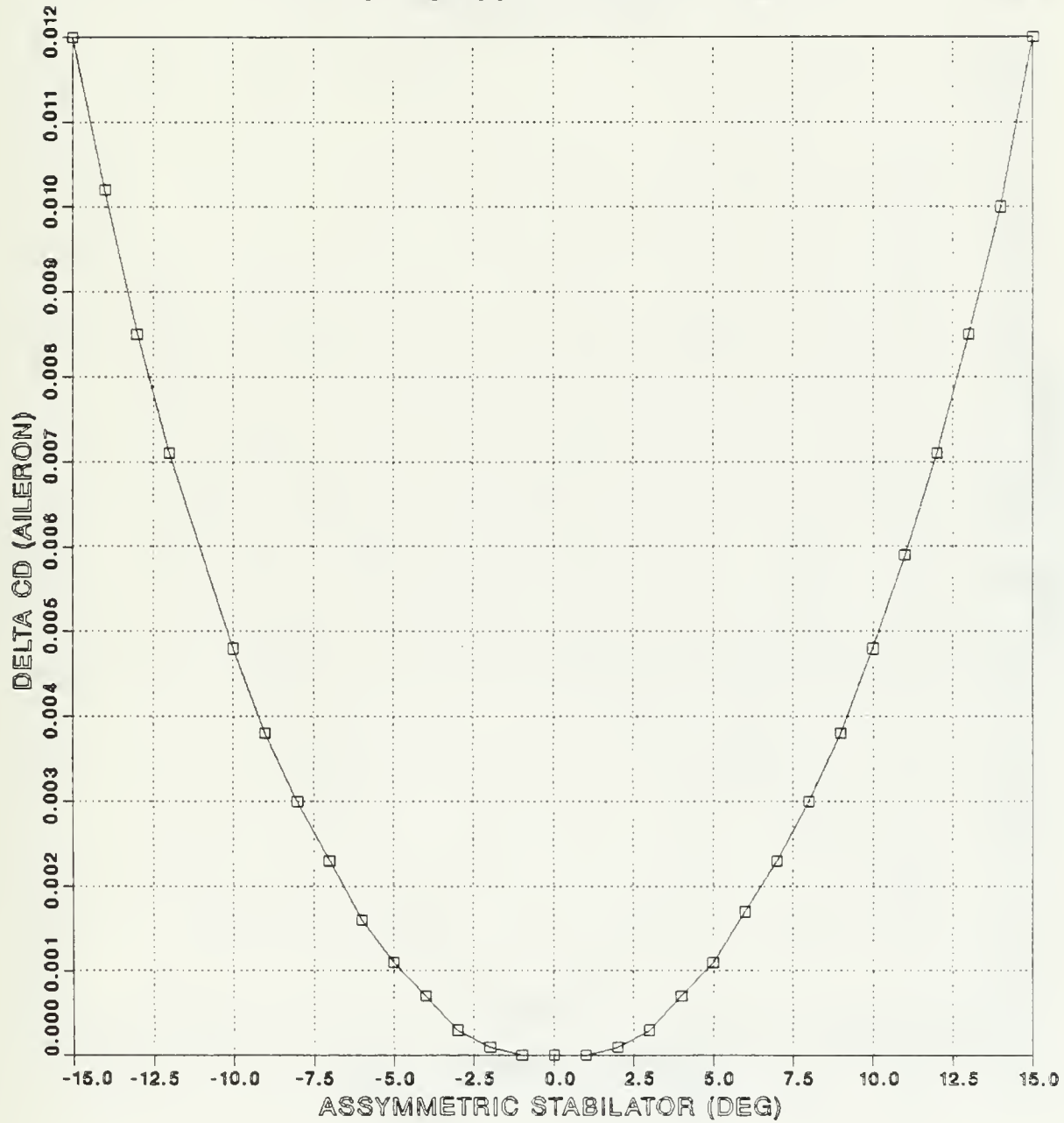


Figure A.6 Data Array DRG3.

STATIC AERODYNAMIC COEFFICIENTS

DRAG COEFFICIENT DATA

DELTA CD VS RUDDER

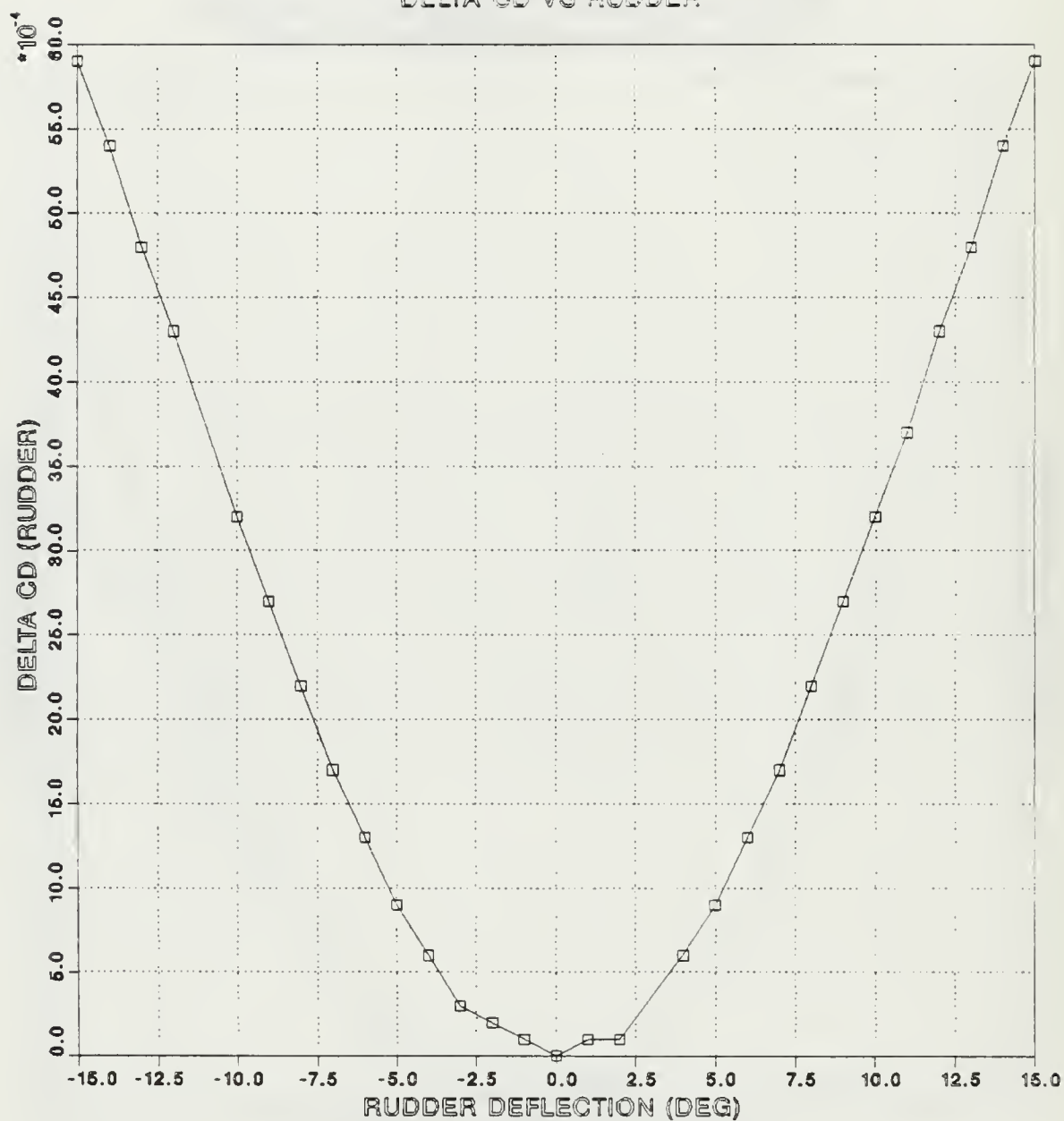


Figure A.7 Data Array DRG4.

STATIC AERODYNAMIC COEFFICIENTS
PITCHING MOMENT COEFFICIENT DATA
BASIC CM VS. AOA

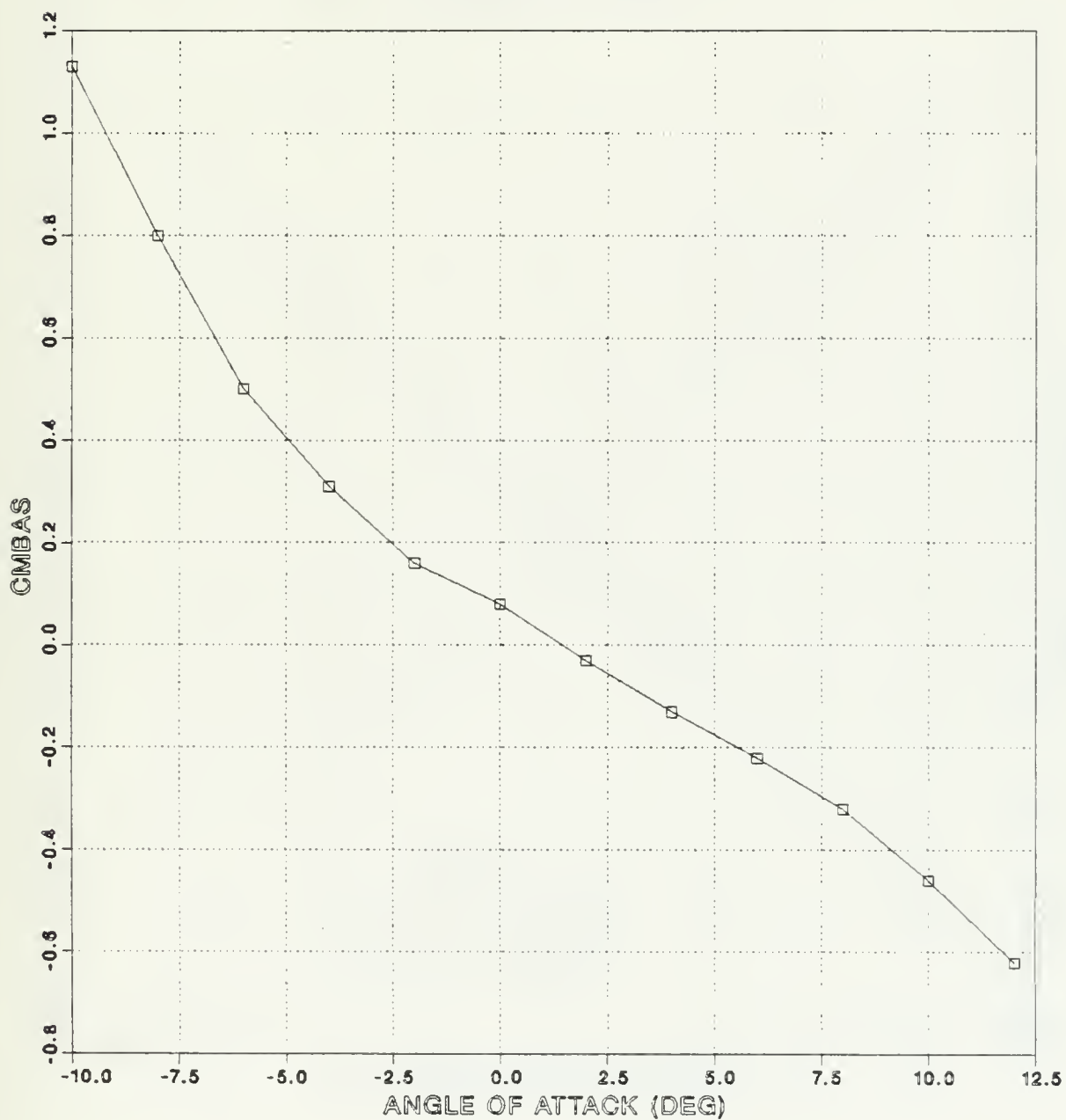


Figure A.8 Data Array PTCH1.

STATIC AERODYNAMIC COEFFICIENTS
PITCHING MOMENT COEFFICIENT DATA
DELTA CM VS SYMMETRIC STABILATOR

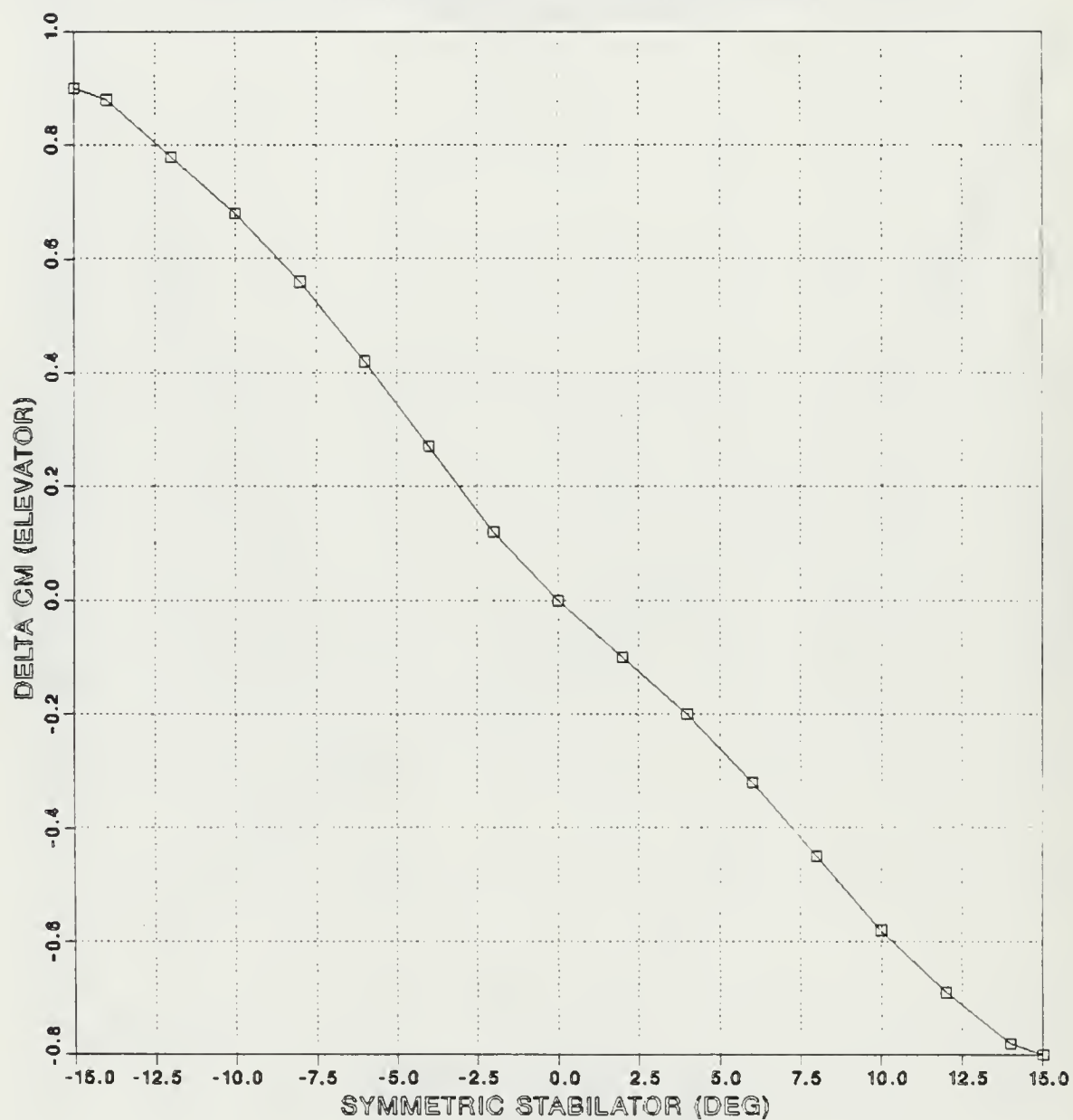


Figure A.9 Data Array PTCH2.

STATIC AERODYNAMIC COEFFICIENTS
SIDESLIP COEFFICIENT DATA
BASIC CY VS. BETA

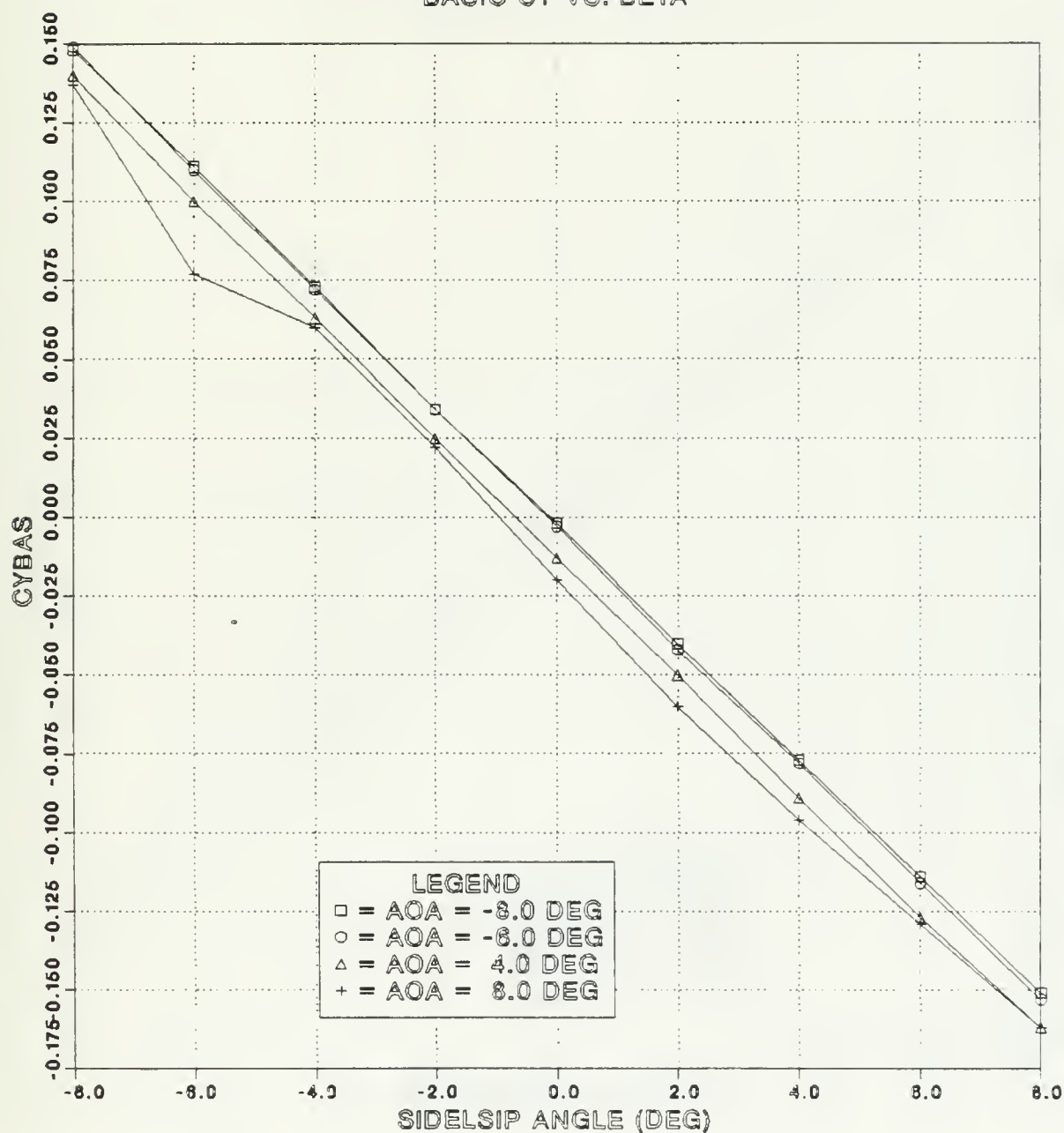


Figure A.10 Data Array SID1.

STATIC AERODYNAMIC COEFFICIENTS
SIDELIP COEFFICIENT DATA
 BASIC CROLL VS. BETA

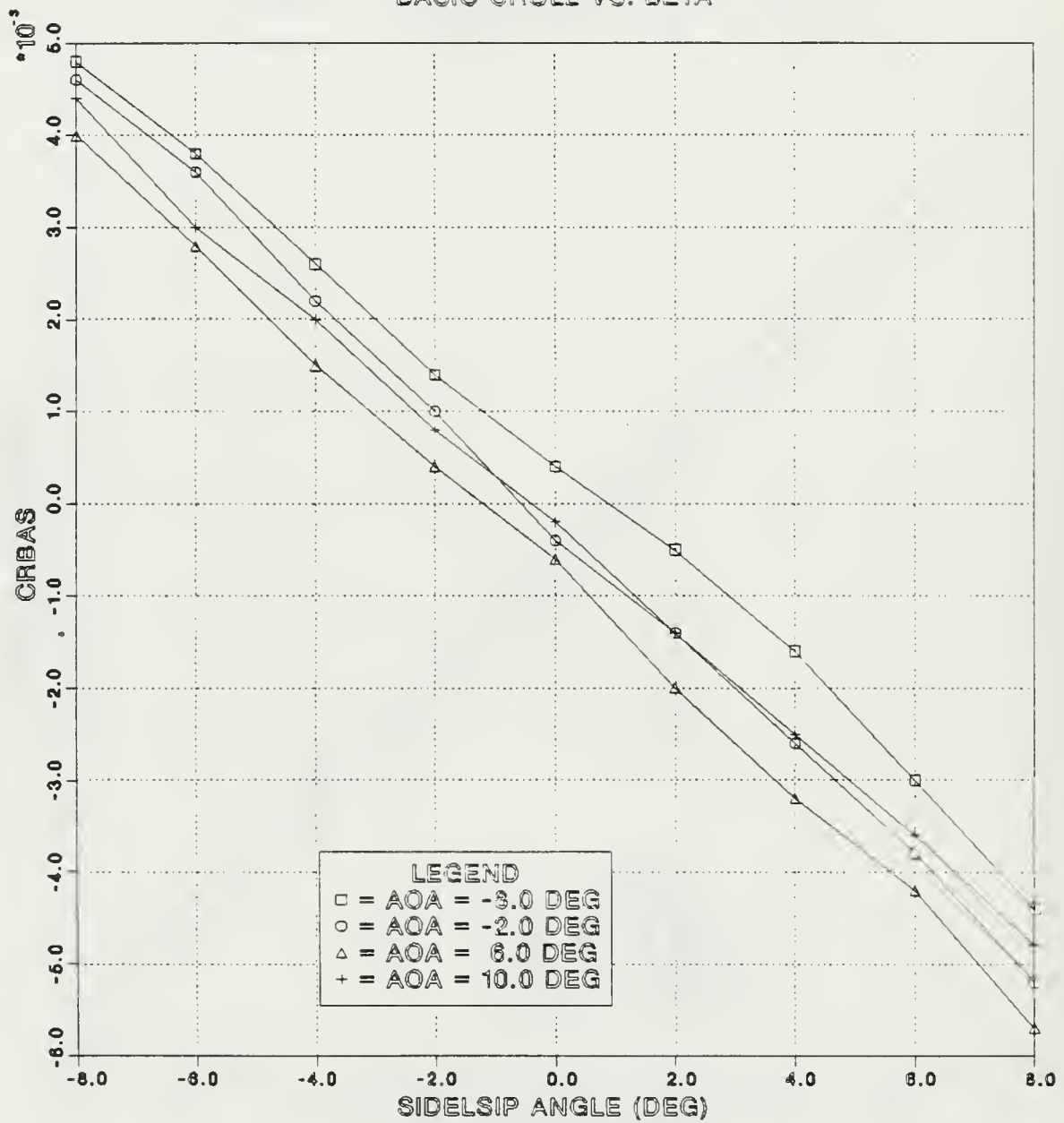


Figure A.11 Data Array SID2.

STATIC AERODYNAMIC COEFFICIENTS
SIDESLIP COEFFICIENT DATA
 BASIC CYAW VS. BETA

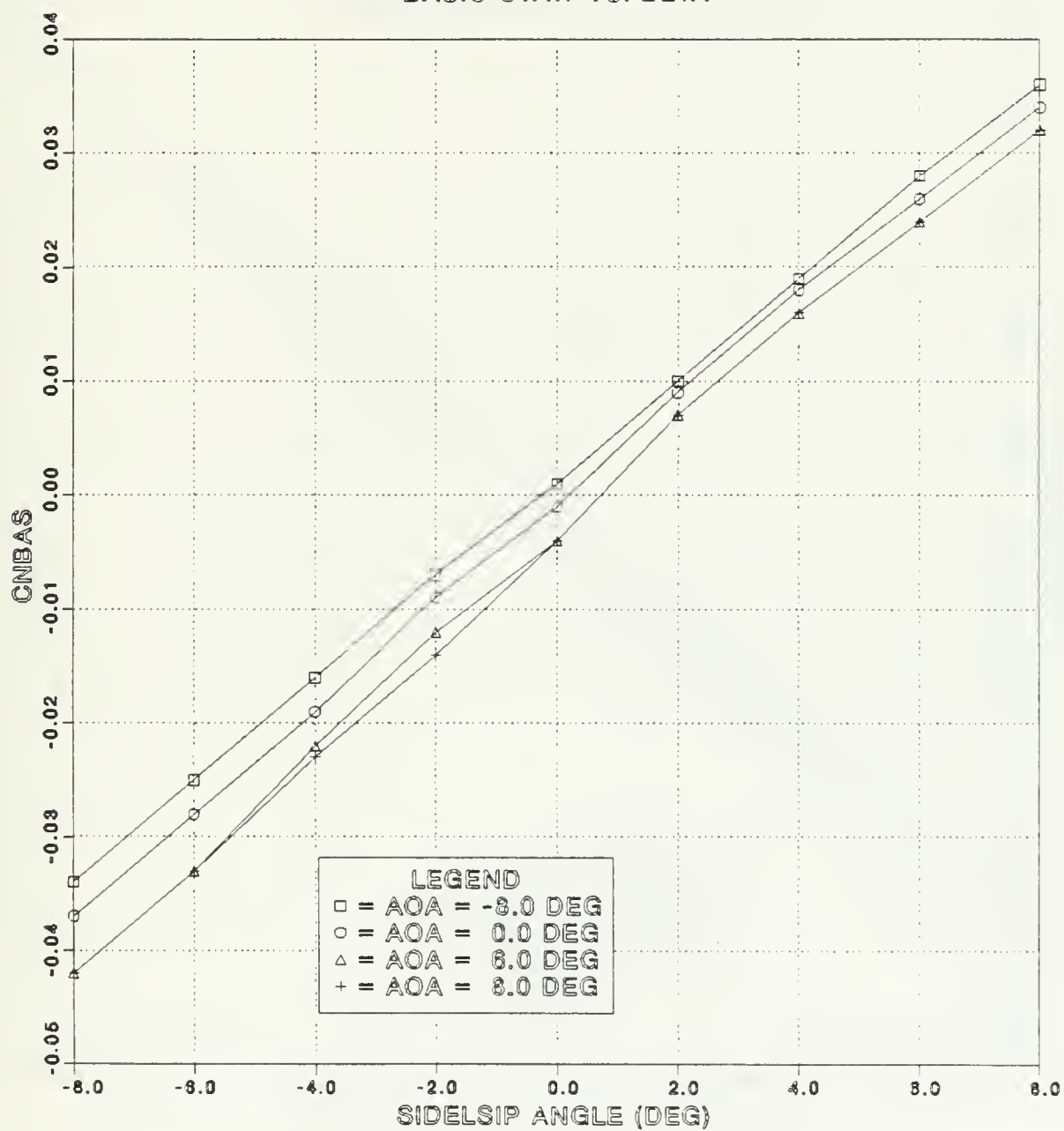


Figure A.12 Data Array SID3.

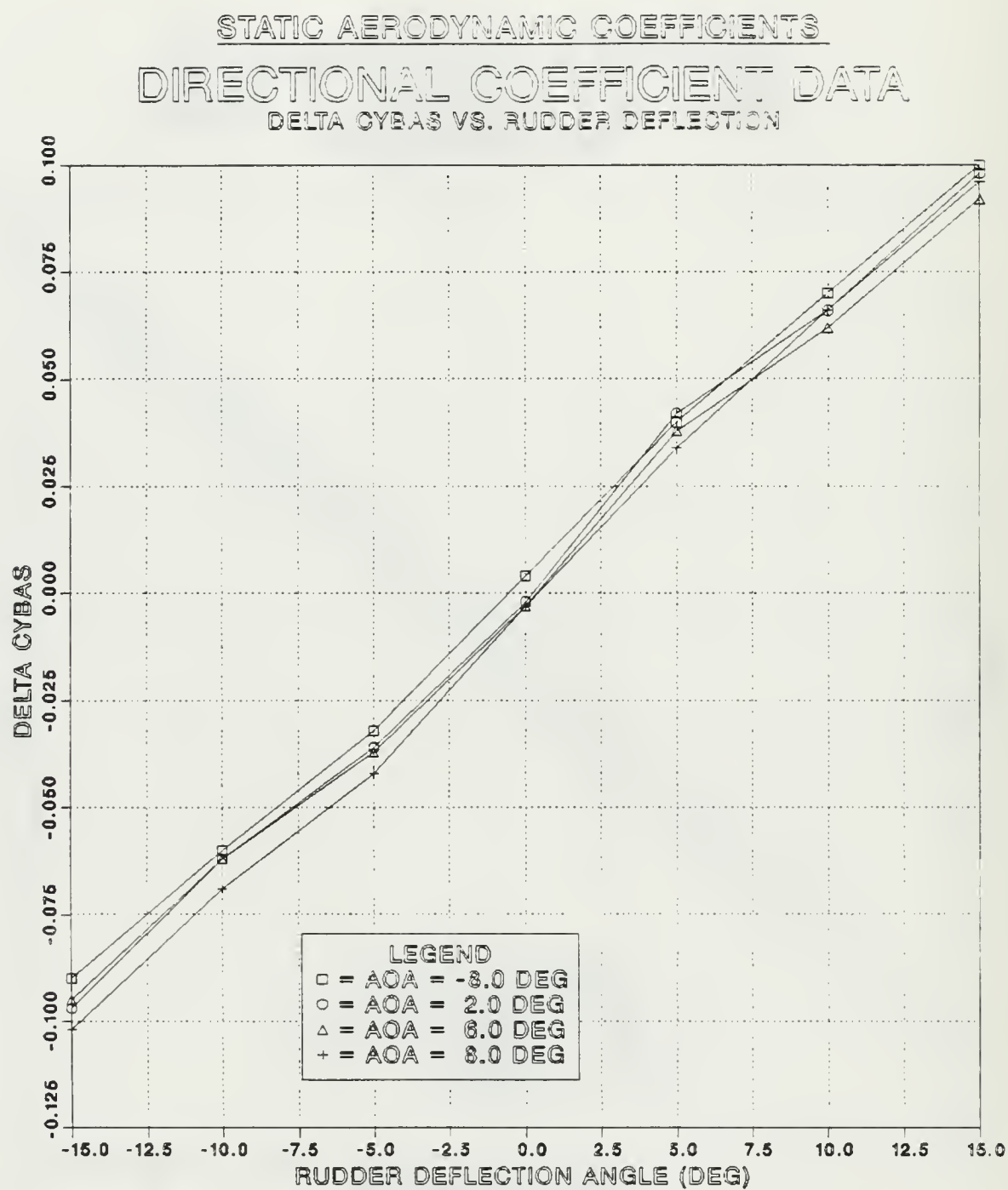


Figure A.13 Data Array DREC1.

STATIC AERODYNAMIC COEFFICIENTS
DIRECTIONAL COEFFICIENT DATA
DELTA CN VS. RUDDER DEFLECTION

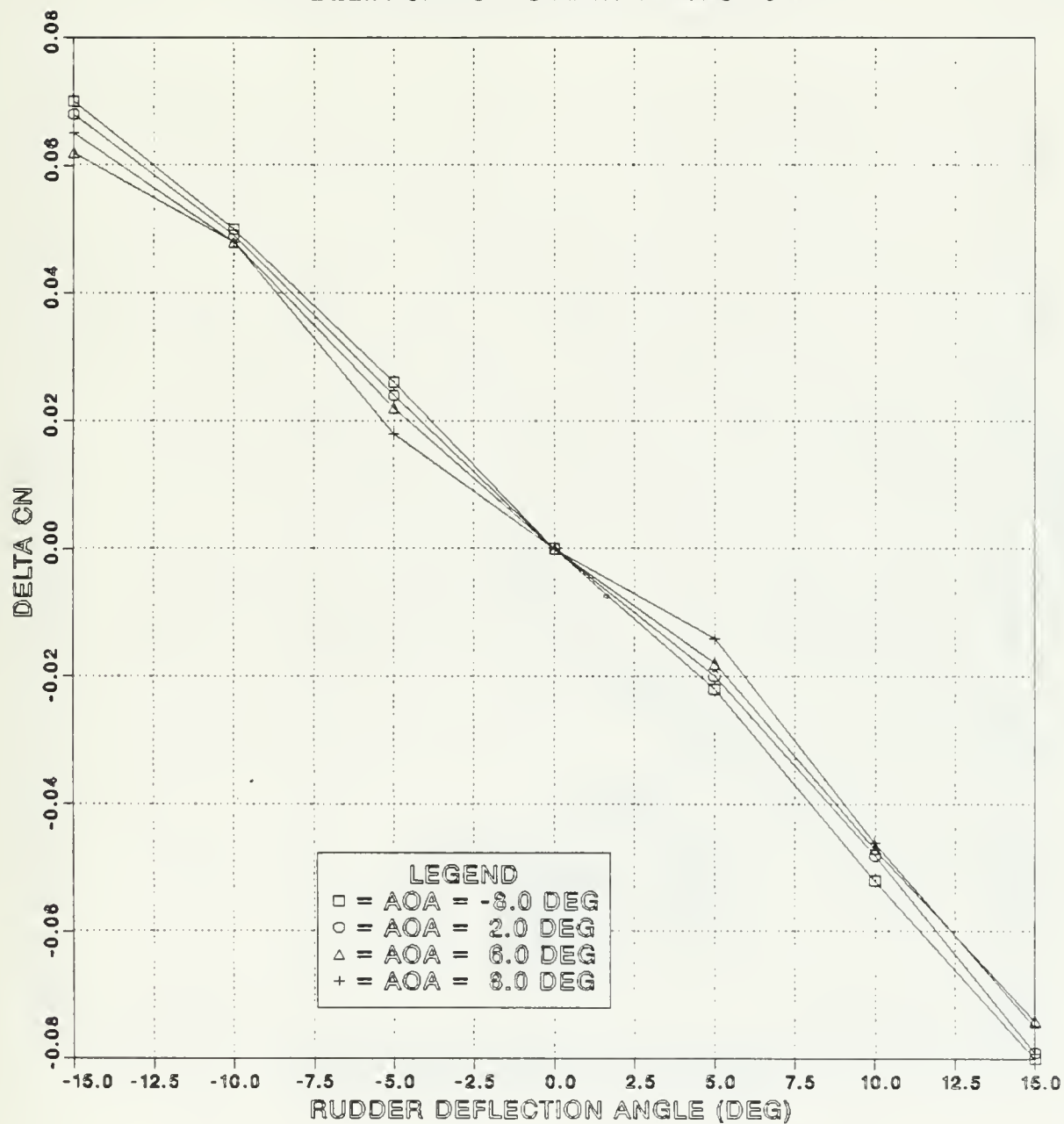


Figure A.14 Data Array DREC2.

STATIC AERODYNAMIC COEFFICIENTS
DIRECTIONAL COEFFICIENT DATA
DELTA CROLL VS. RUDDER DEFLECTION

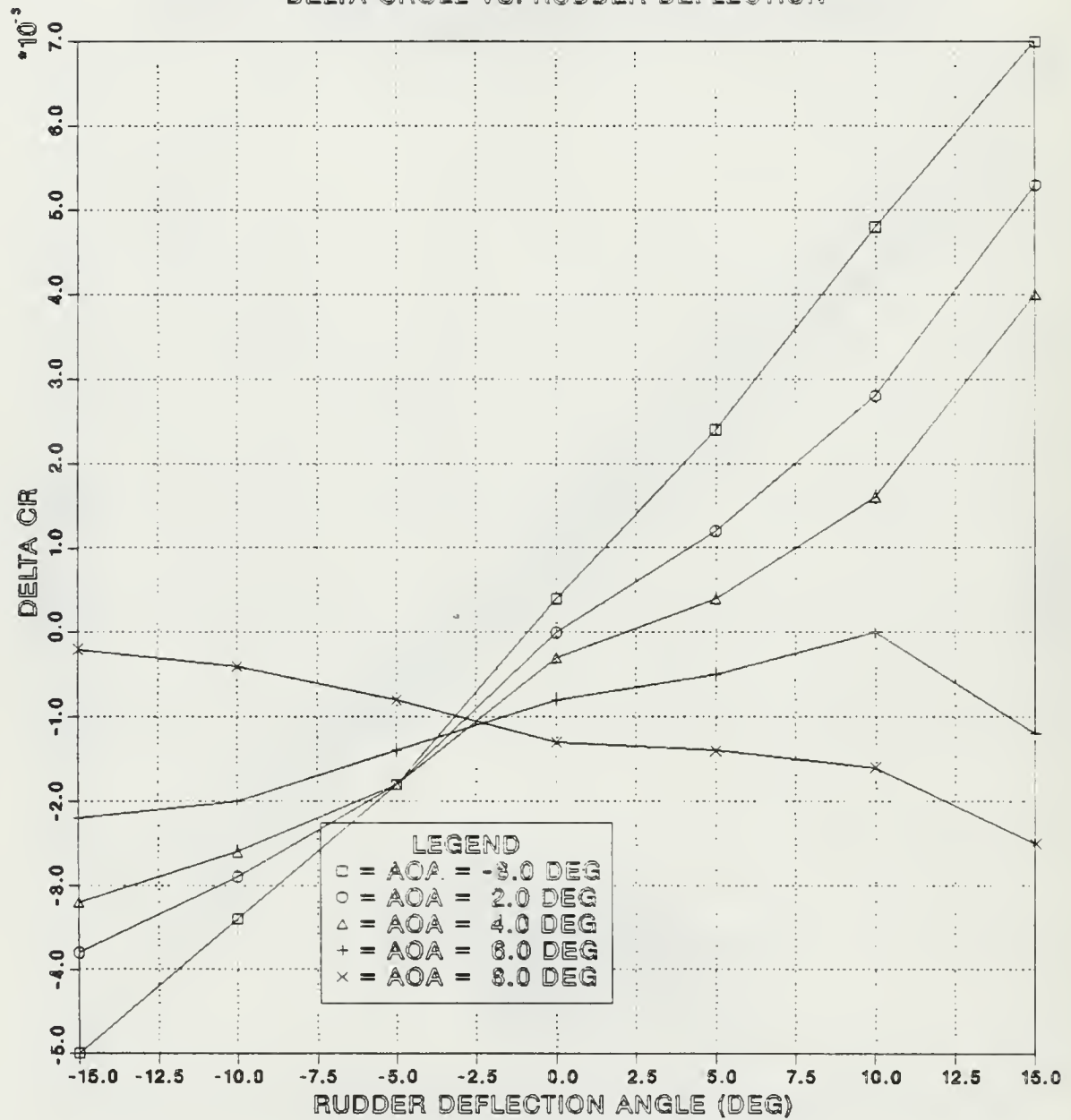


Figure A.15 Data Array DREC3.

STATIC AERODYNAMIC COEFFICIENTS
LATERAL COEFFICIENT DATA
DELTA CYBAS VS. ASYMMETRIC STABILATOR

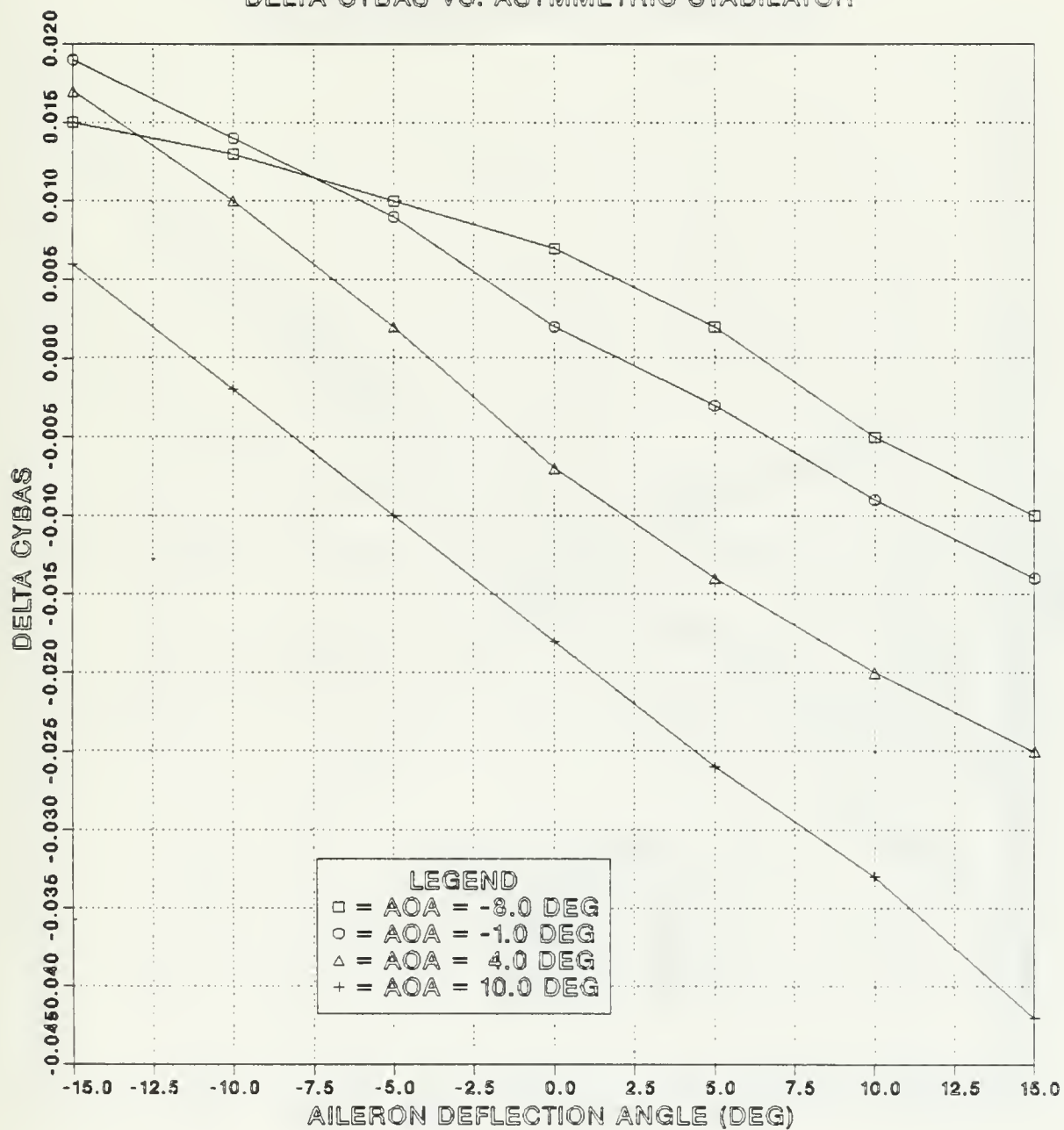


Figure A.16 Data Array LTRL1.

STATIC AERODYNAMIC COEFFICIENTS
LATERAL COEFFICIENT DATA
DELTA CN VS. ASYMMETRIC STABILATOR

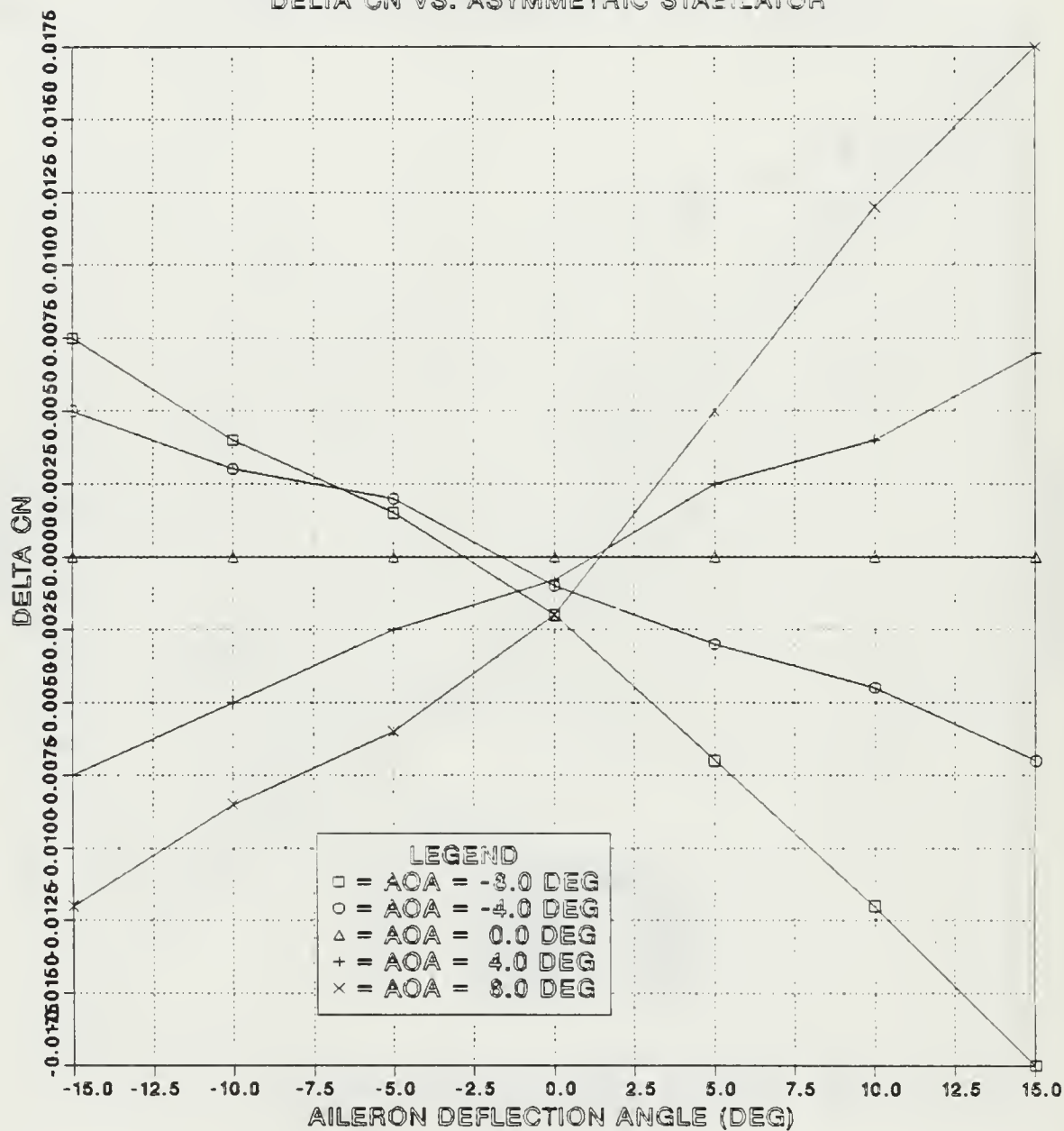


Figure A.17 Data Array LTFL2.

STATIC AERODYNAMIC COEFFICIENTS
LATERAL COEFFICIENT DATA
 DELTA CROLL VS. ASYMMETRIC STABILATOR

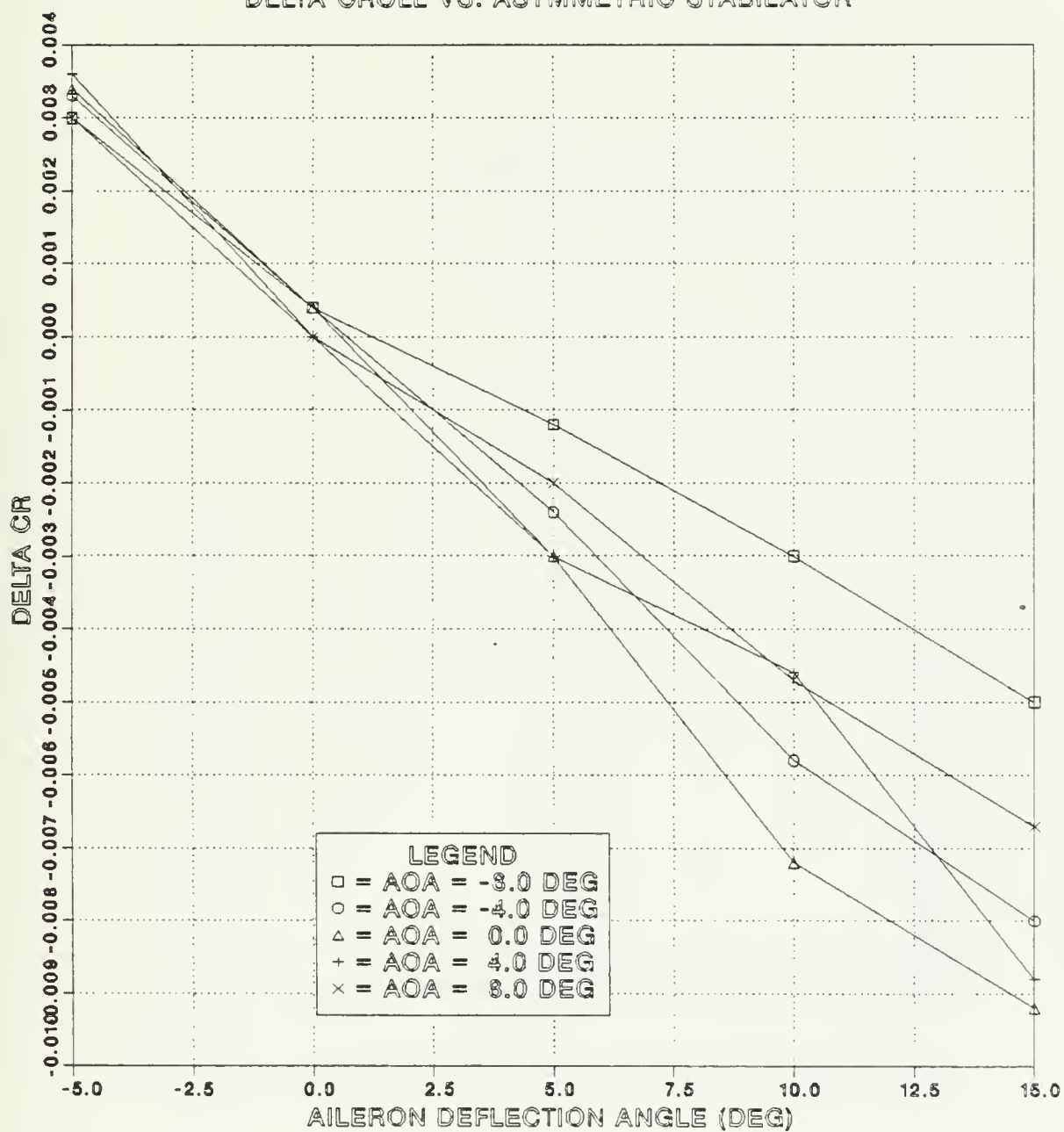


Figure A.18 Data Array LTRL3.

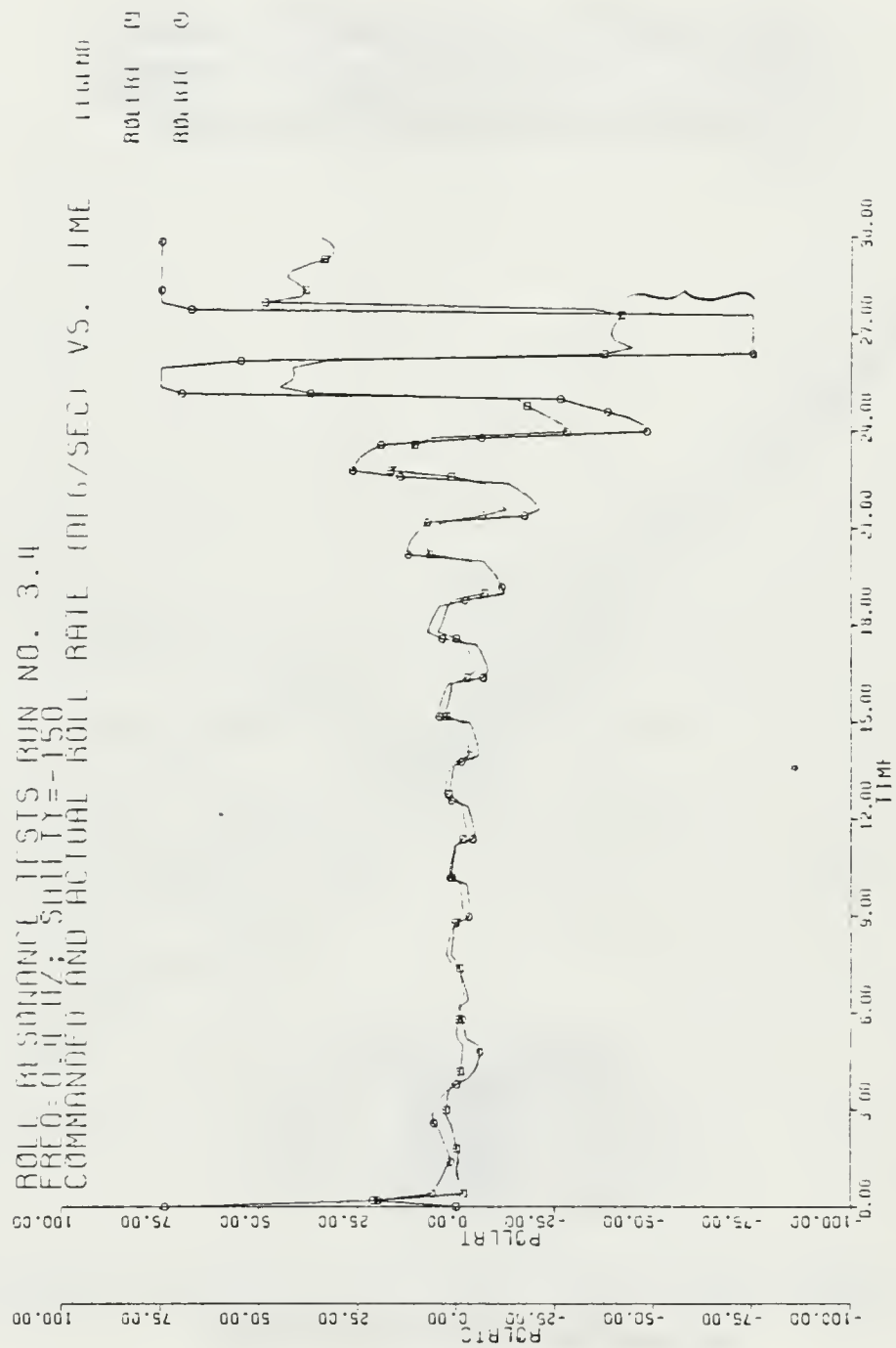


Figure A.19 CSMP Data (Roll Rate) - KROLLR = 0.1.

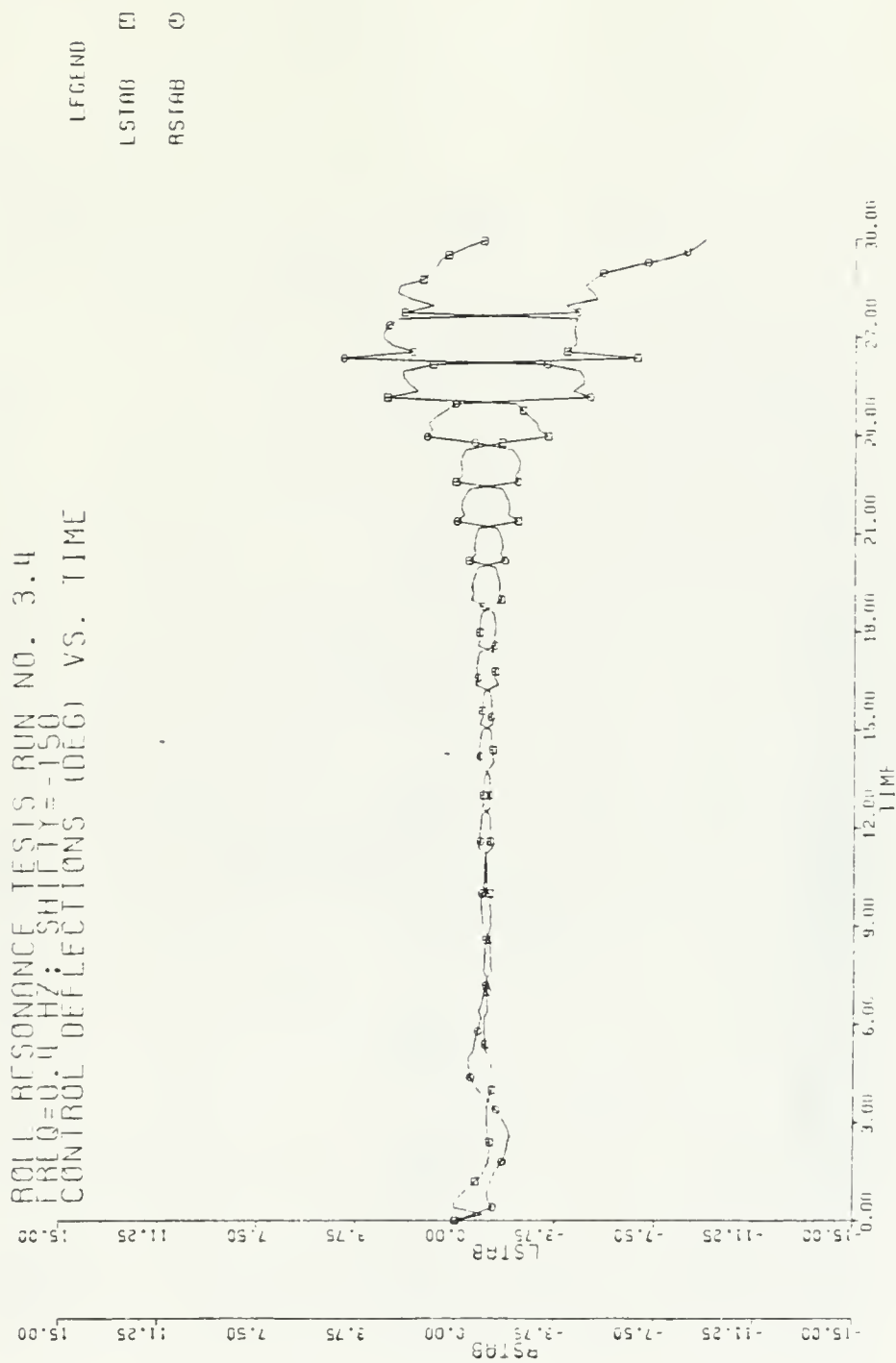


Figure A.20 CSMP Data (Controls) - KROLLP = 0.1.

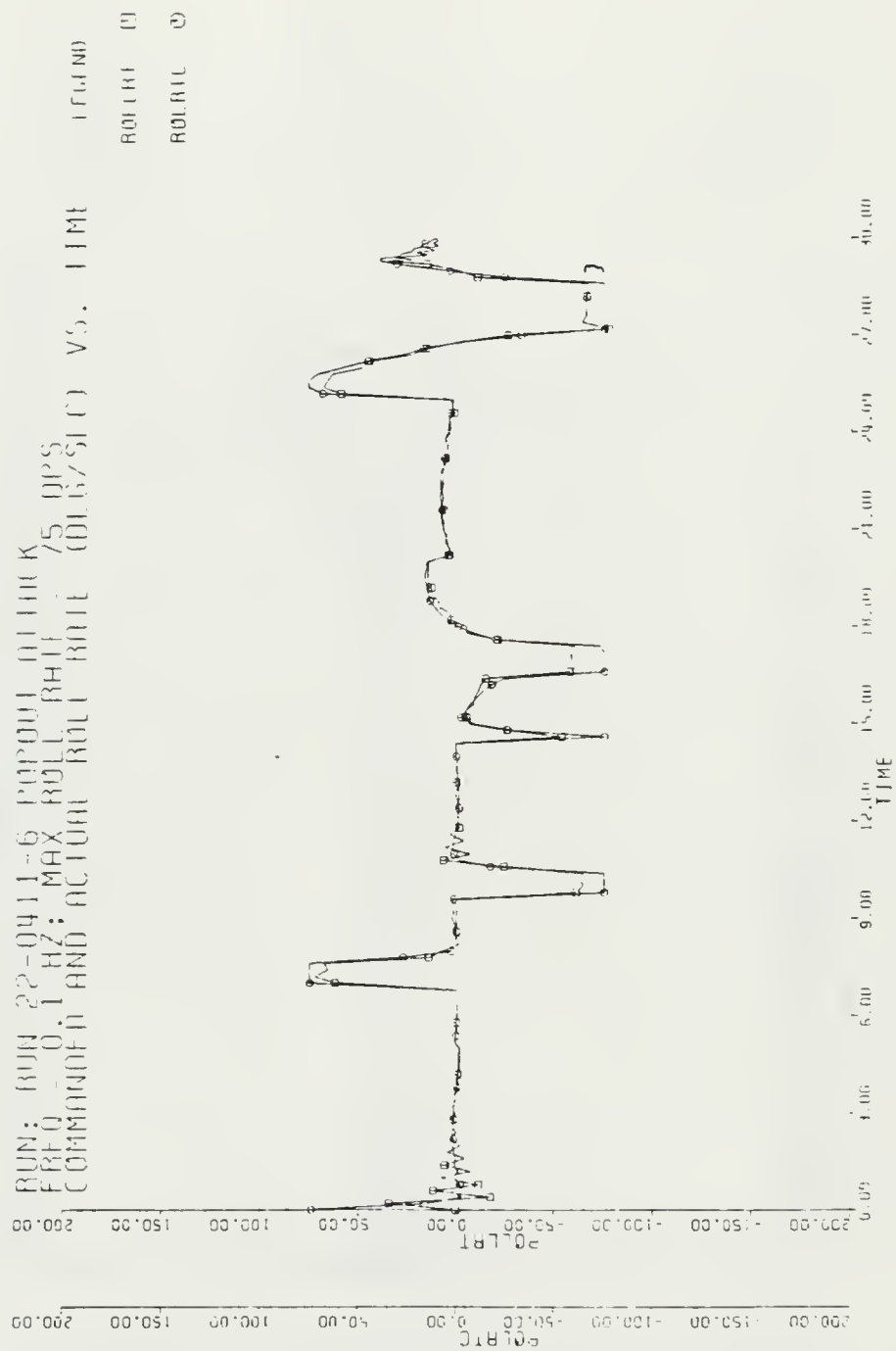


Figure A.21 CSMP Data (Roll Rate) - KROLLR = 0.5.

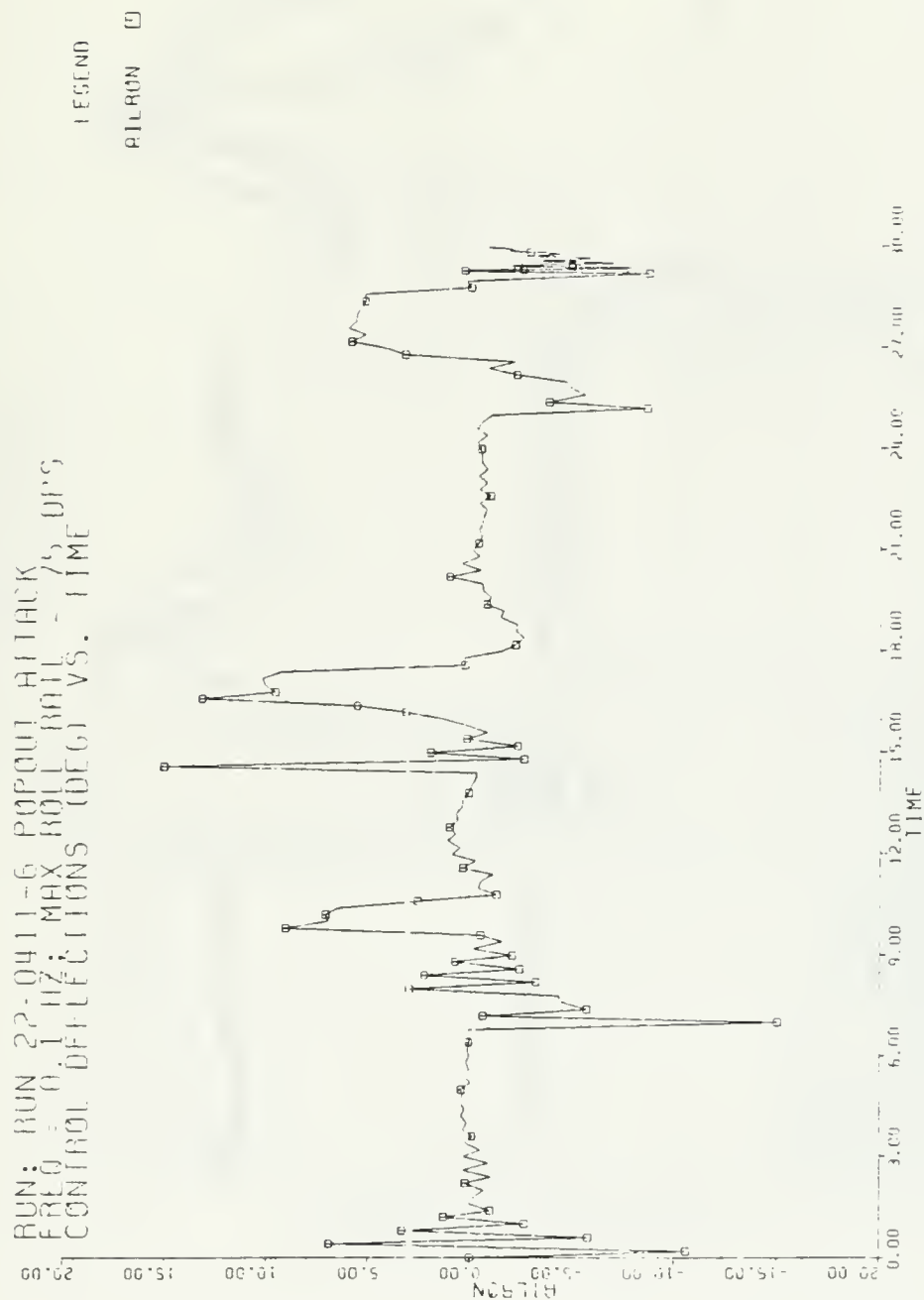


Figure A.22 CSMP Data (Controls) - Krollr = 0.5.

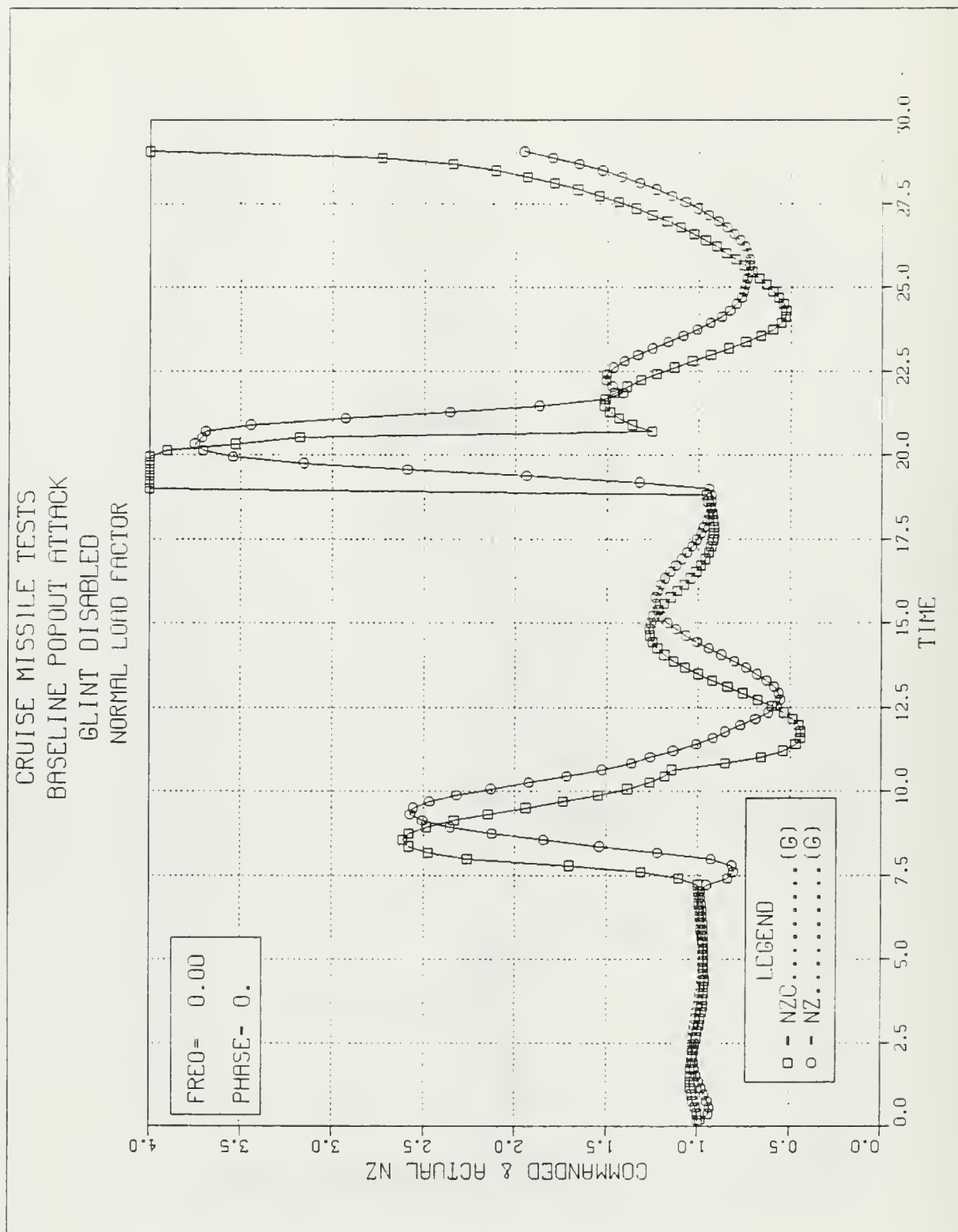


Figure A.23 Baseline - no ECM or GLINT - Load Factor.

CRUISE MISSILE TESTS
 BASELINE POPOUT ATTACK
 GLINT DISABLED
 ROLL RATE CONTROL

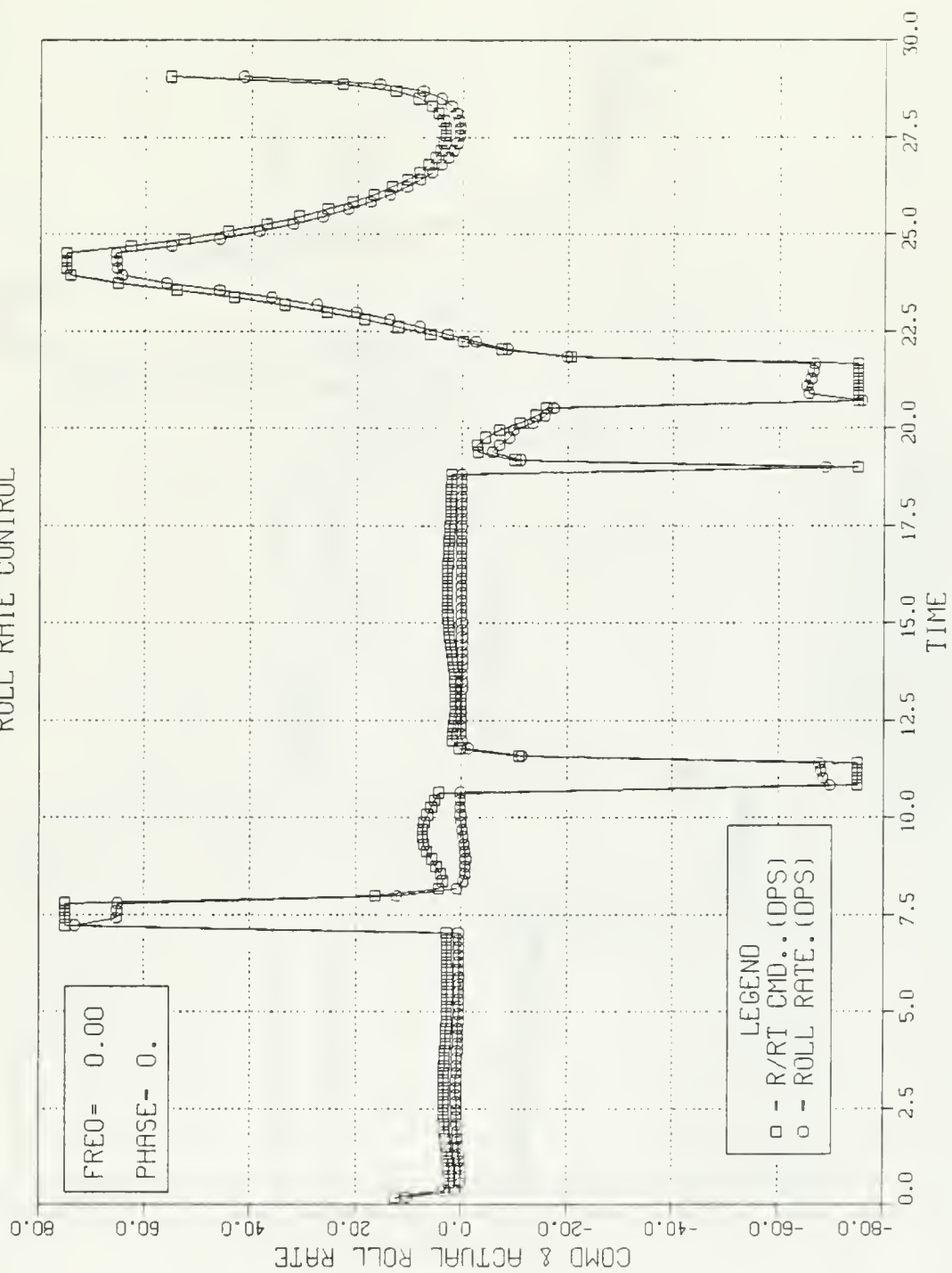


Figure A.24 Baseline - no ECM or GLINT - Roll Rate.

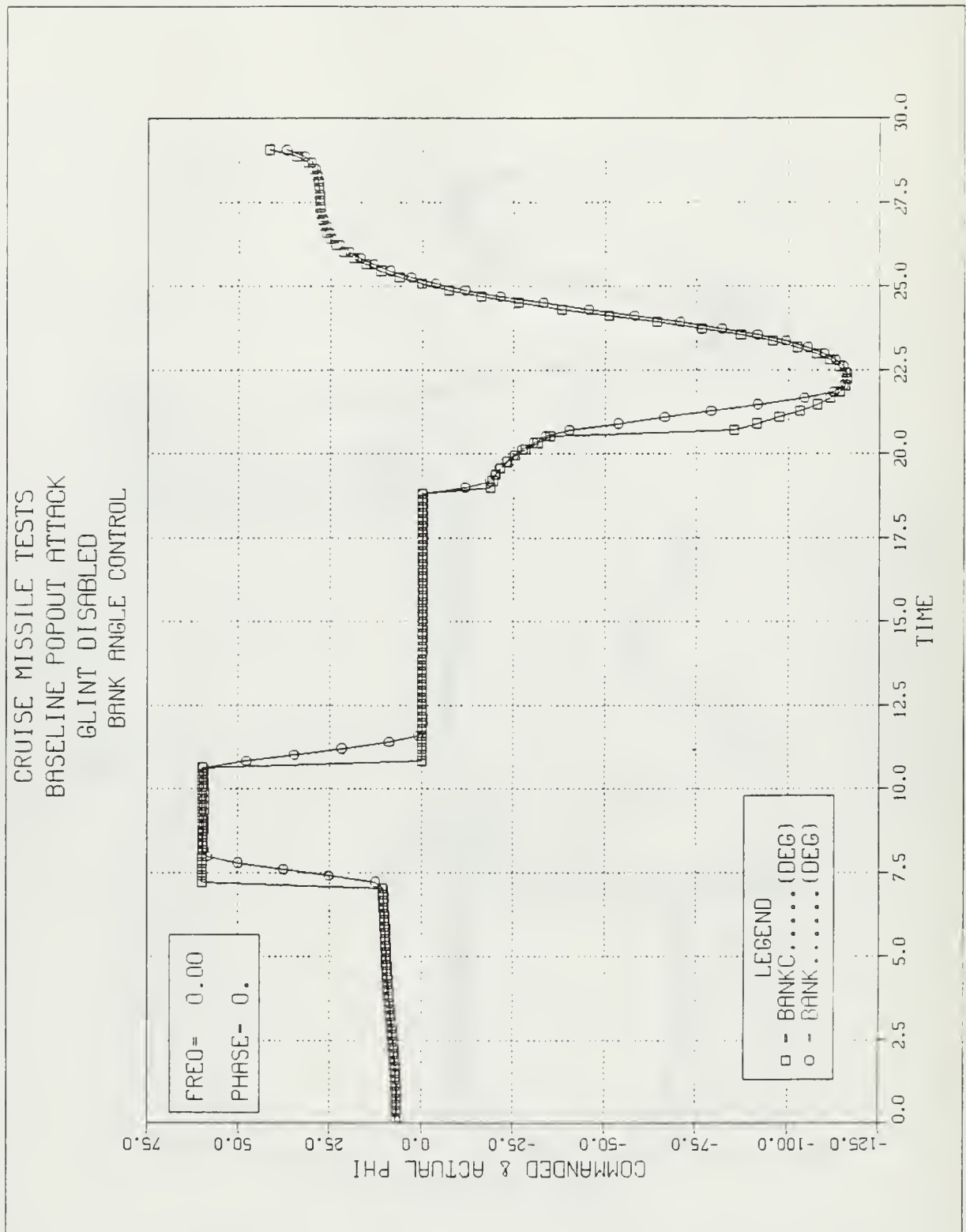


Figure A.25 Baseline - no ECM or GLINT - Bank.

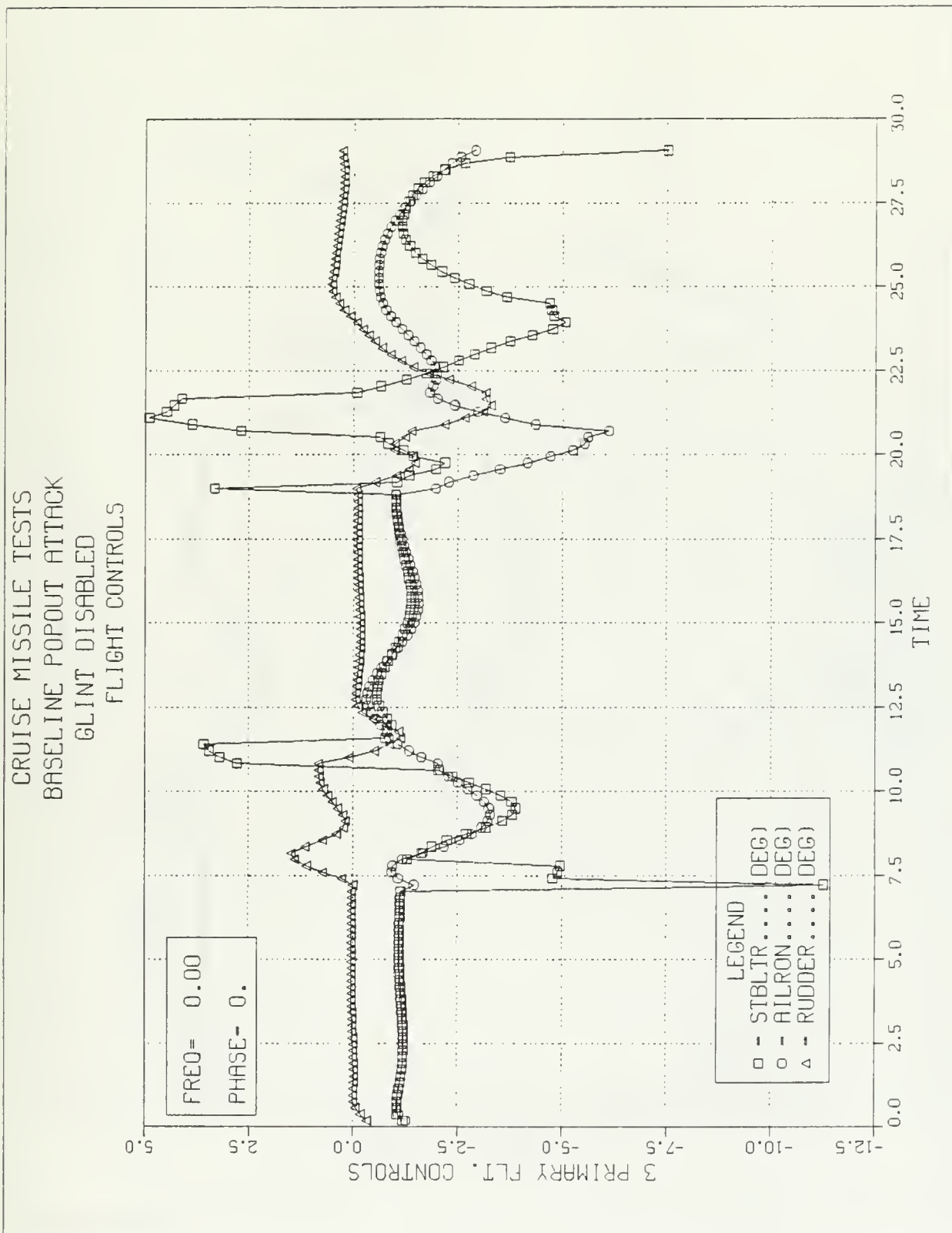


Figure A.26 Baseline - no ECM or GLINT - Controls.

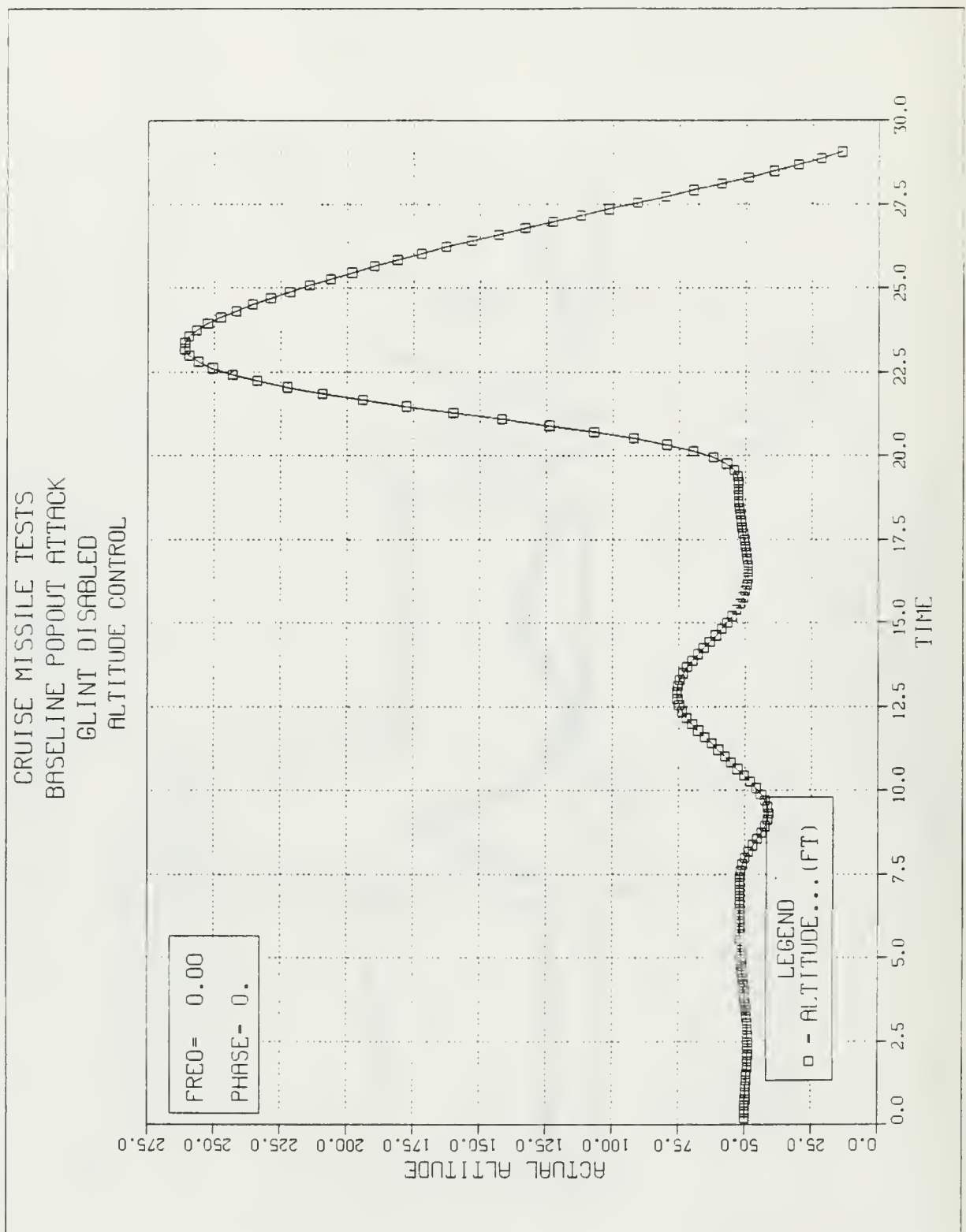


Figure A.27 Baseline - no ECM or GLINT - Altitude.

CRUISE MISSILE TESTS
 BASELINE POPOUT ATTACK
 GLINT DISABLED

FREQ= 0.
 PHASE= 0.

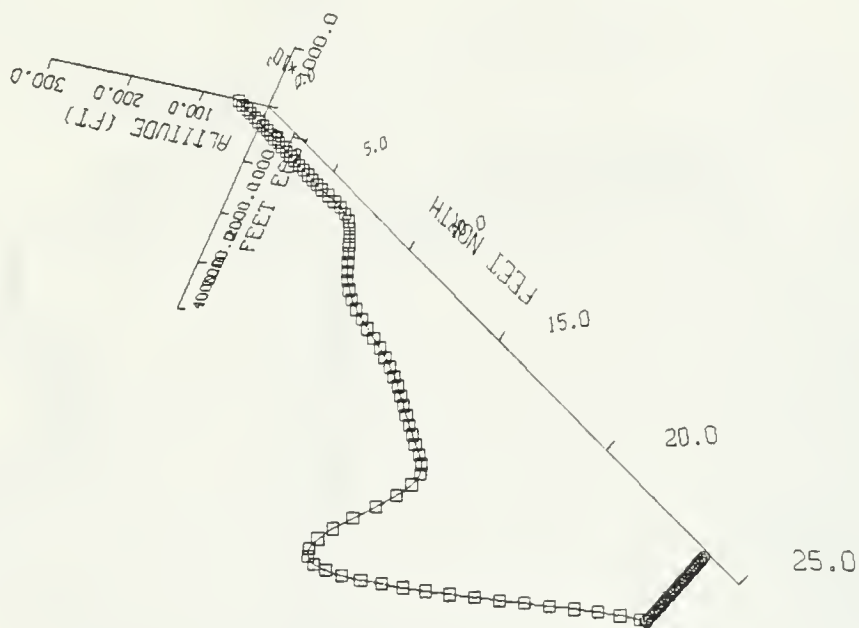


Figure A.28 Baseline - no ECM or GLINT - Geo Plot.

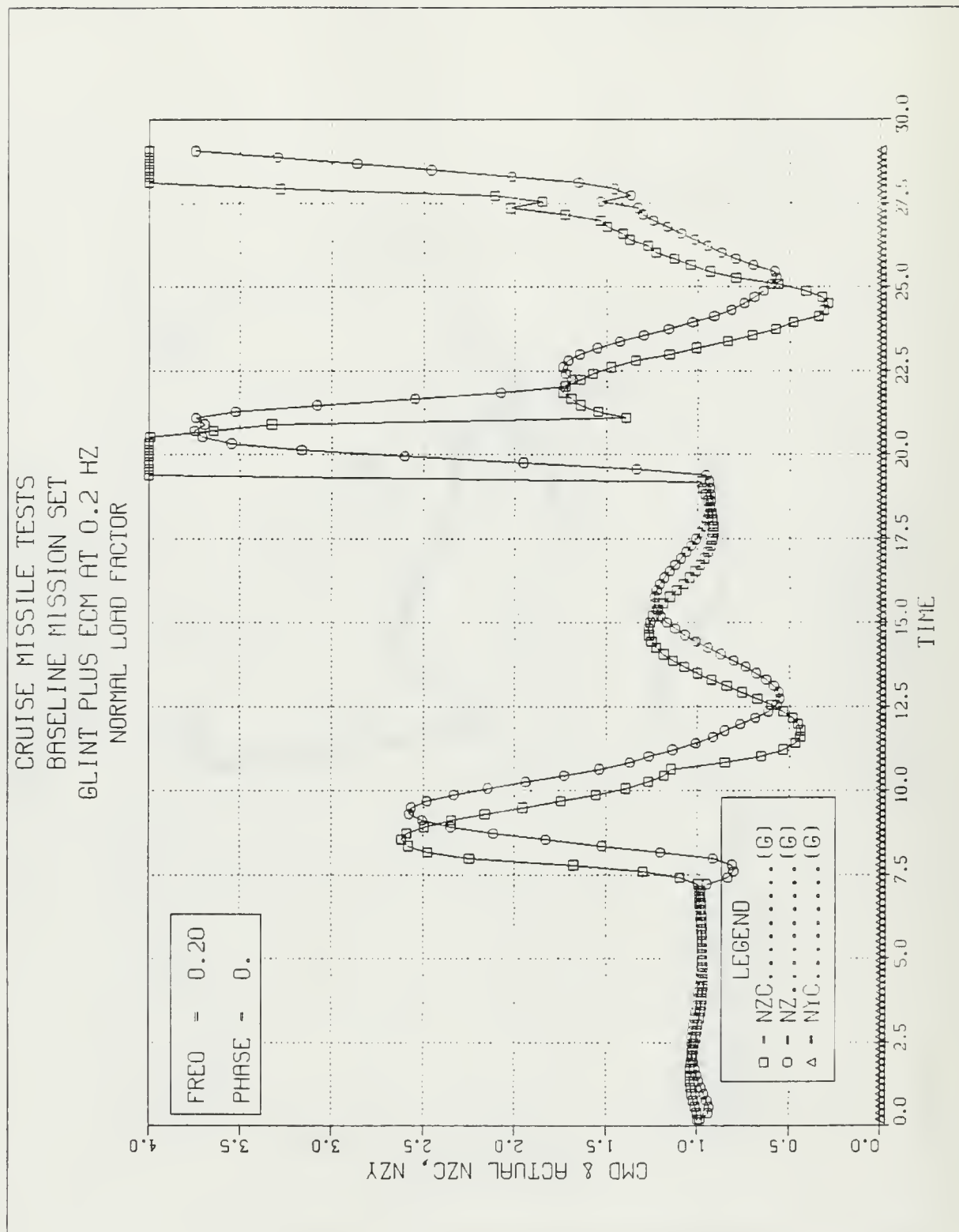


Figure A.29 Baseline with GLINT & ECM - Load Factor.

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 BANK ANGLE CONTROL

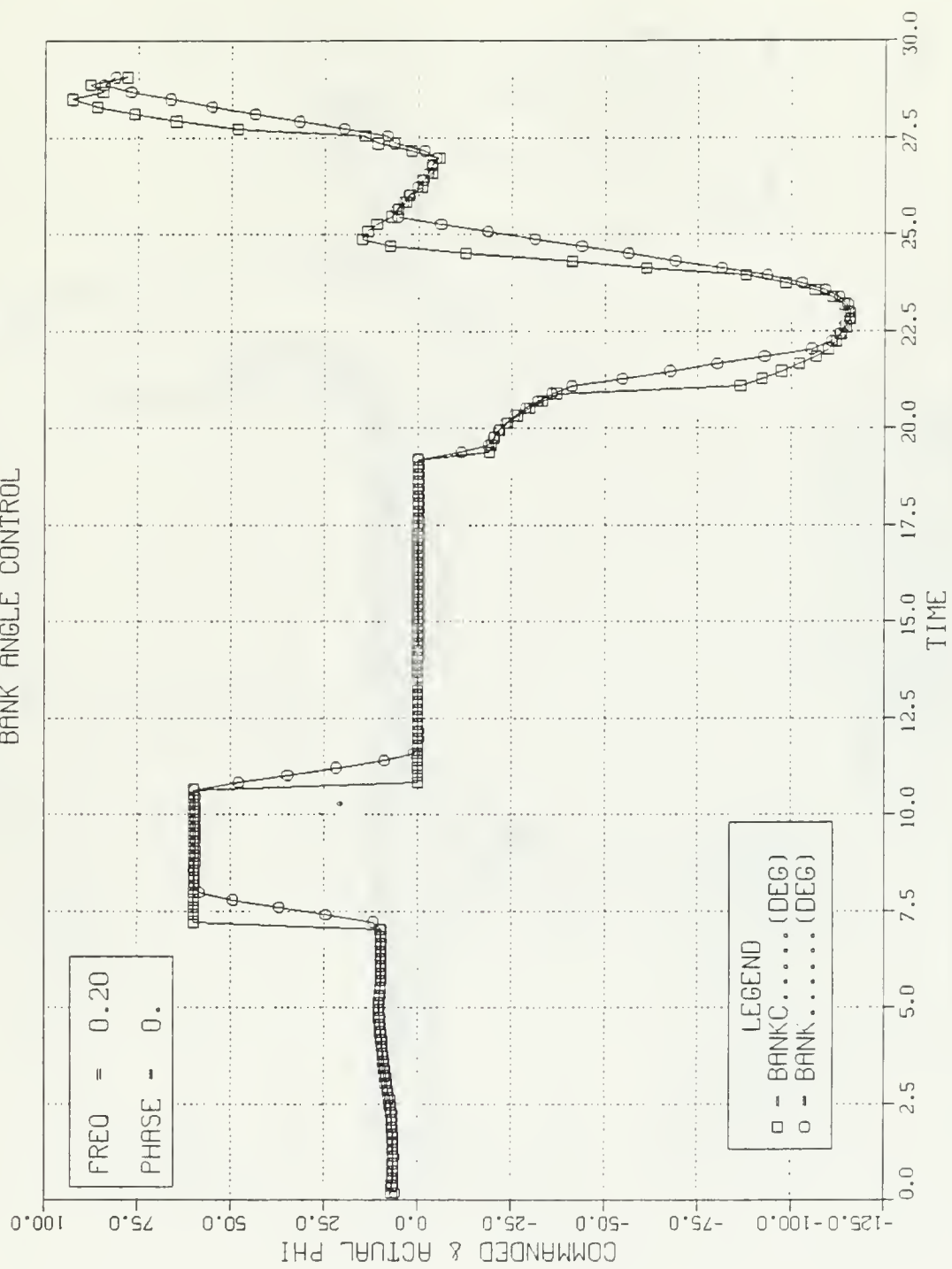


Figure A.30 Baseline with GLINT & ECM - Bank.

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ROLL RATE CONTROL

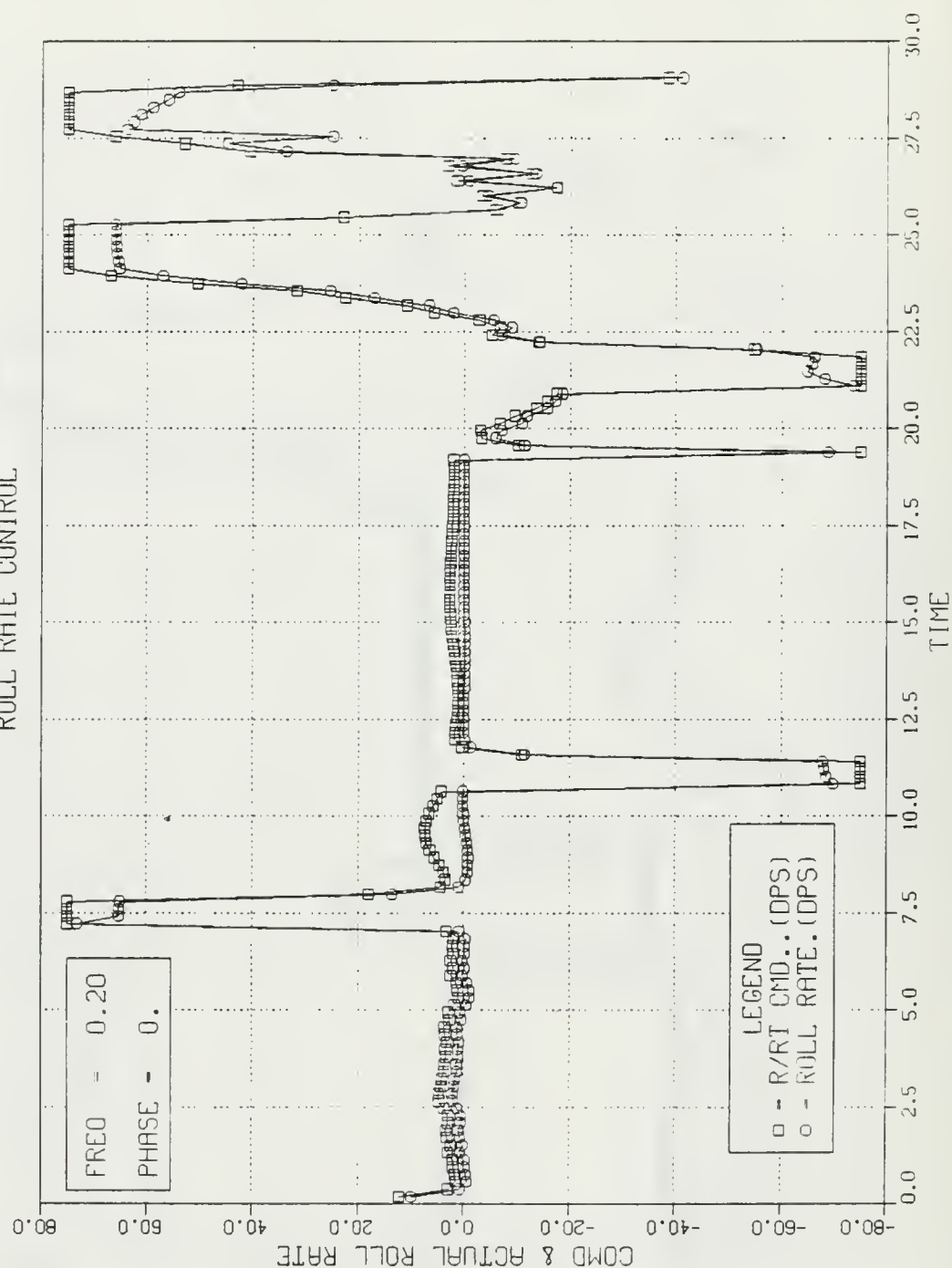


Figure A.31 Baseline with GLINT & ECM - Roll Rate.

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 FLIGHT CONTROLS

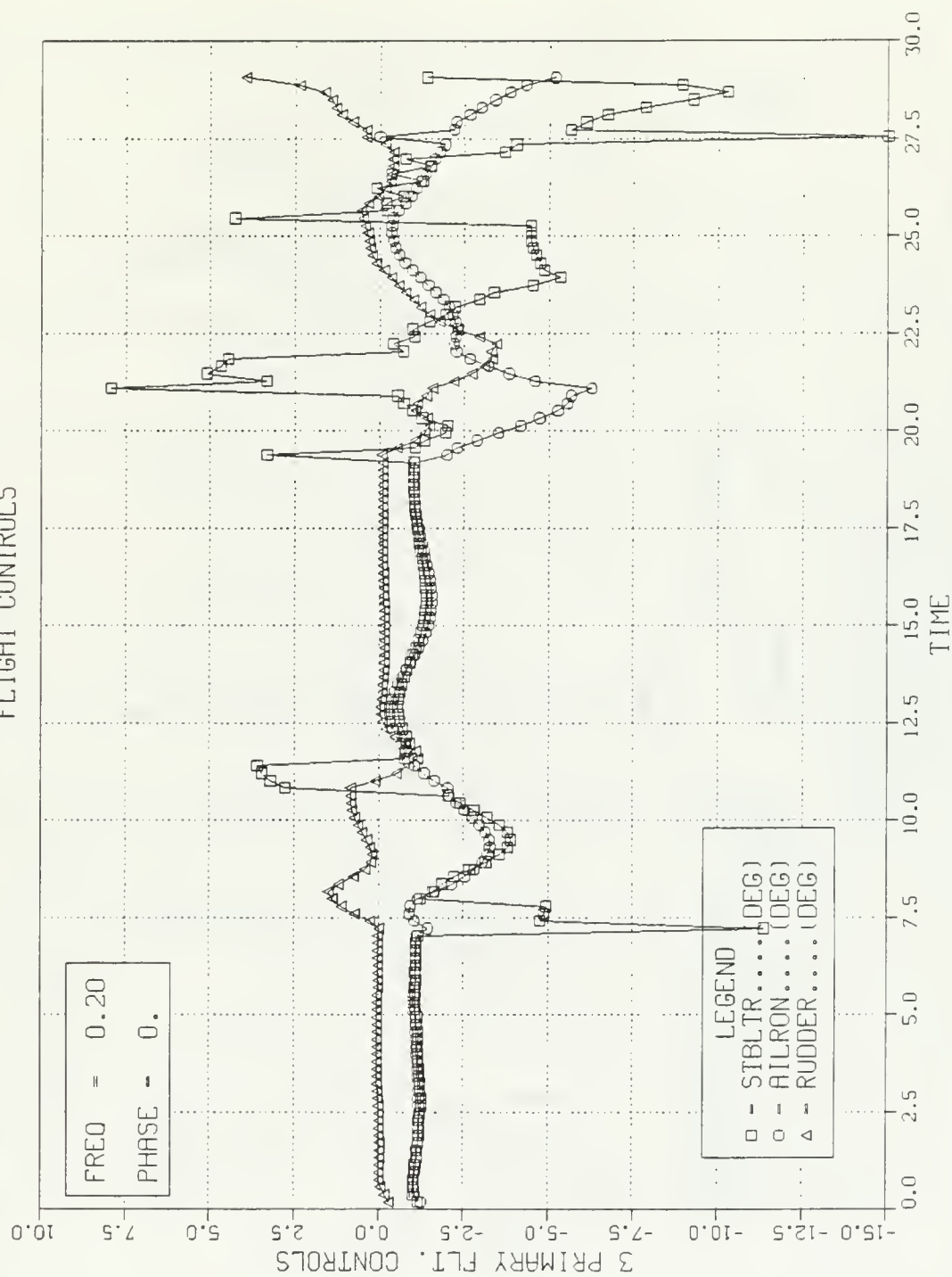


Figure A.32 Baseline with GLINT & ECM - Controls.

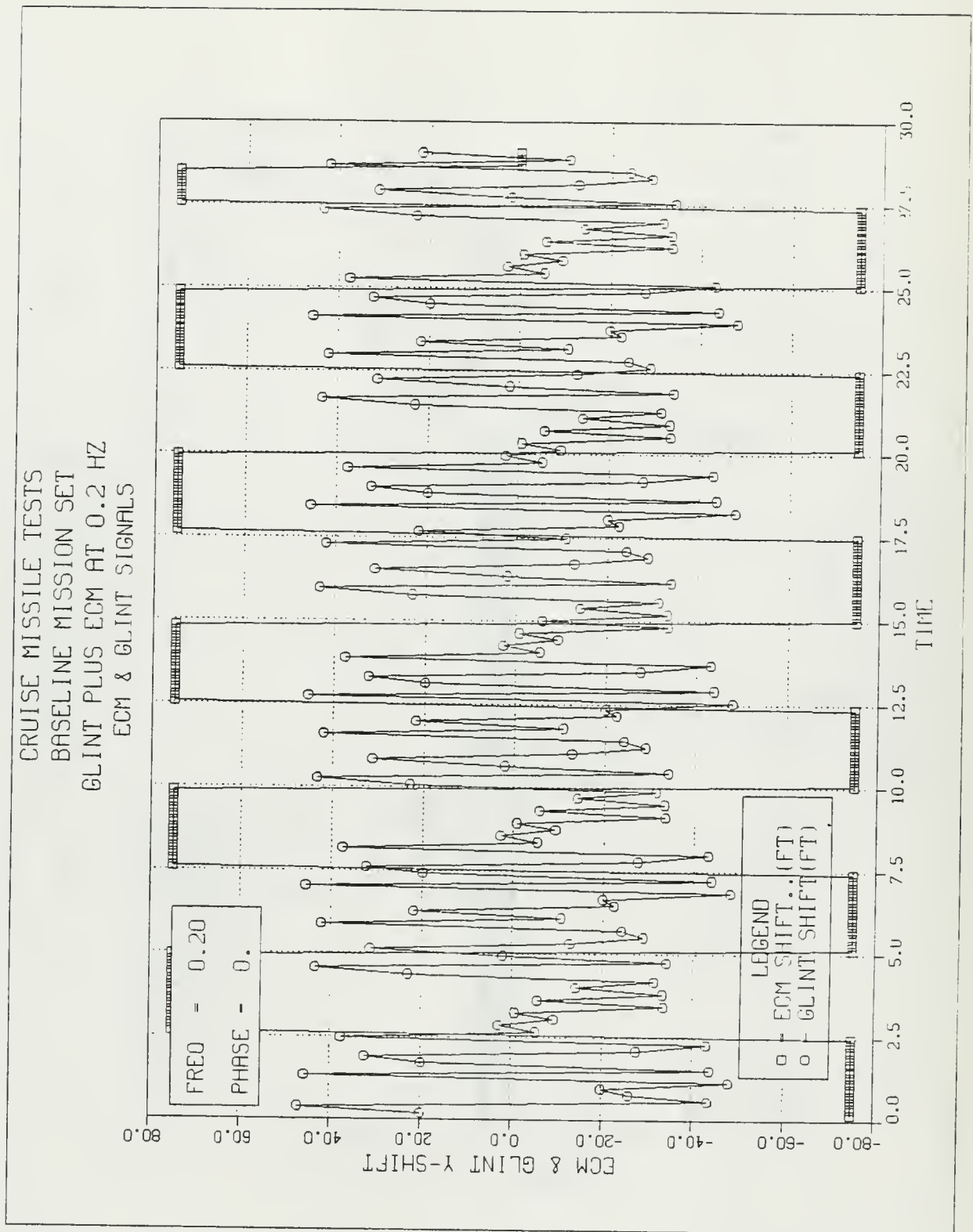


Figure A.33 Baseline with GLINT & ECM - ECM & GLINT.

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ALTITUDE CONTROL

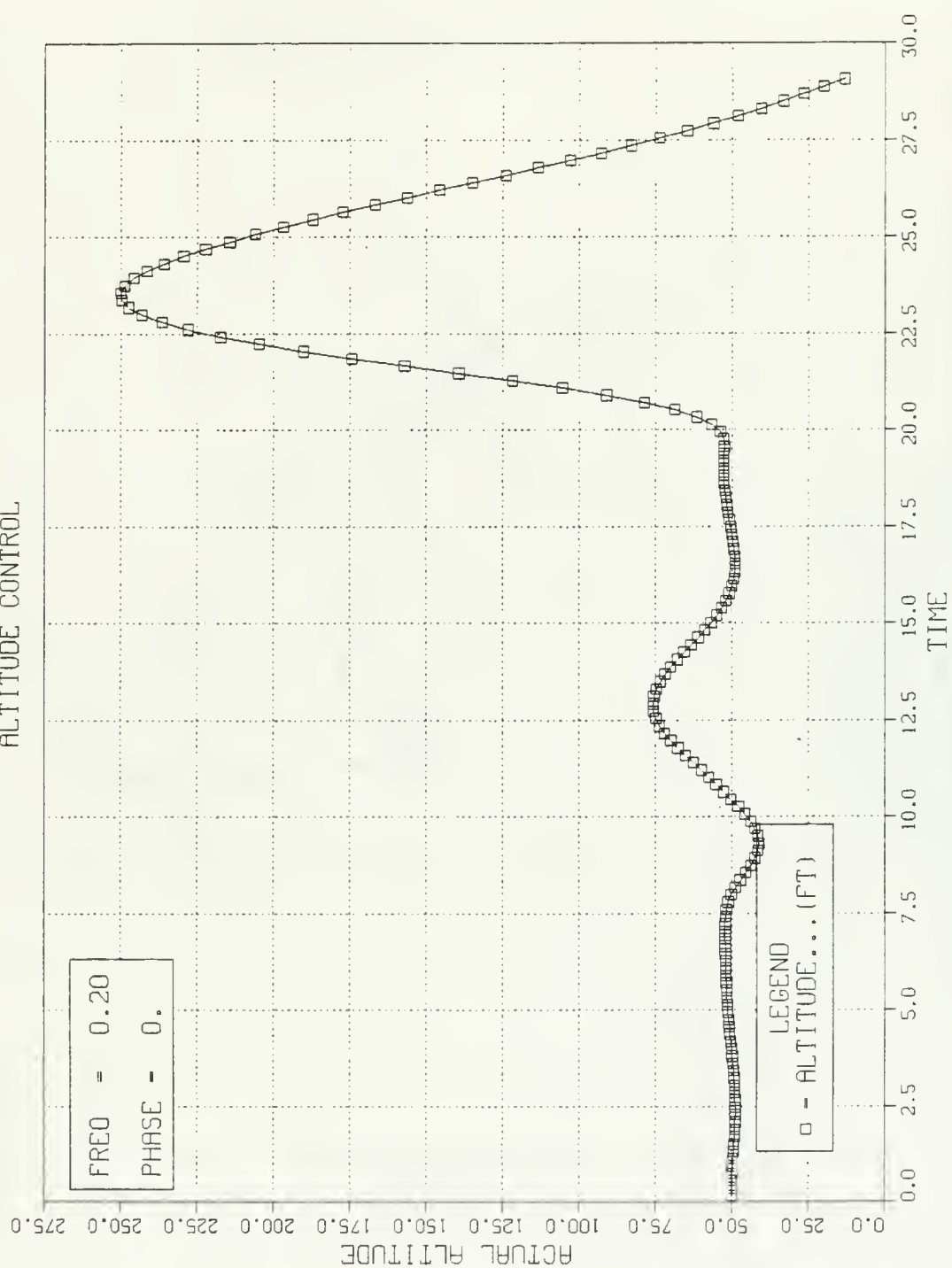


Figure A.34 Baseline with GLINT & ECM - Altitude.

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 GEOGRAPHICAL TRACKS

FREQ	=	0.20
PHASE	=	0.



Figure A.35 Baseline with GLINT & ECM - Geo Plot.

BASELINE SCAN RESULTS

MISS DISTANCES

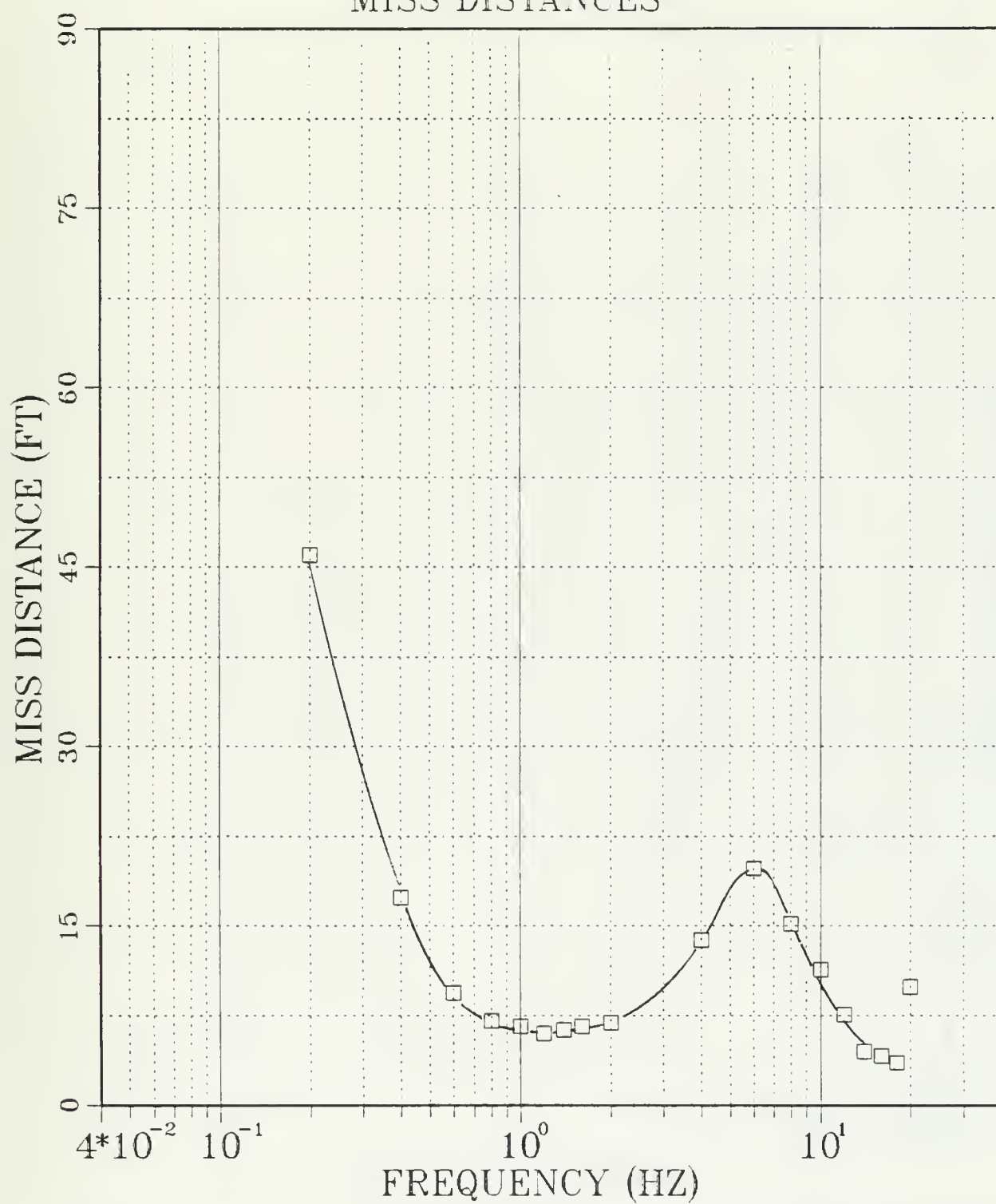


Figure A.36 Mean Miss Distances - Baseline.

CONFIGURATION II SCANS

MISS DISTANCES

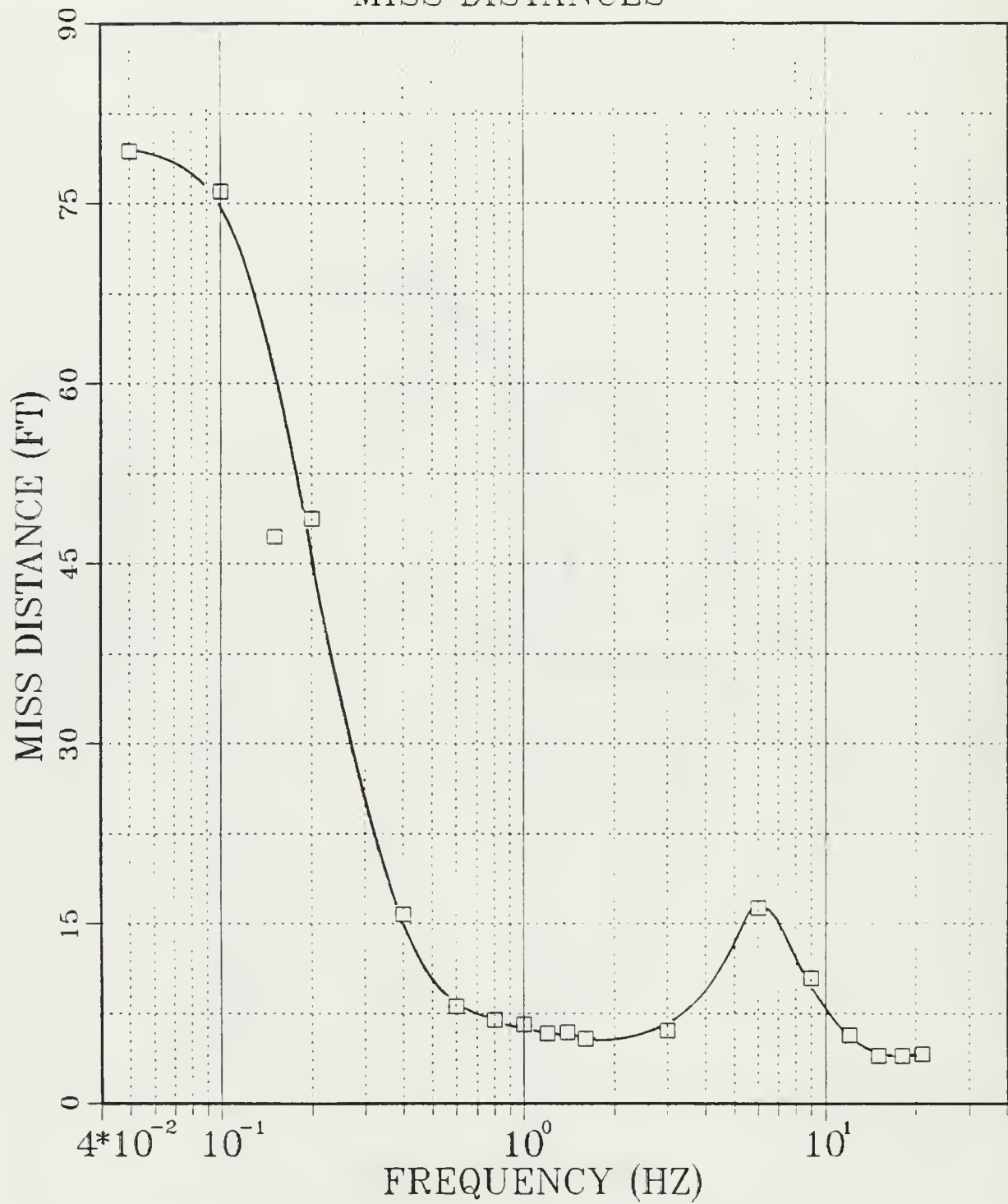


Figure A.37 Mean Miss Distances - Configuration II.

CONFIGURATION III SCANS

MISS DISTANCES

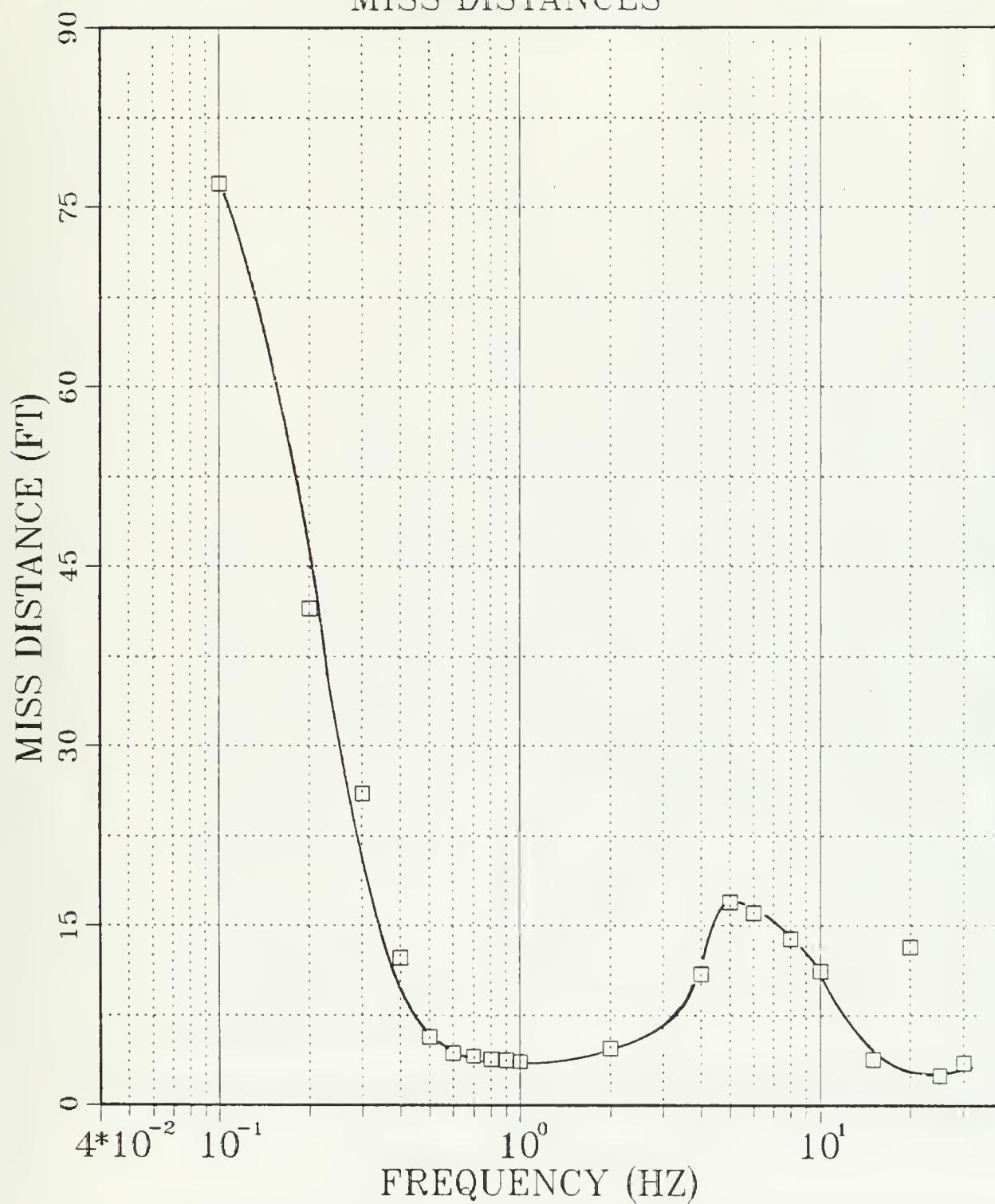


Figure A.38 Mean Miss Distances - Configuration III.

CONFIGURATION IV SCANS

MISS DISTANCES

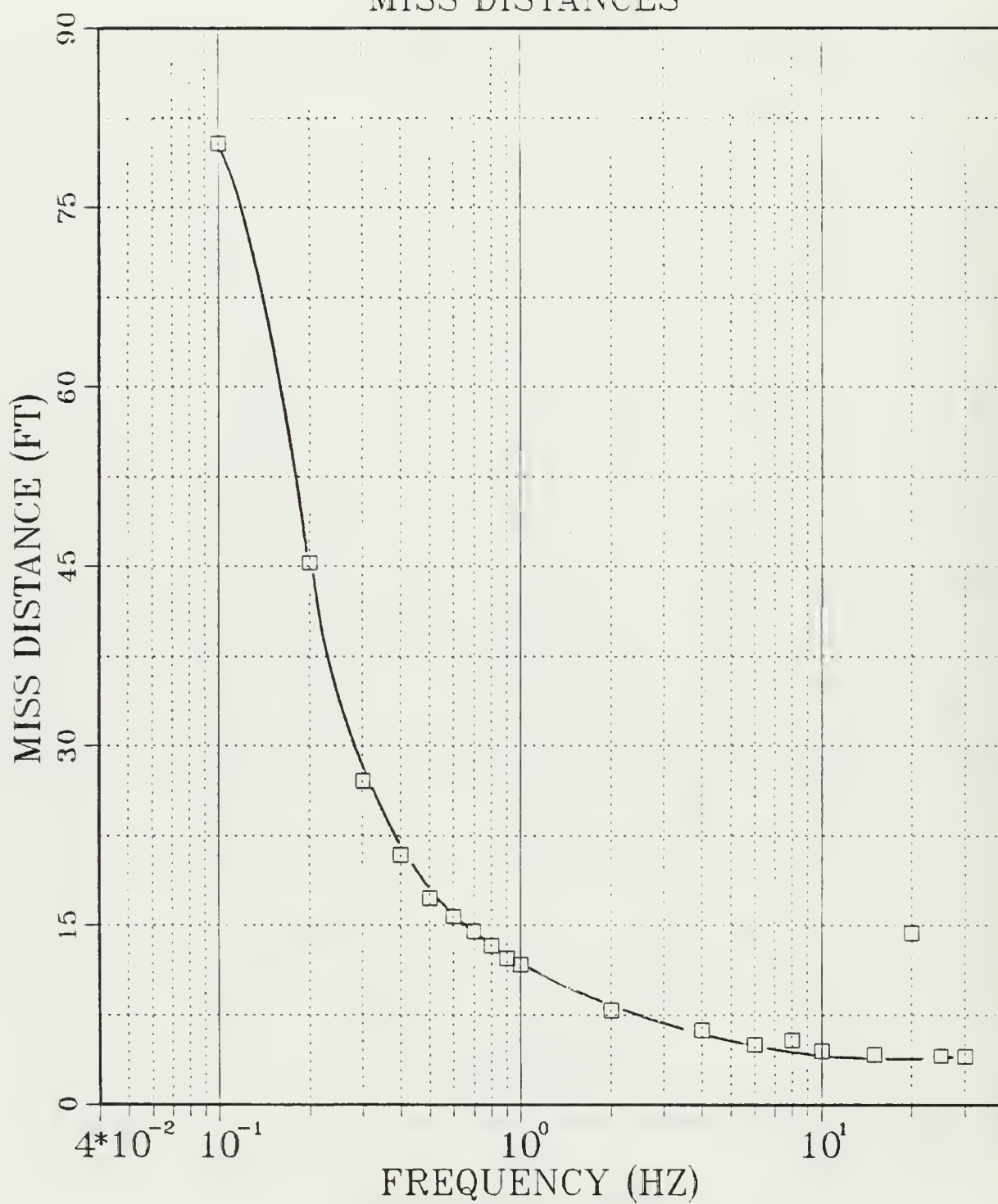


Figure A.39 Mean Miss Distances - Configuration IV.

BASELINE SCAN RESULTS

AUTOPILOT ERRORS

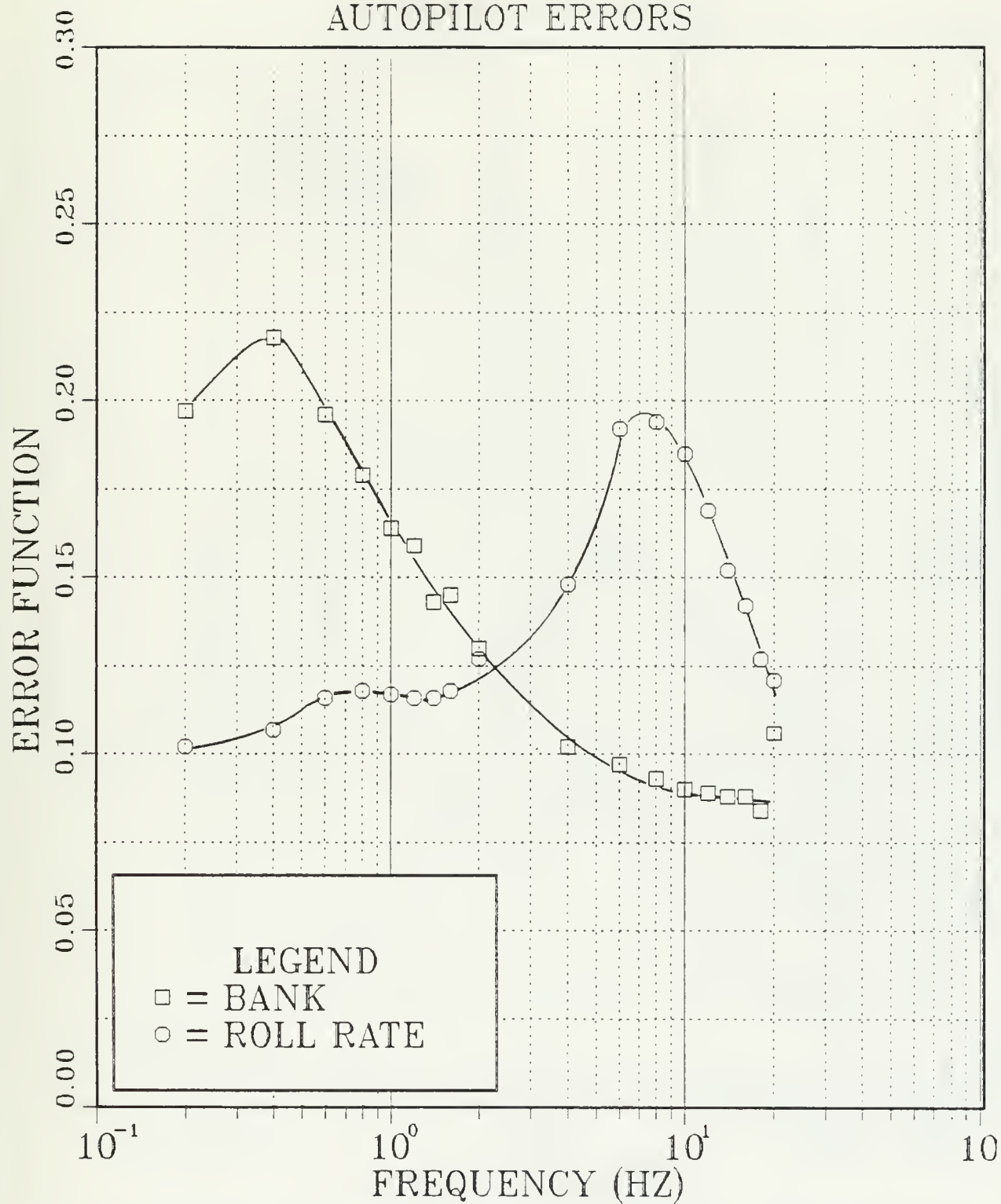


Figure A.40 Autopilot Errors - Baseline.

CONFIGURATION II SCANS

AUTOPILOT ERRORS



Figure A.41 Autopilot Errors - Configuration II.

CONFIGURATION III SCANS

AUTOPILOT ERRORS

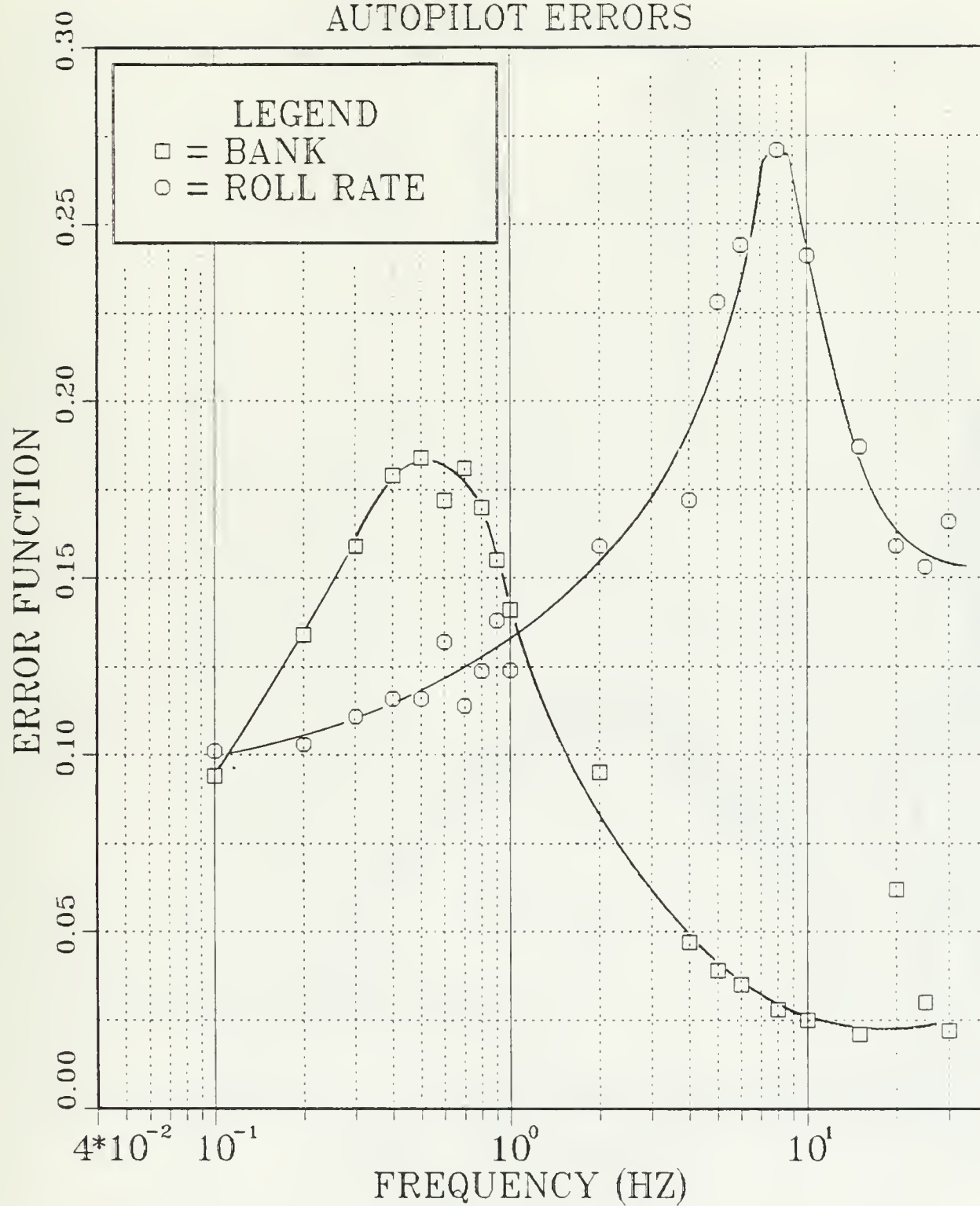


Figure A.42 Autopilot Errors - Configuration III.

CONFIGURATION IV SCANS

AUTOPILOT ERRORS

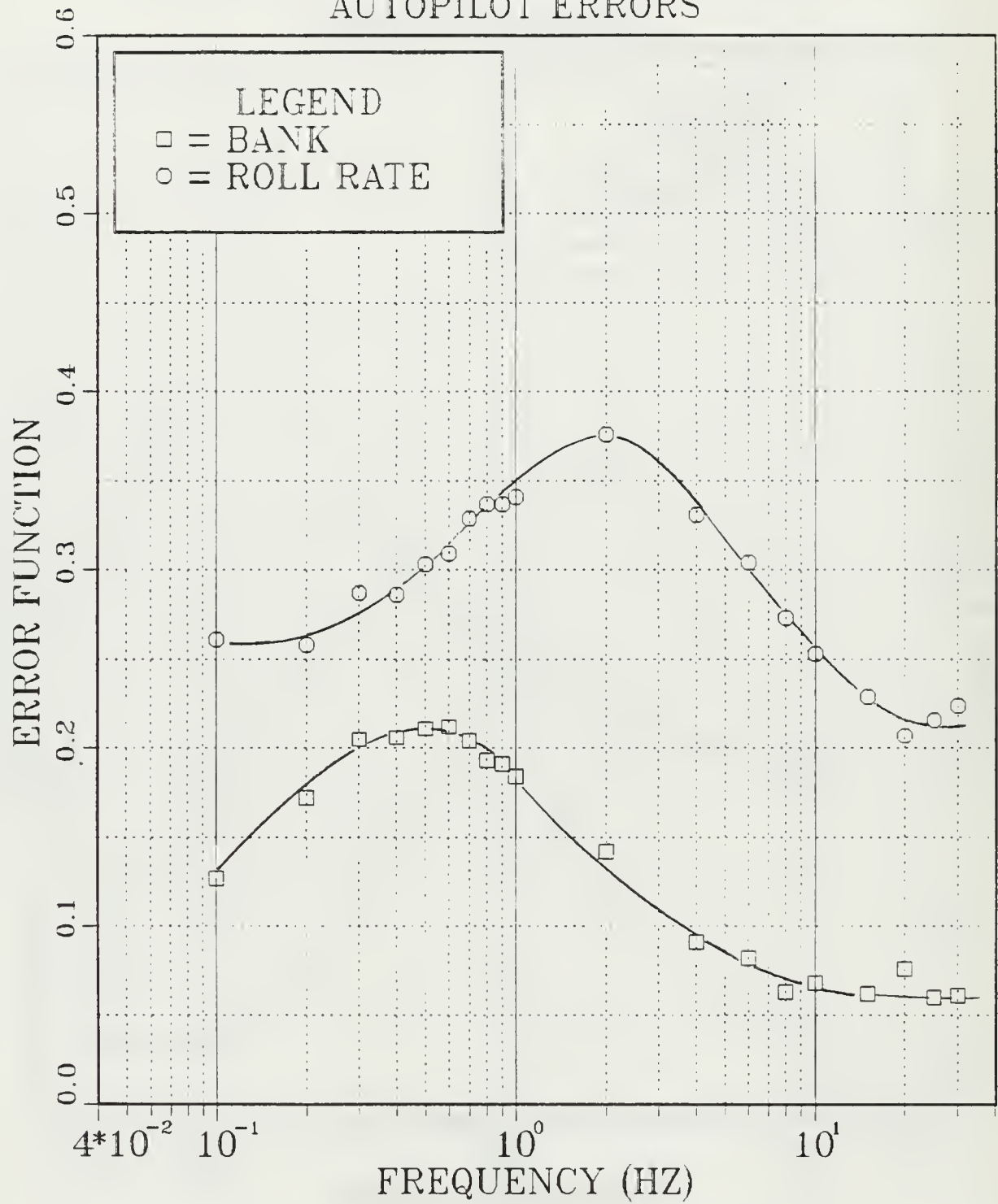


Figure A.43 Autopilot Errors - Configuration IV.

BASELINE SCAN RESULTS

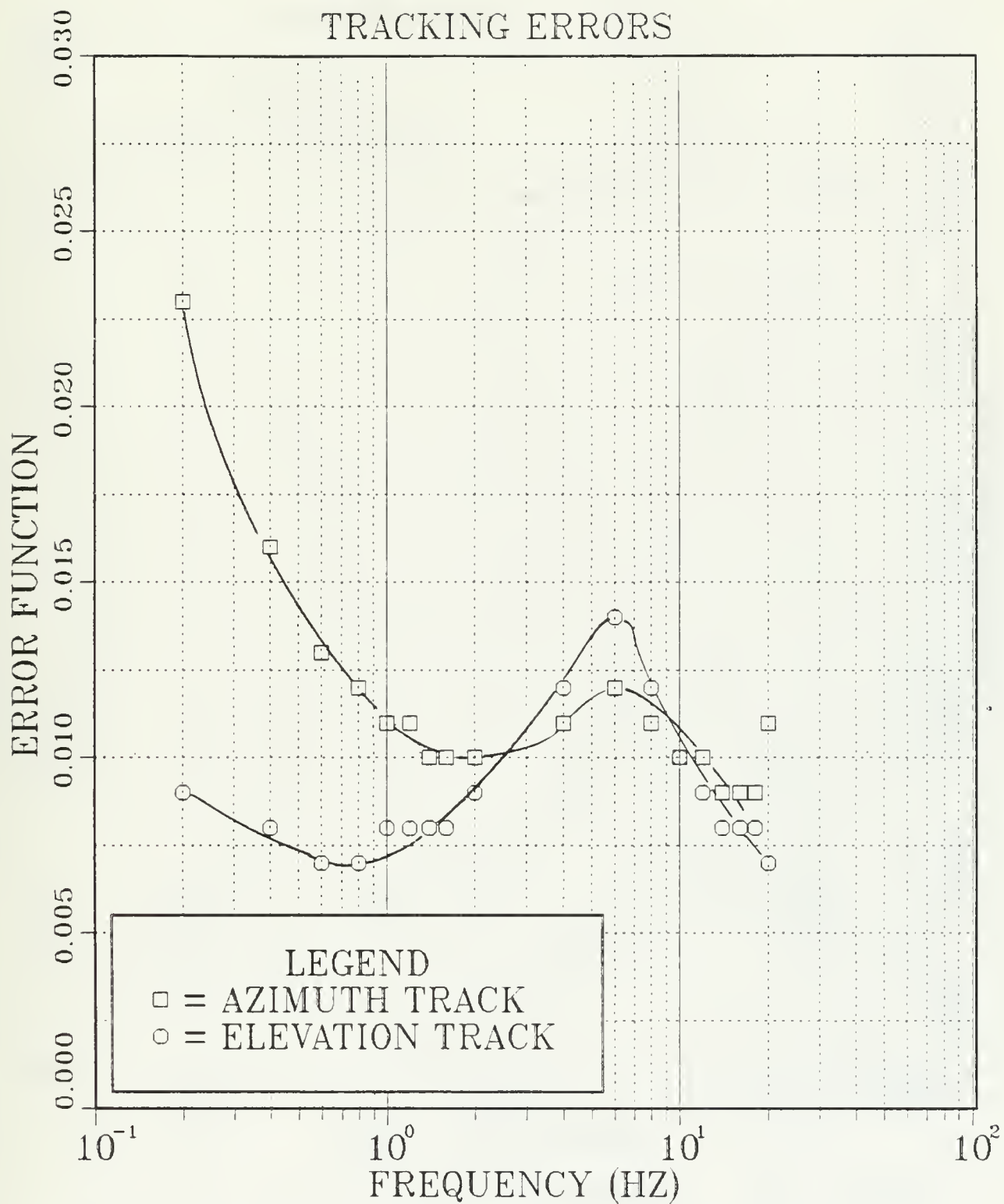


Figure A.44 Tracking Errors - Baseline.

CONFIGURATION II SCANS

TRACKING ERRORS

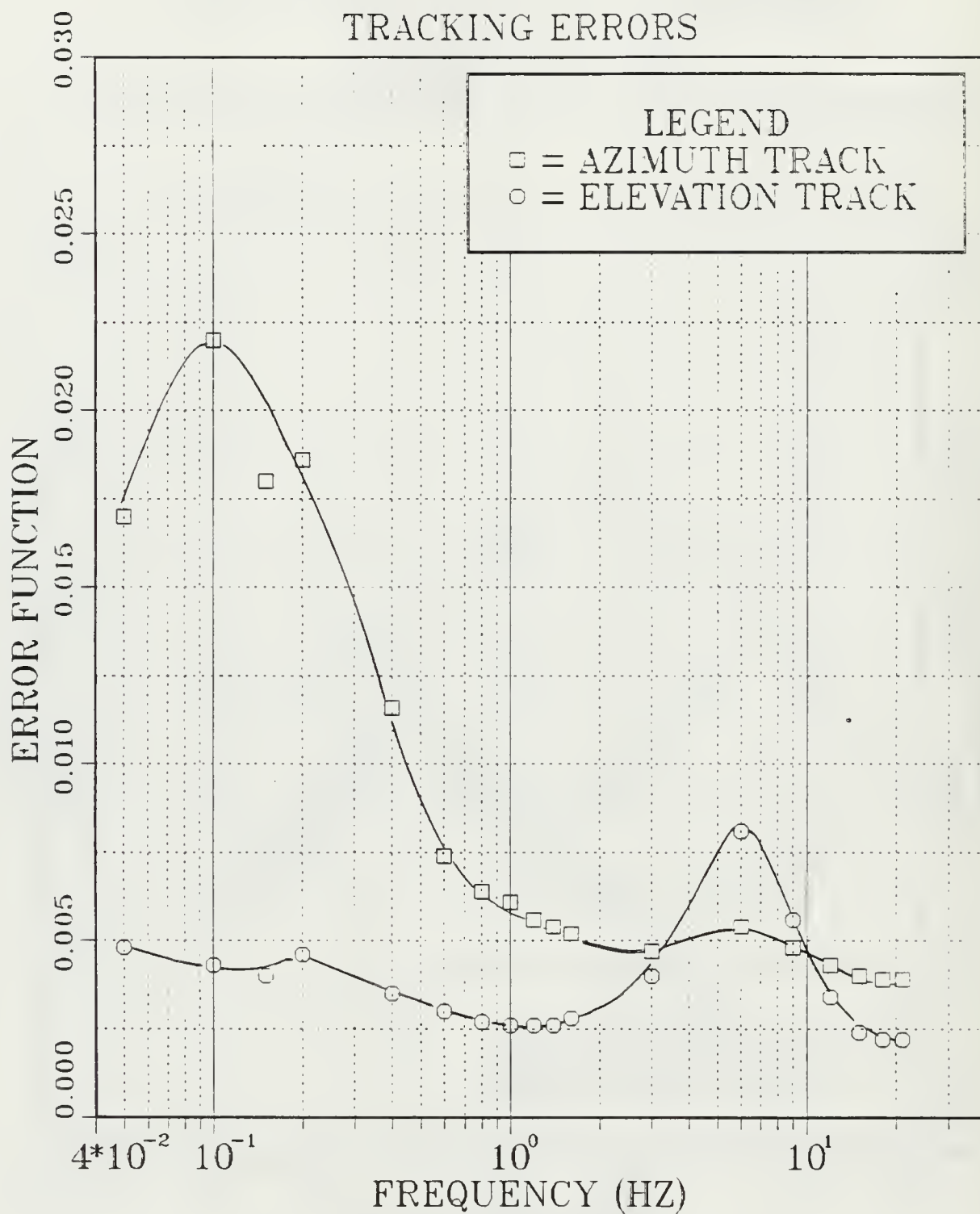


Figure A.45 Tracking Errors - Configuration II.

CONFIGURATION III SCANS

TRACKING ERRORS

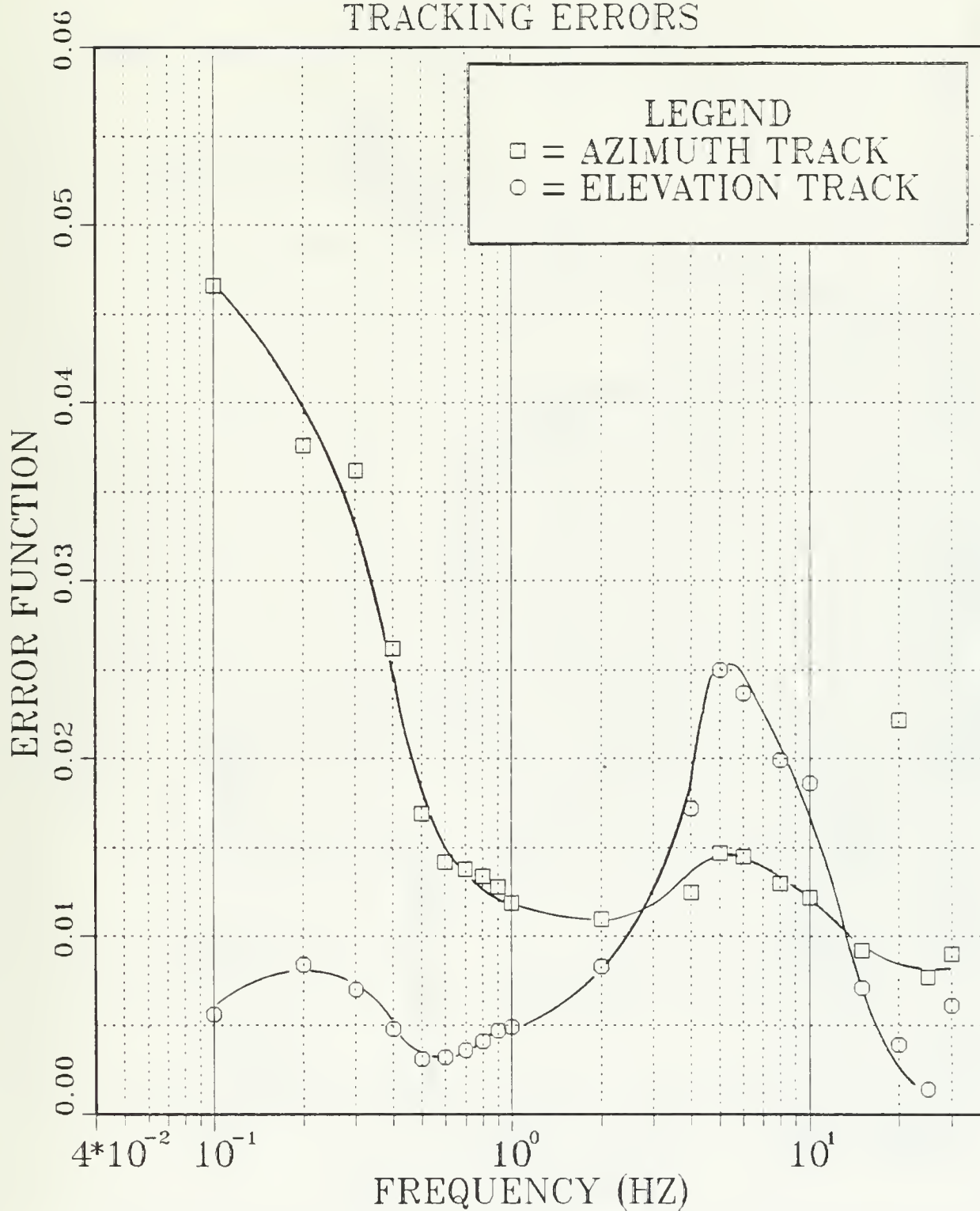


Figure A.46 Tracking Errors - Configuration III.

CONFIGURATION IV SCANS

TRACKING ERRORS

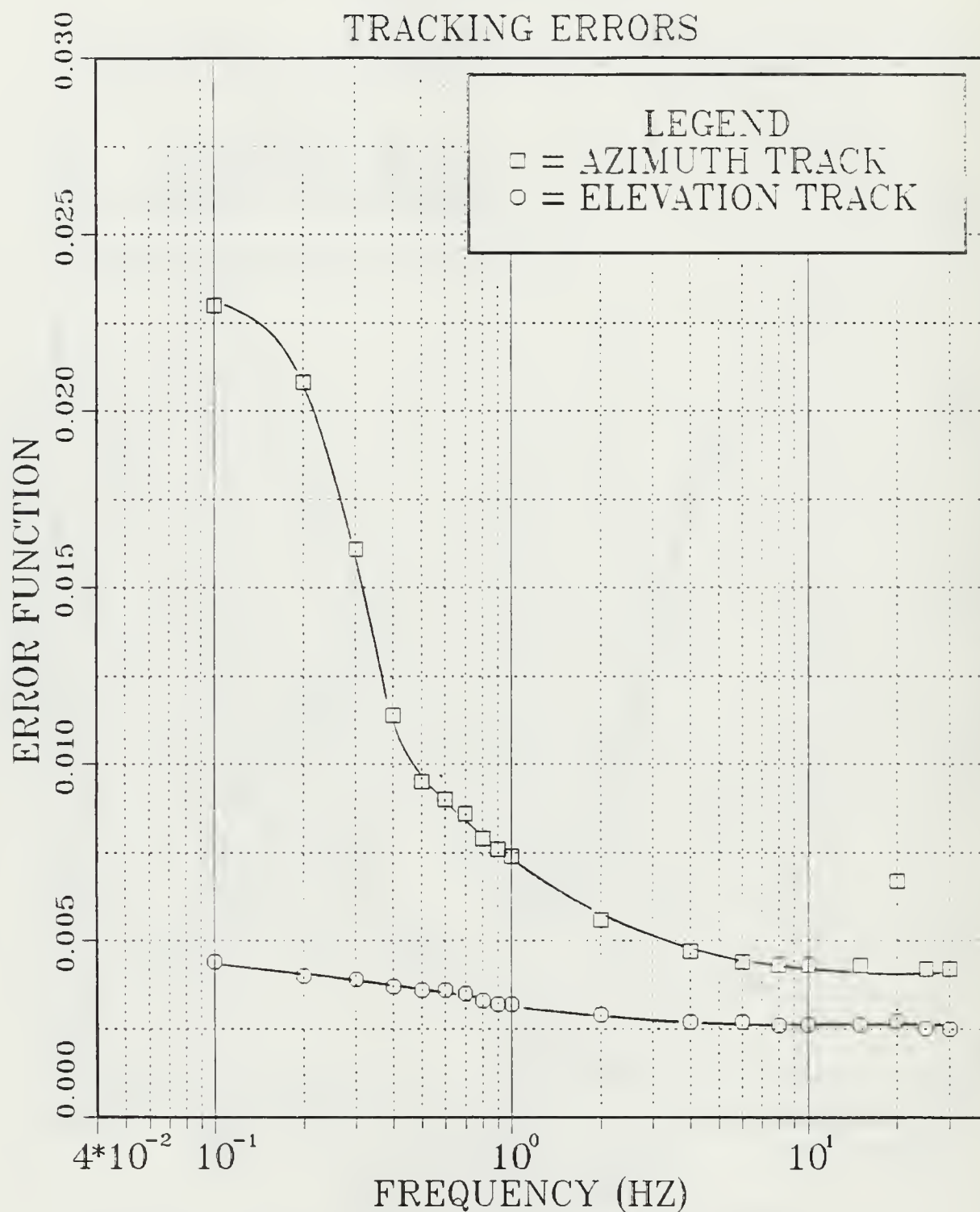


Figure A.47 Tracking Errors - Configuration IV.

CRUISE MISSILE TESTS
 BASELINE POPOUT ATTACK-NO GLNT
 LO-FREQUENCY SCAN 0.2-1.6 HZ
 BANK ANGLE CONTROL

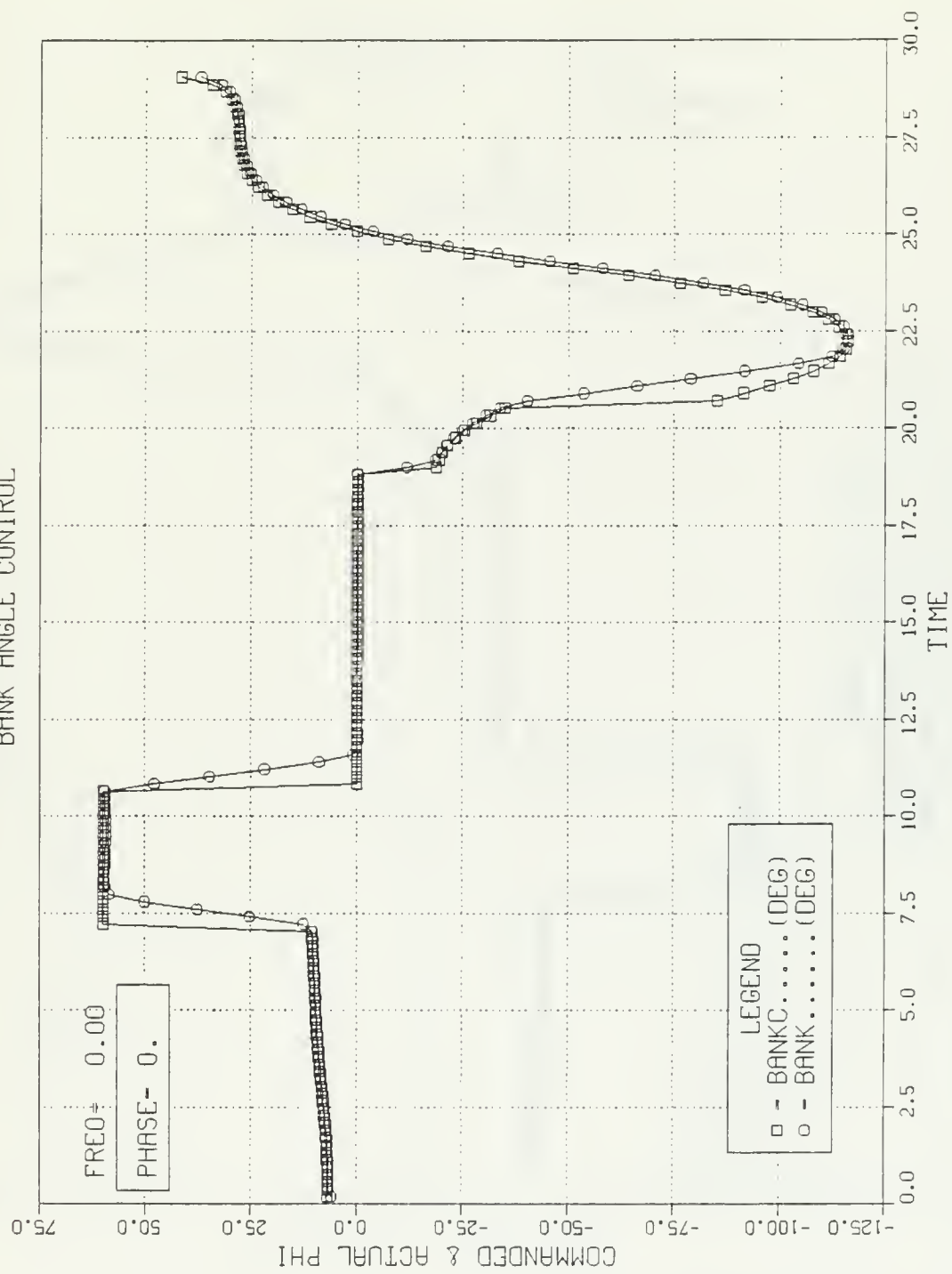


Figure A.48 Baseline/ECM Freq = 0.0 Hz - Bank.

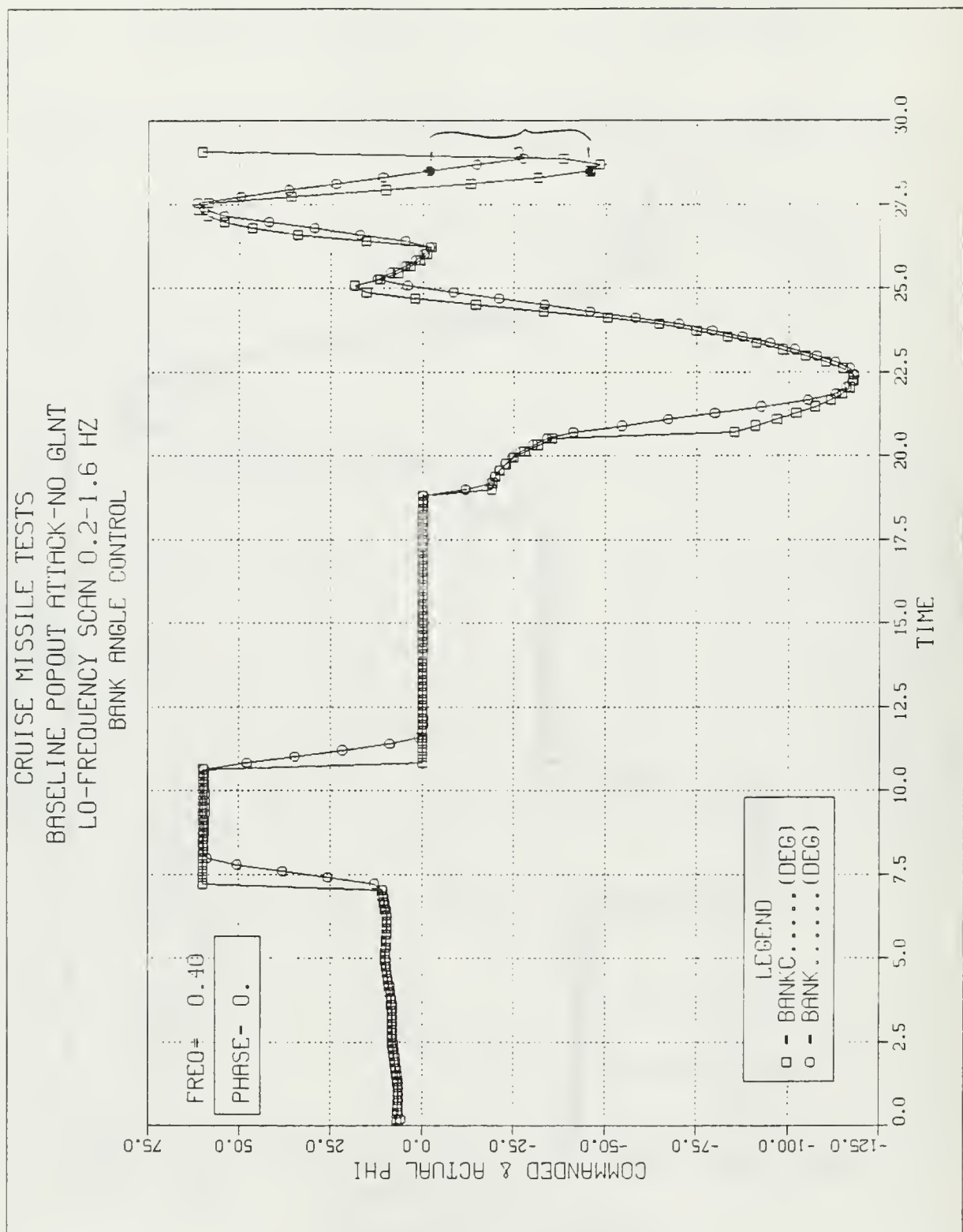


Figure A.49 Baseline/ECM Freq = 0.4 Hz - Bank.

CRUISE MISSILE TESTS
 BASELINE POPOUT ATTACK-NO GLNT
 HI-FREQUENCY SCAN 0.0-20. HZ
 BANK ANGLE CONTROL

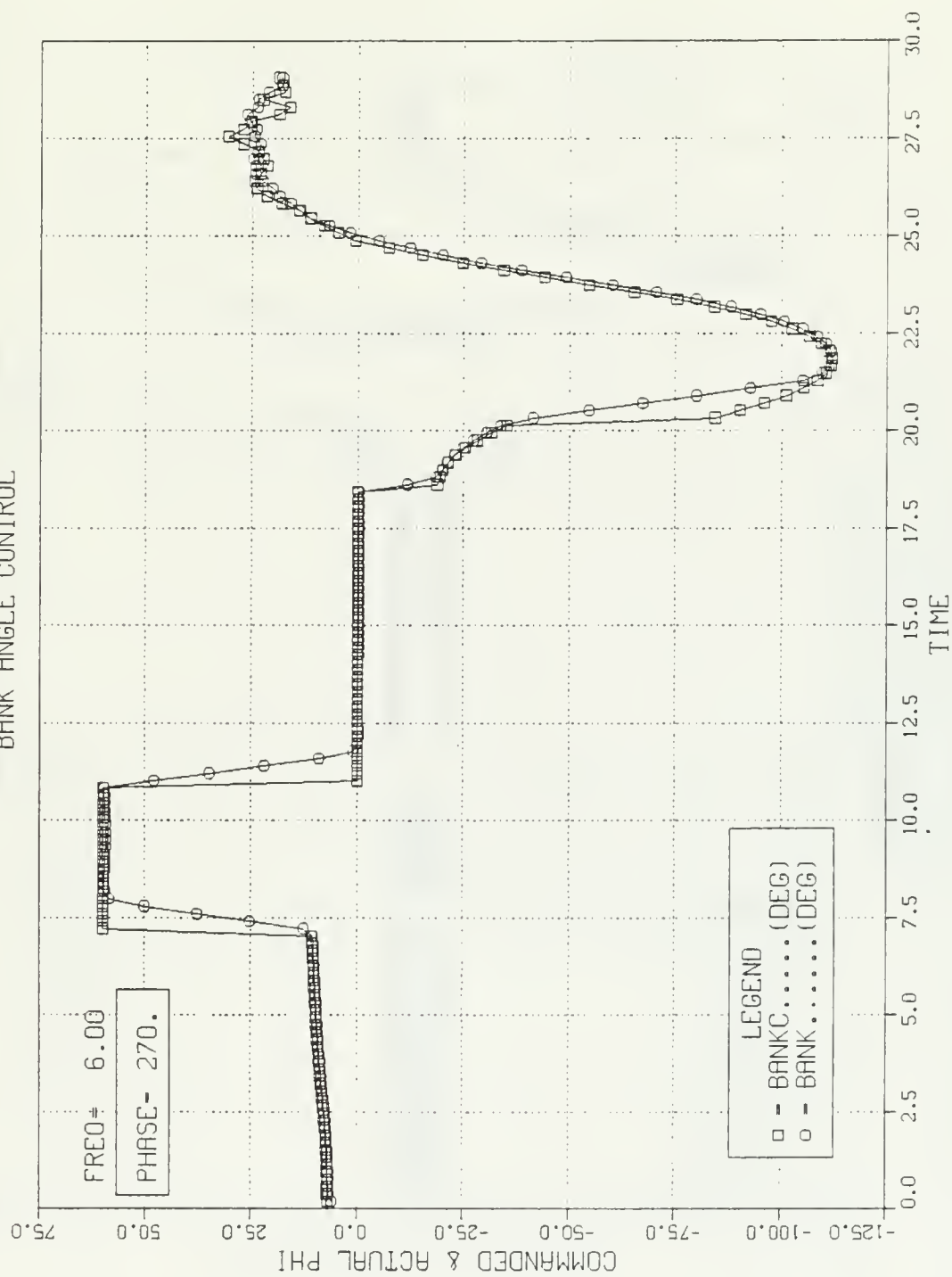


Figure A.50 Baseline/ECM Freq = 6.0 Hz - Bank.

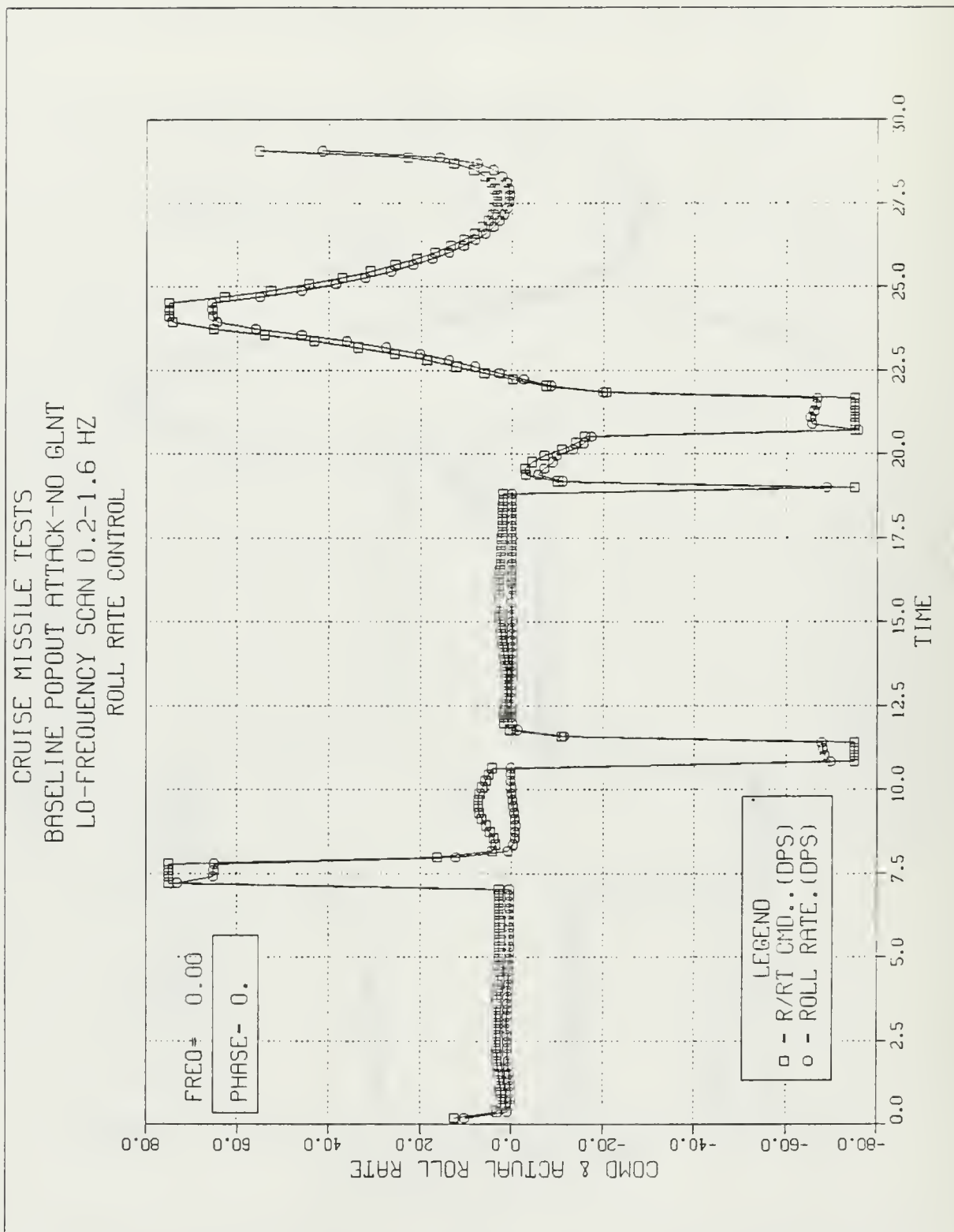


Figure A.51 Baseline/ECM Freq = 0.0 Hz - Roll Fate.

CRUISE MISSILE TESTS
 BASELINE POPOUT ATTACK-NO GLNT
 LO-FREQUENCY SCAN 0.2-1.6 HZ
 ROLL RATE CONTROL

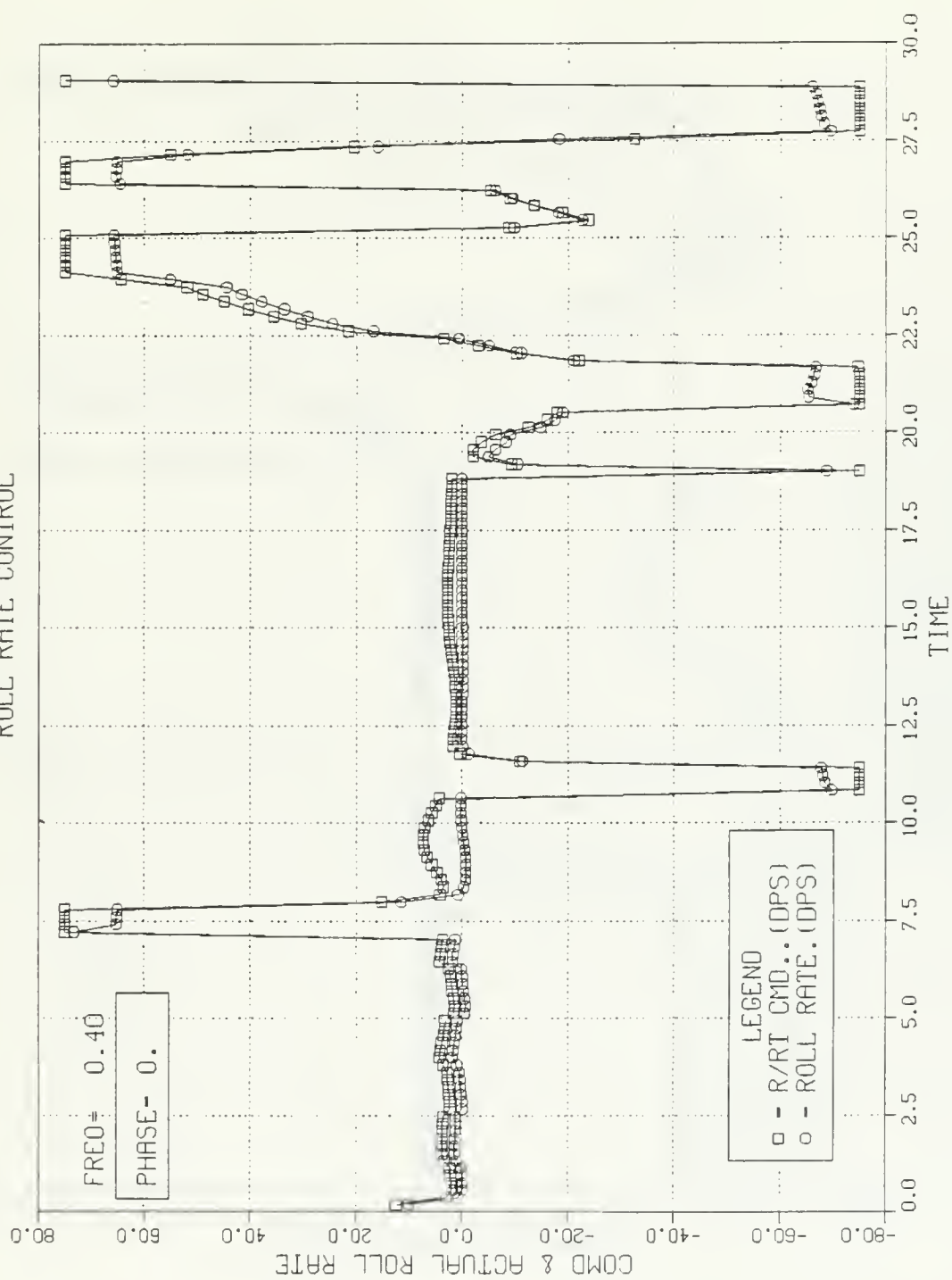


Figure A.52 Baseline/ECM Freq = 0.4 Hz - Roll Rate.

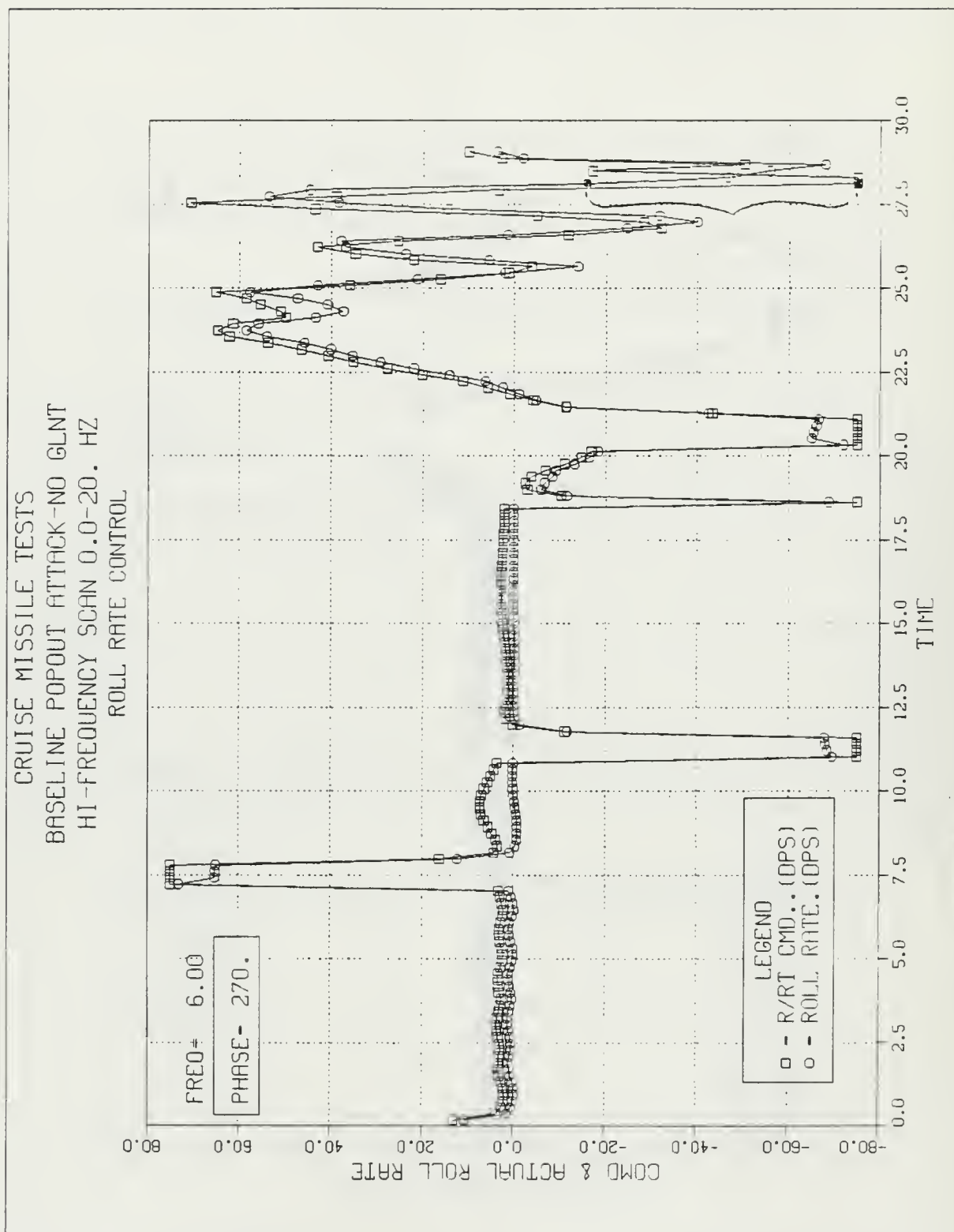


Figure A.53 Baseline/ECM Freq = 6.0 Hz - Roll Rate.

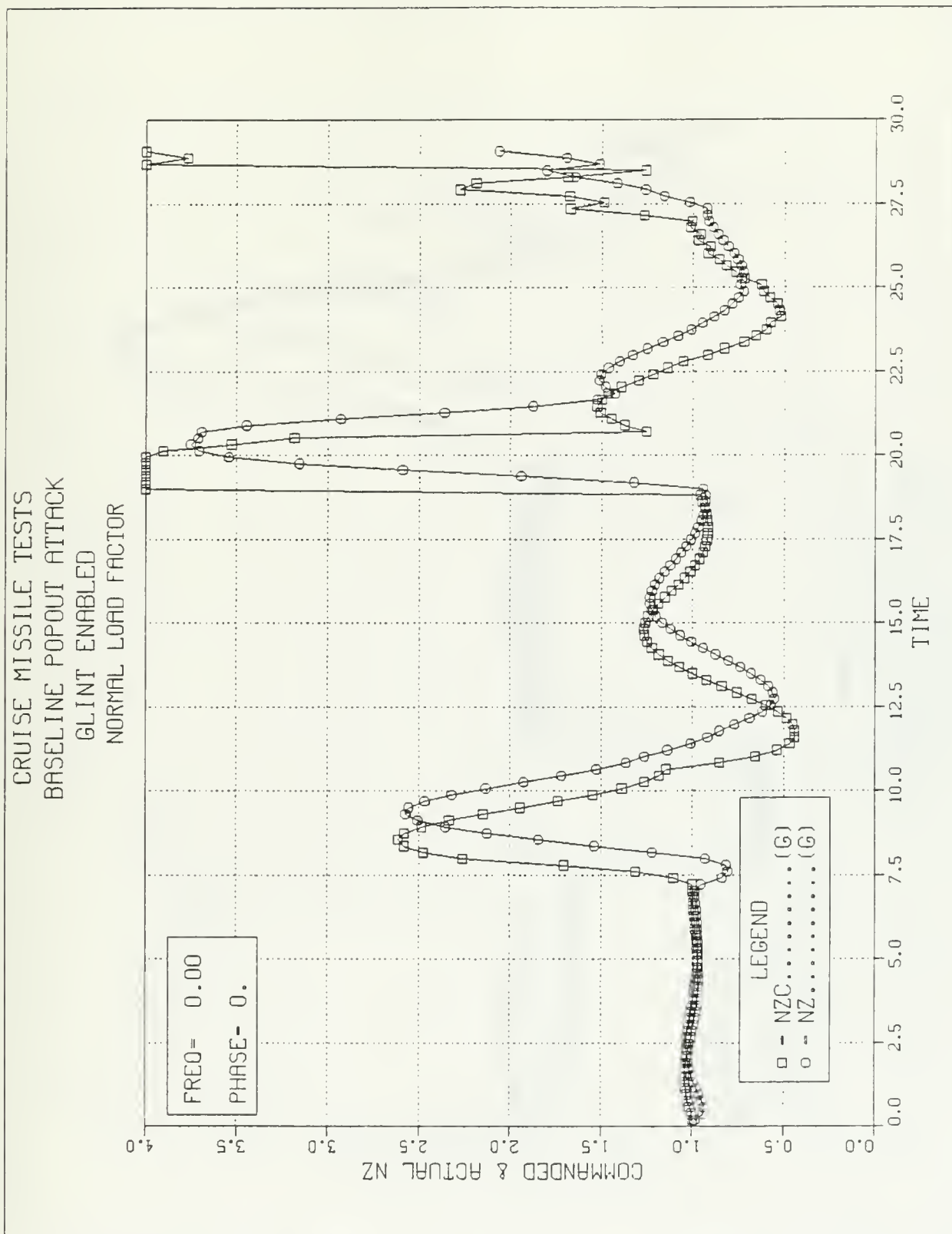


Figure A.54 Baseline with GLINT only - Load Factor.

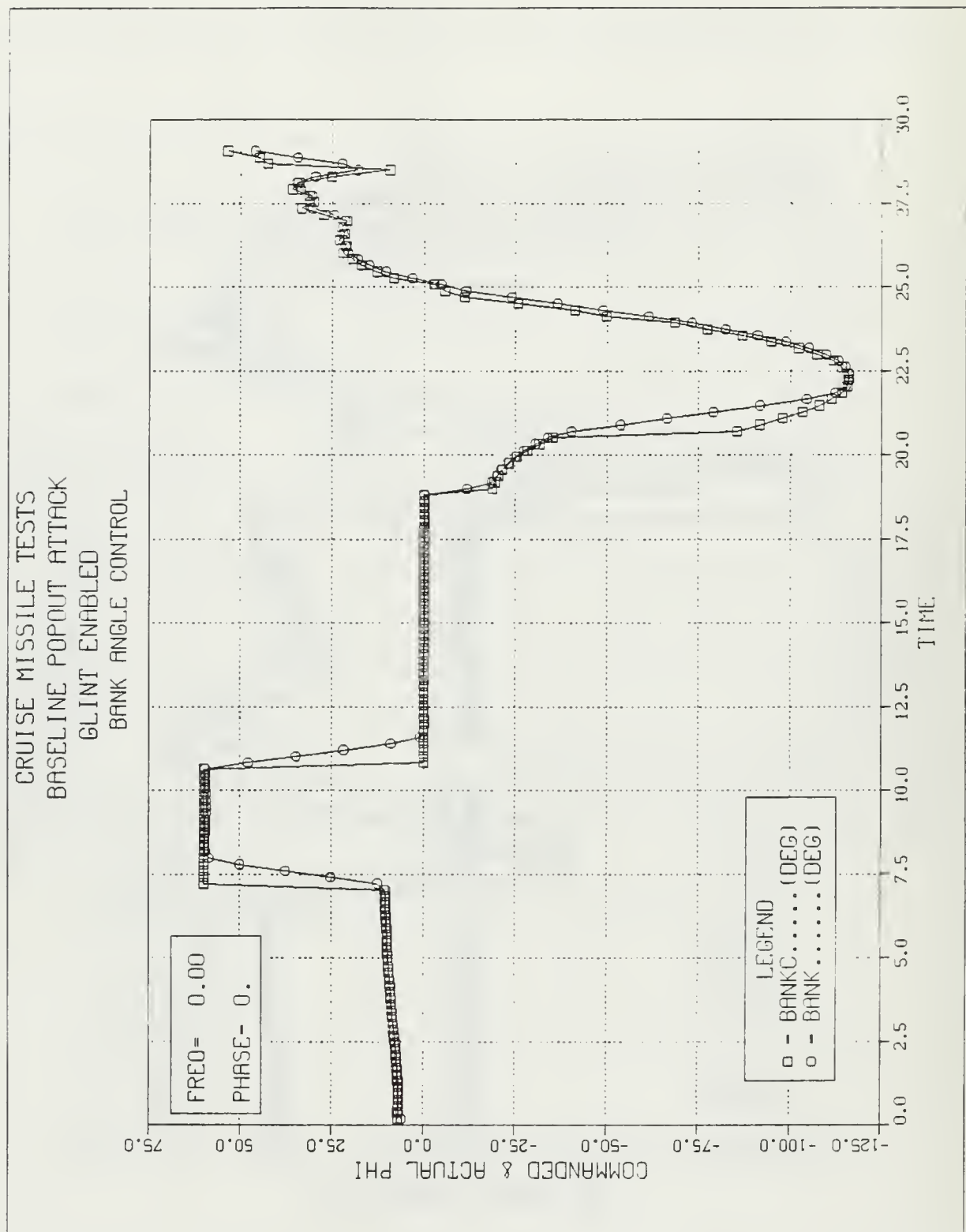


Figure A.55 Baseline with GLINT only - Bank.

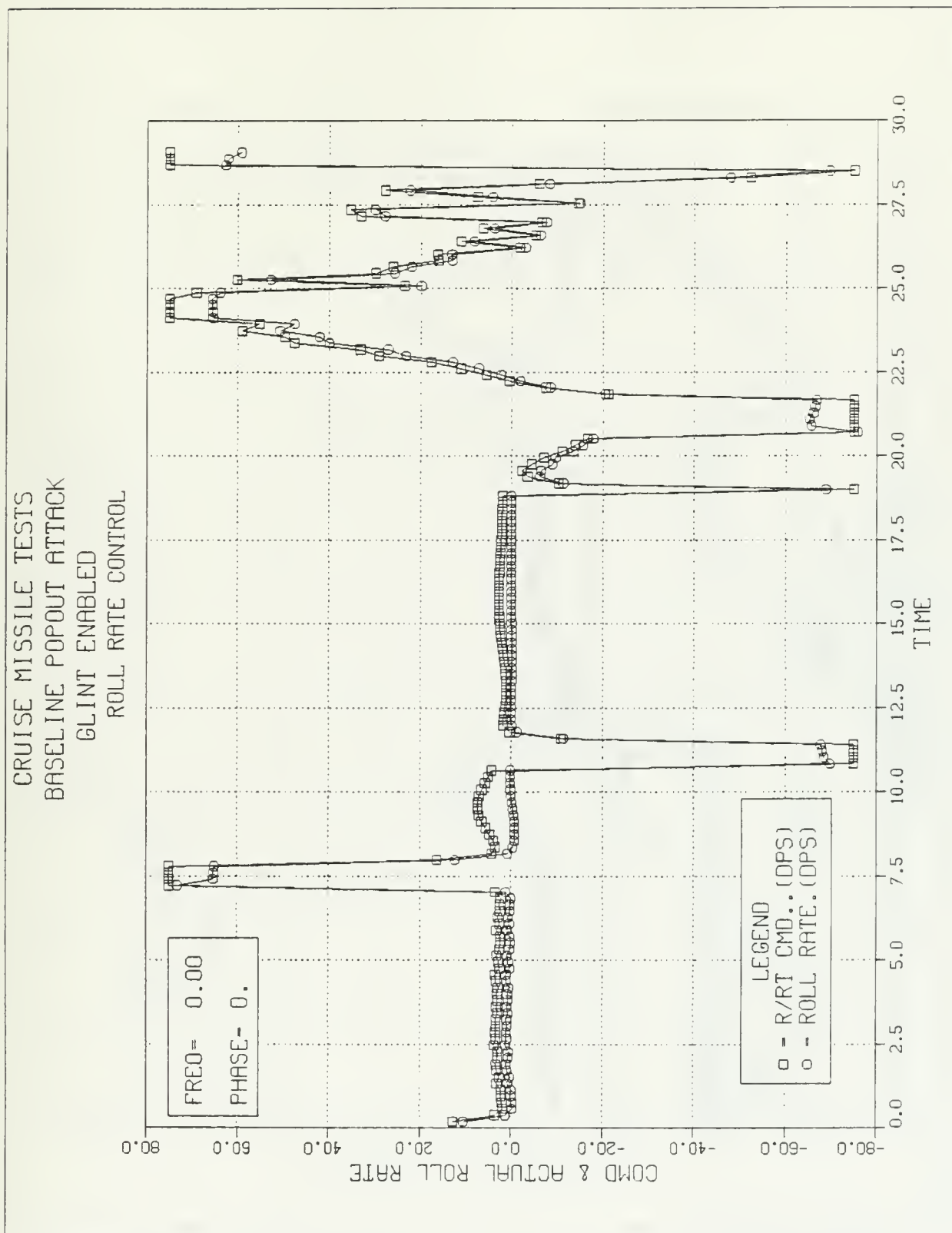


Figure A.56 Baseline with GLINT only - Roll Rate.

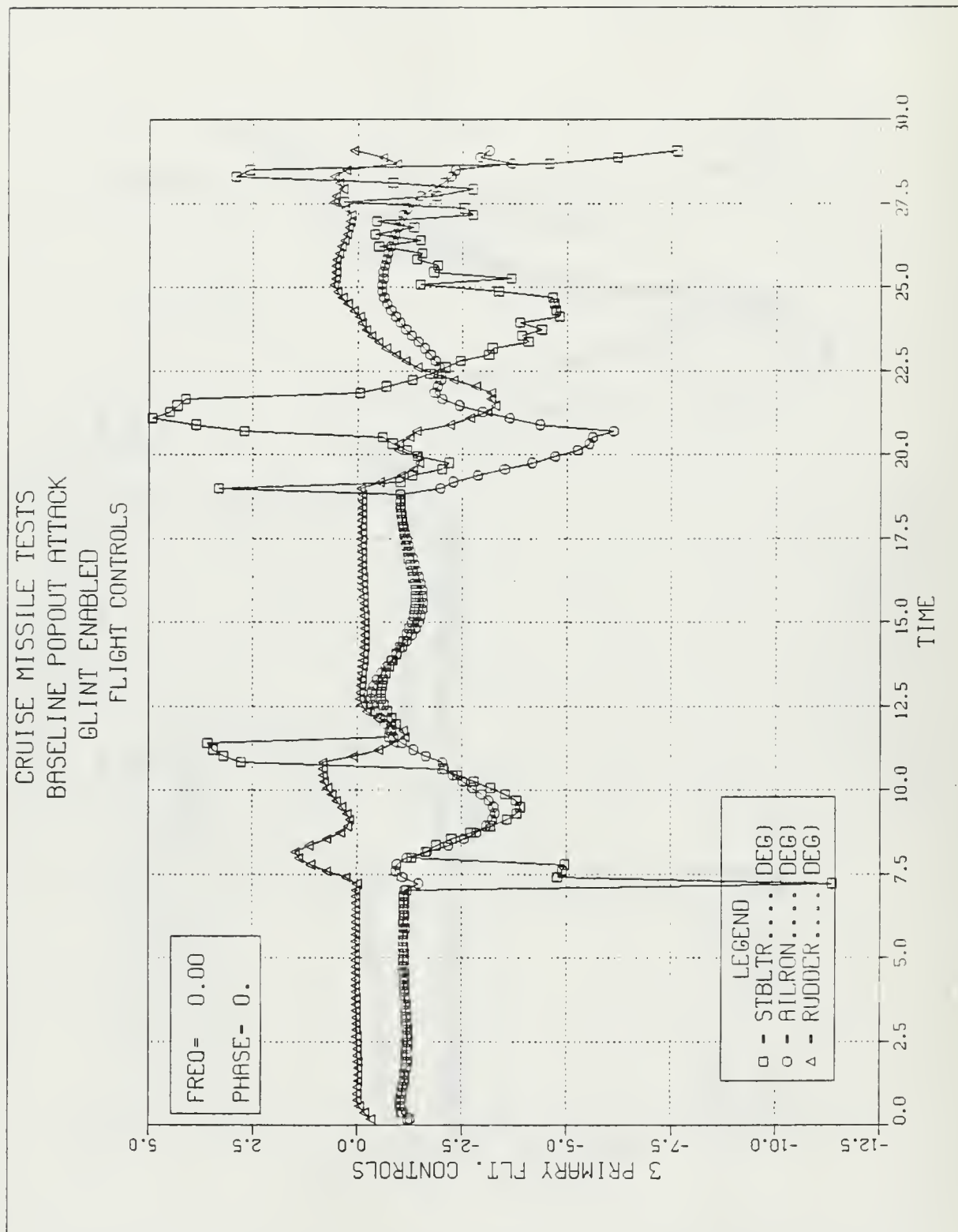


Figure A.57 Baseline with GLINT only - Controls.

CRUISE MISSILE TESTS
 CONFIGURATION II MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 NORMAL LOAD FACTOR

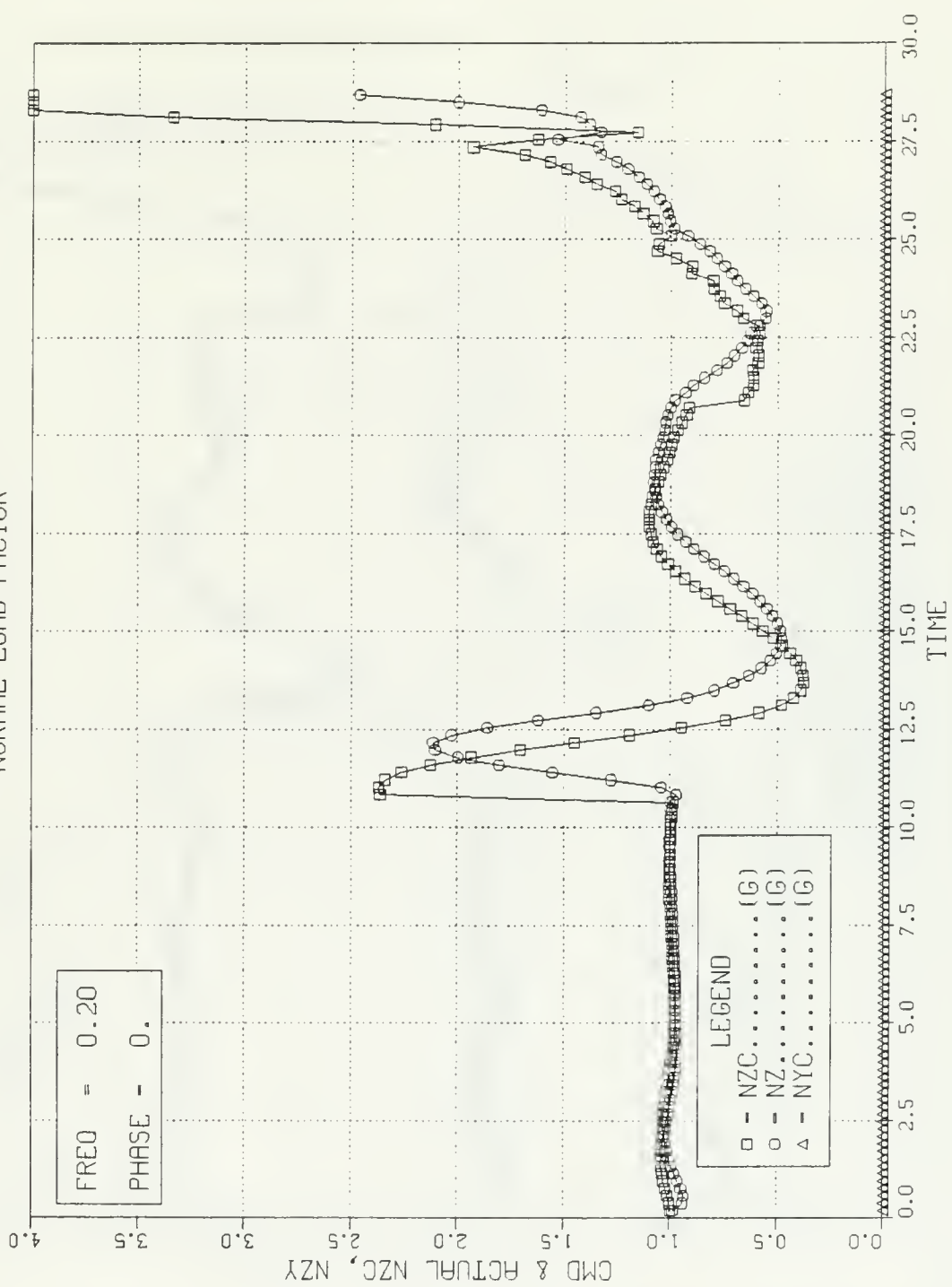


Figure A.58 Conf. II Mission Set - Load Factor.

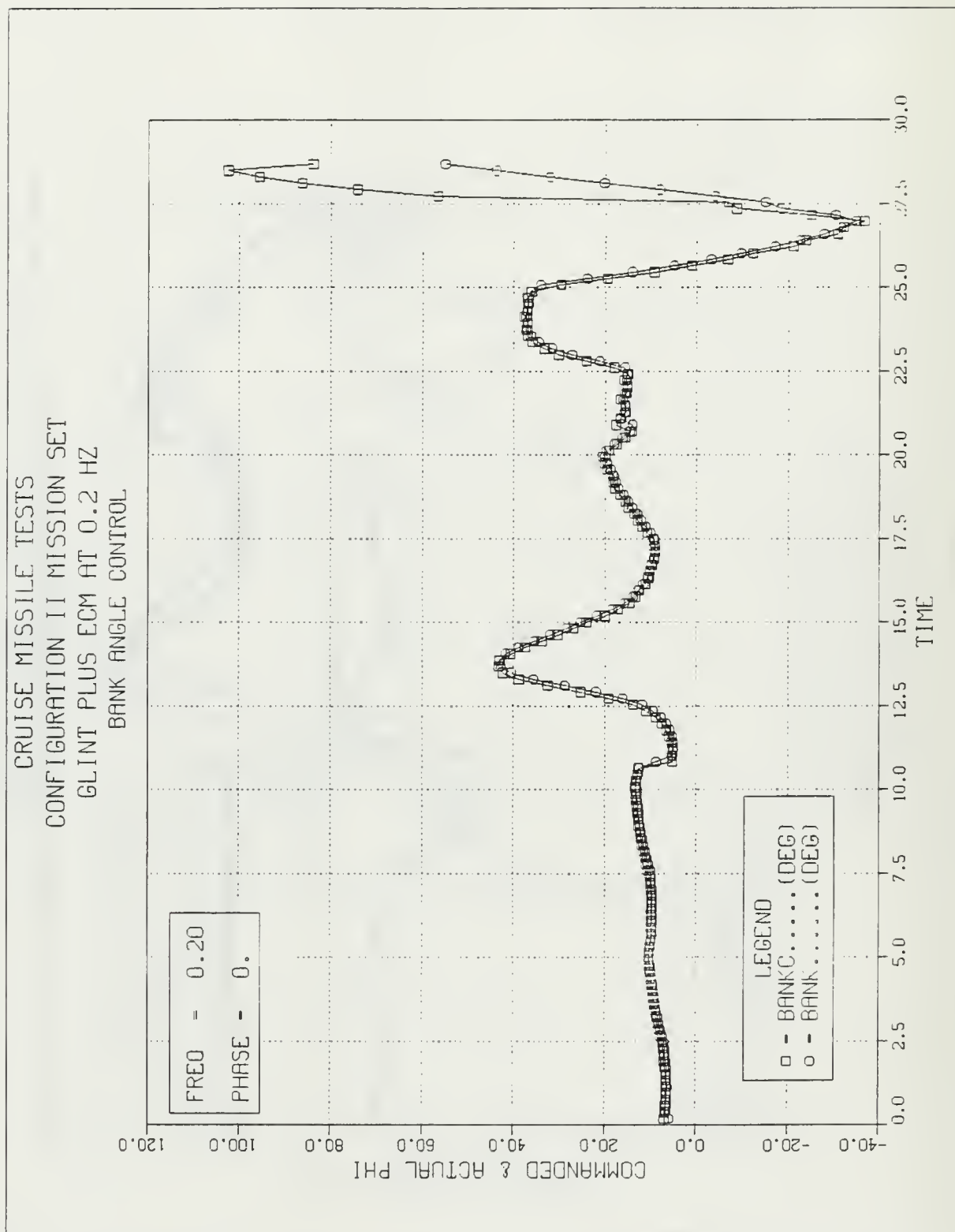


Figure A.59 Conf. II Mission Set - Bank.

CRUISE MISSILE TESTS
 CONFIGURATION II MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ROLL RATE CONTROL

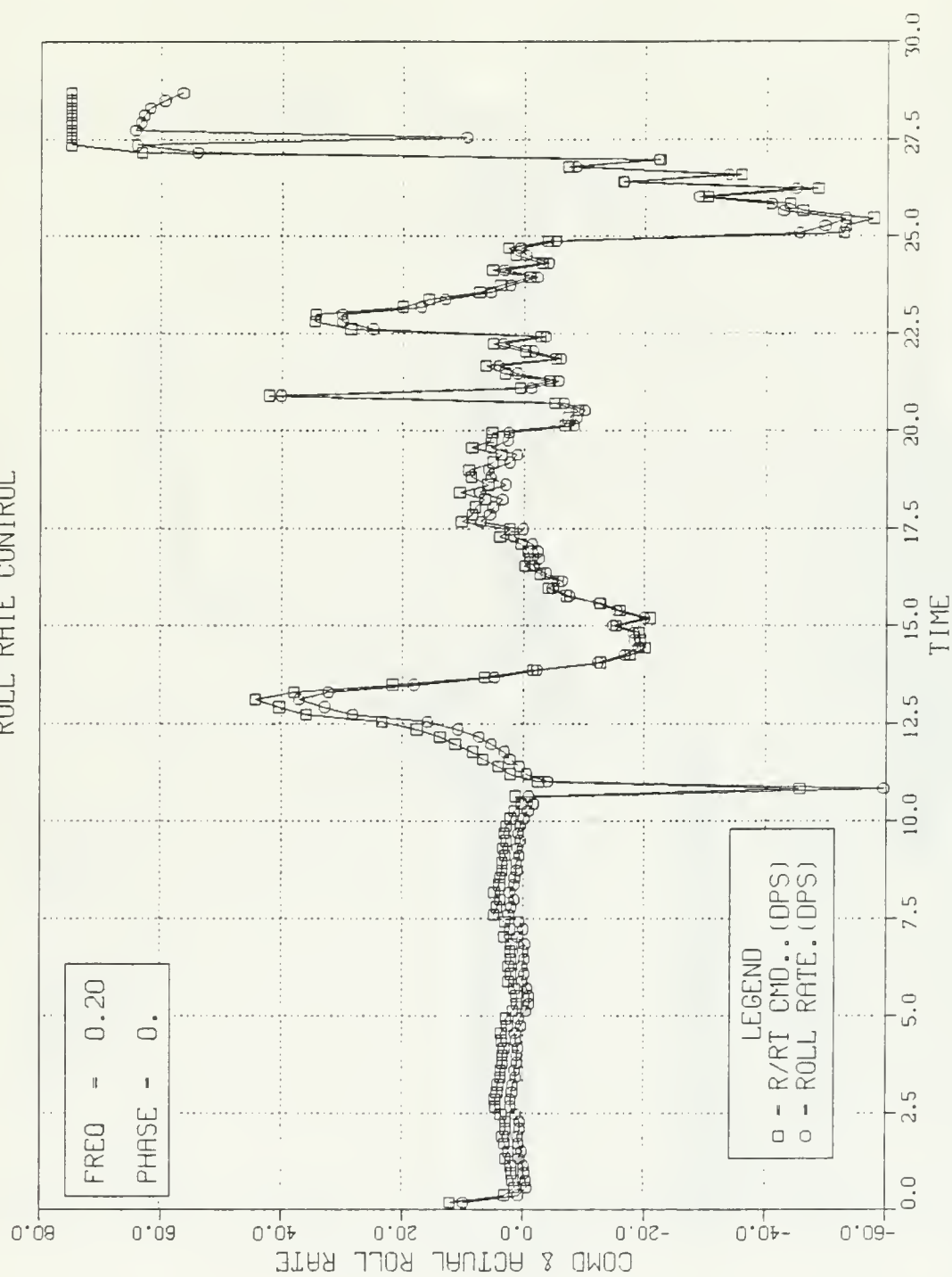


Figure A.60 Conf. II Mission Set - Roll Rate.

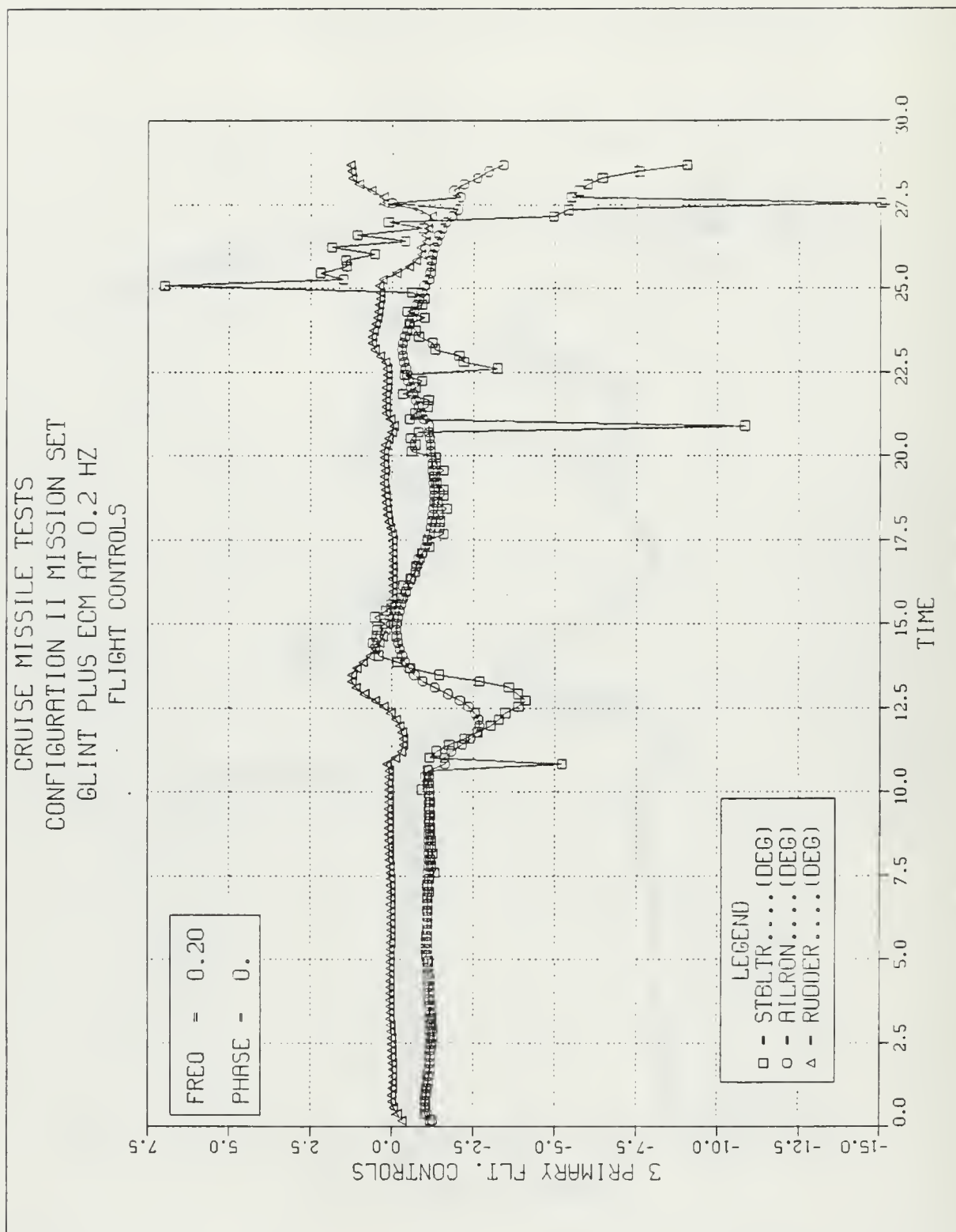


Figure A.61 Conf. II Mission Set - Controls.

CRUISE MISSILE TESTS
 CONFIGURATION II MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ALTITUDE CONTROL

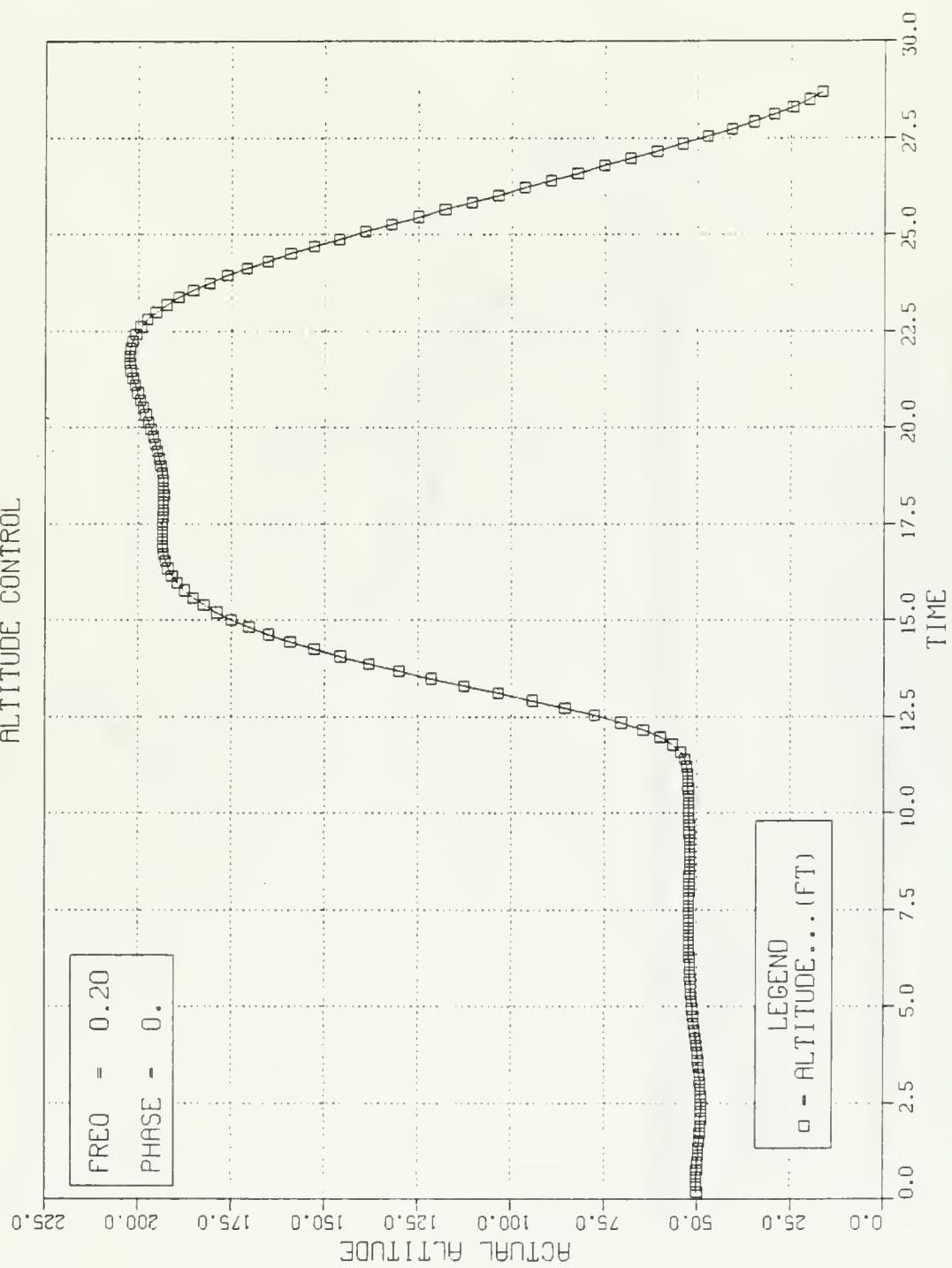


Figure A.62 Conf. II Mission Set - Altitude.

CRUISE MISSILE TESTS
 CONFIGURATION II MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 GEOGRAPHICAL TRACKS

FREQ	=	0.20
PHASE	=	0.

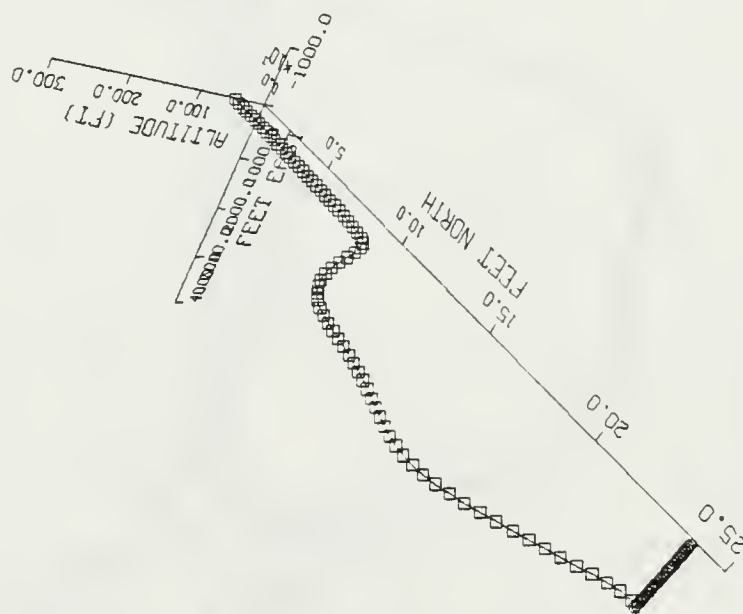


Figure A.63 Conf. II Mission Set - Geo Plot.

CRUISE MISSILE TESTS
 CONFIGURATION III MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 NORMAL LOAD FACTOR

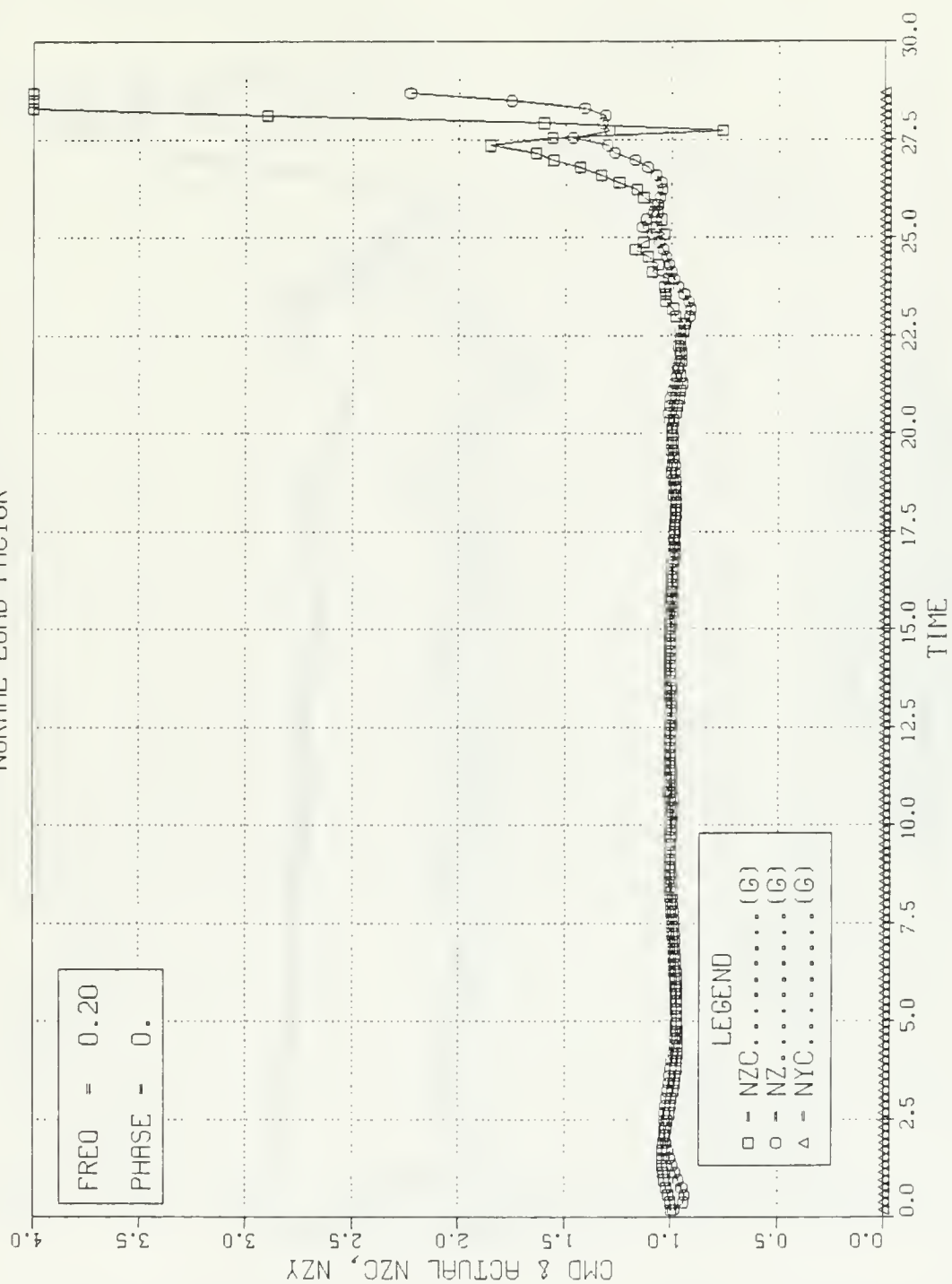


Figure A.64 Conf. III Mission Set - Load Factor.

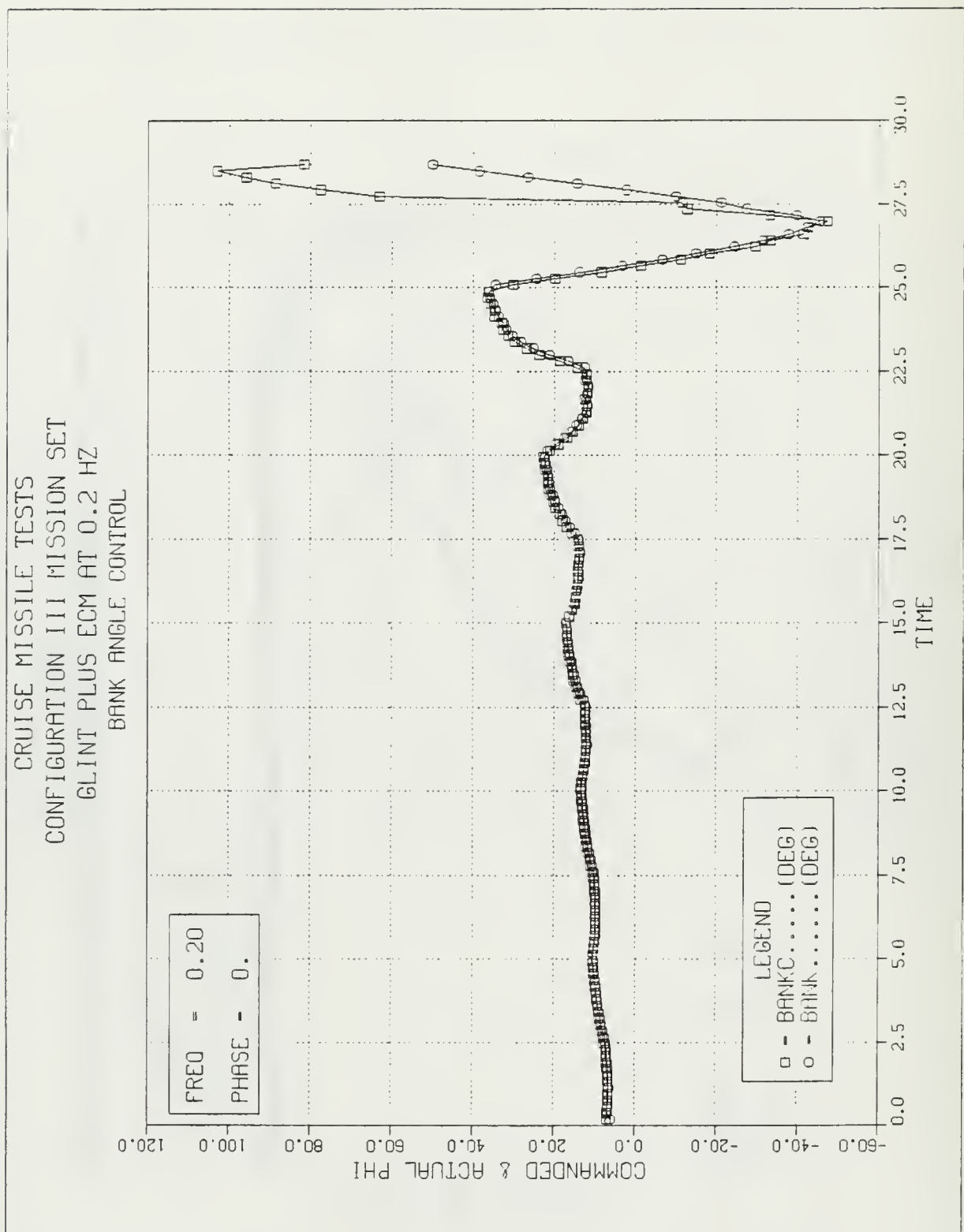


Figure A.65 Conf. III Mission Set - Bank.

CRUISE MISSILE TESTS
 CONFIGURATION III MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ROLL RATE CONTROL

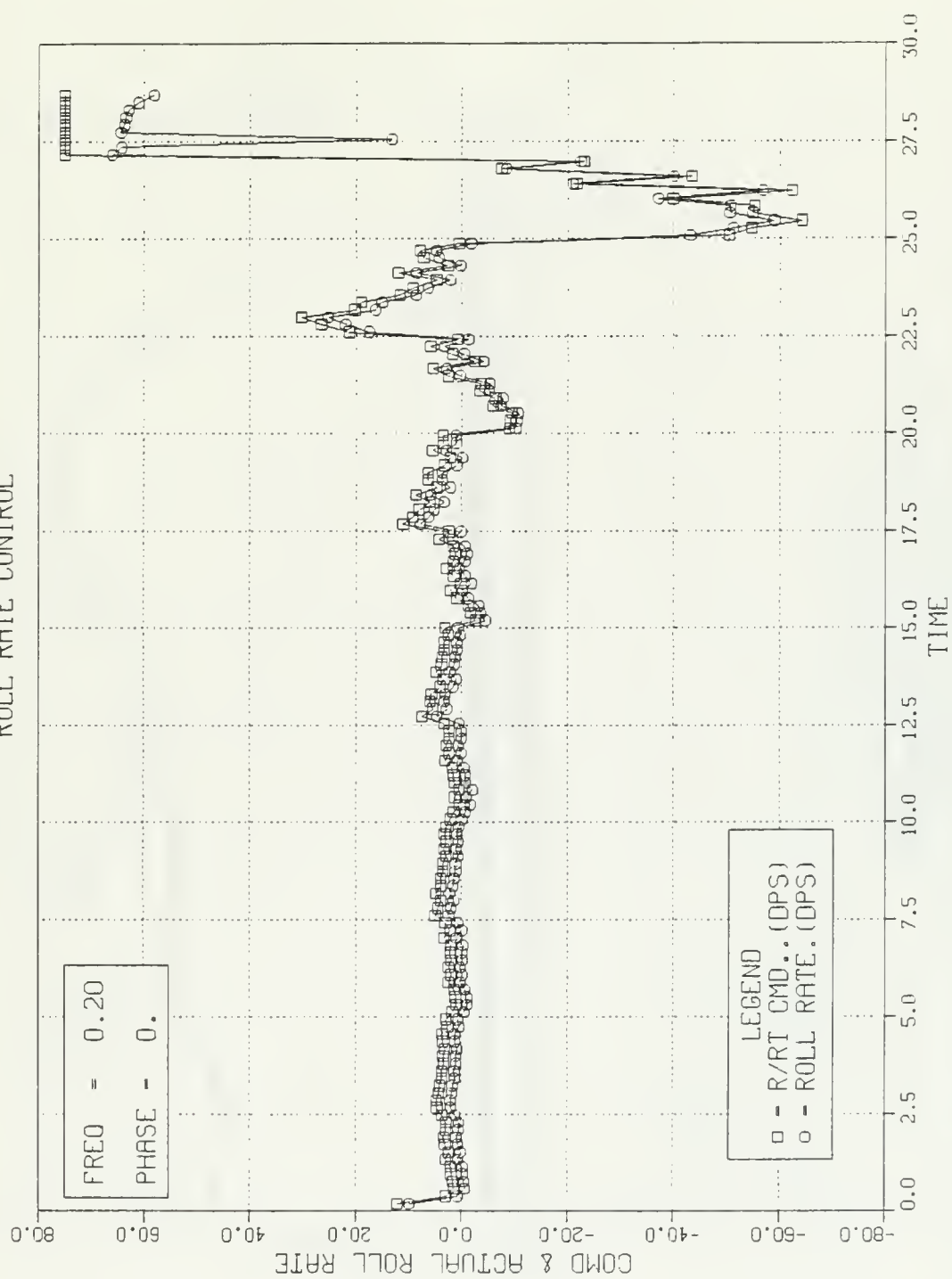


Figure A.66 Conf. III Mission Set - Roll Rate.

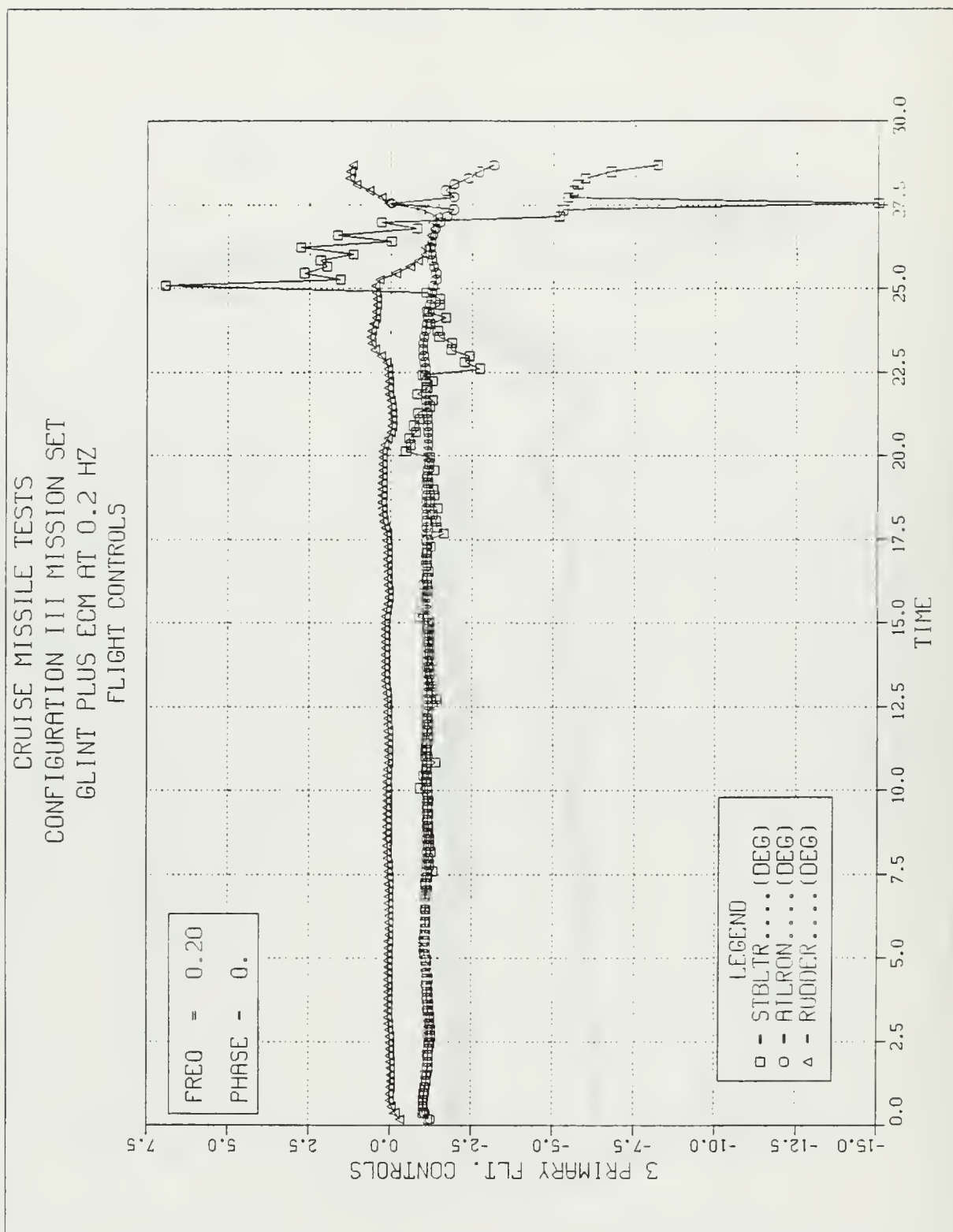


Figure A.67 Conf. III Mission Set - Controls.

CRUISE MISSILE TESTS
 CONFIGURATION III MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ALTITUDE CONTROL

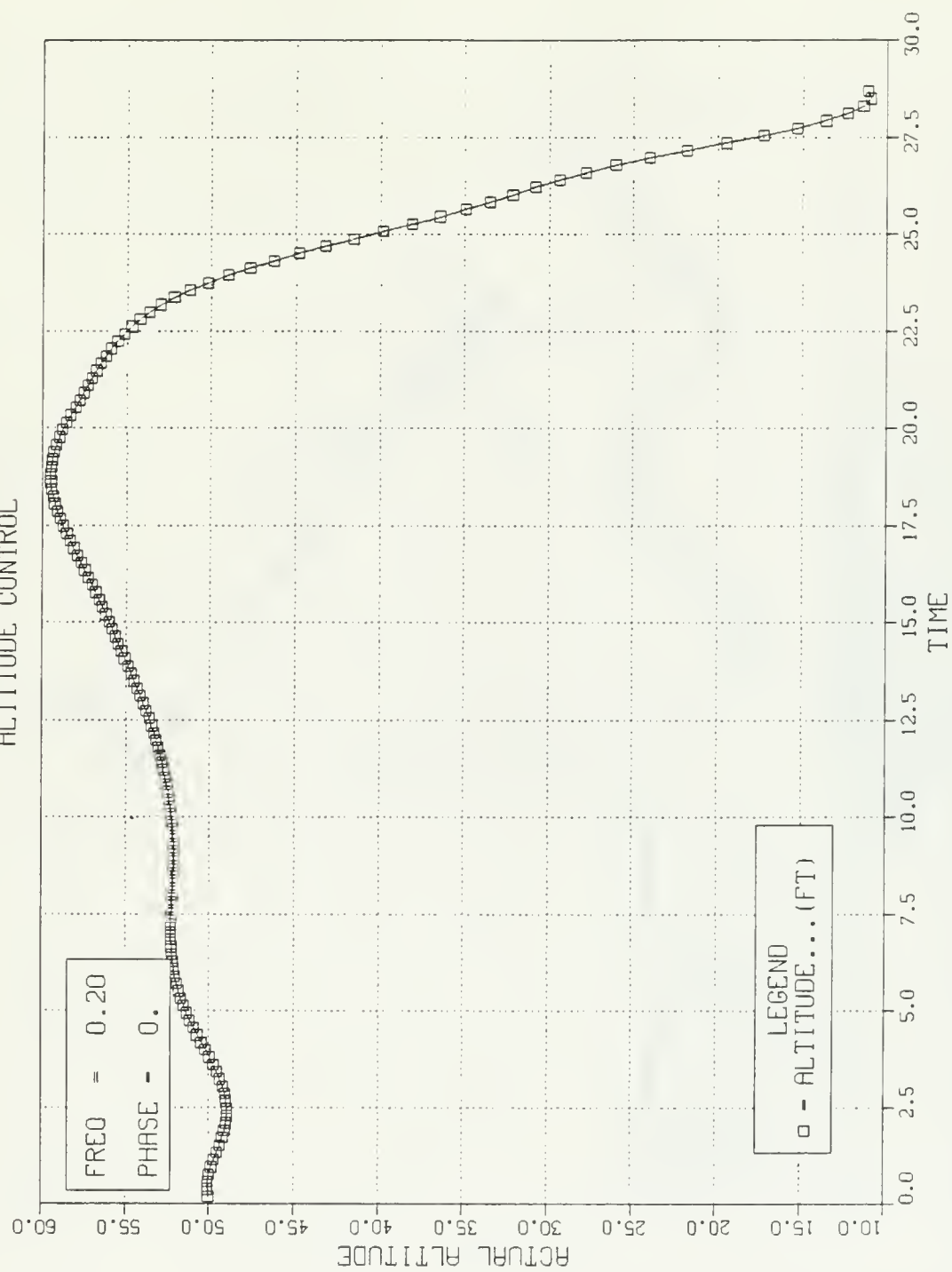


Figure A.68 Conf. III Mission Set - Altitude.

CRUISE MISSILE TESTS
 CONFIGURATION III MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 GEOGRAPHICAL TRACKS

FREQ	=	0.20
PHASE	=	0.

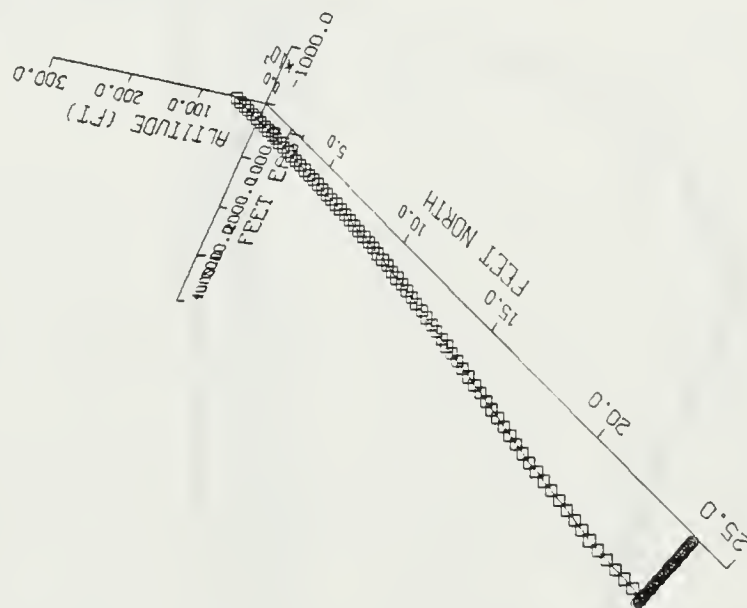


Figure A.69 Conf. III Mission Set - Geo Plot.

CRUISE MISSILE TESTS
 CONFIGURATION IV MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 NORMAL LOAD FACTOR

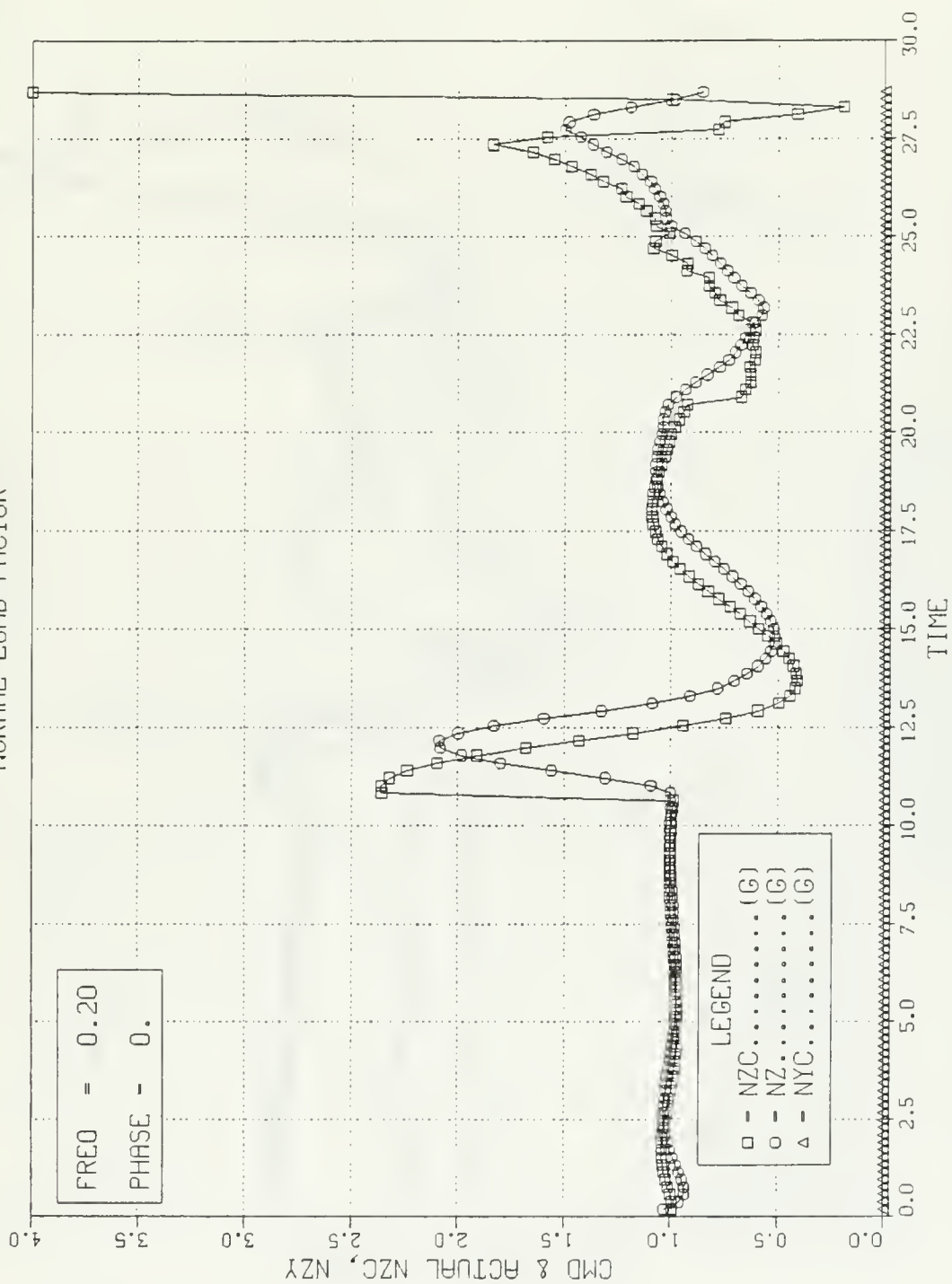


Figure A.70 Conf. IV Mission Set - Load Factor.

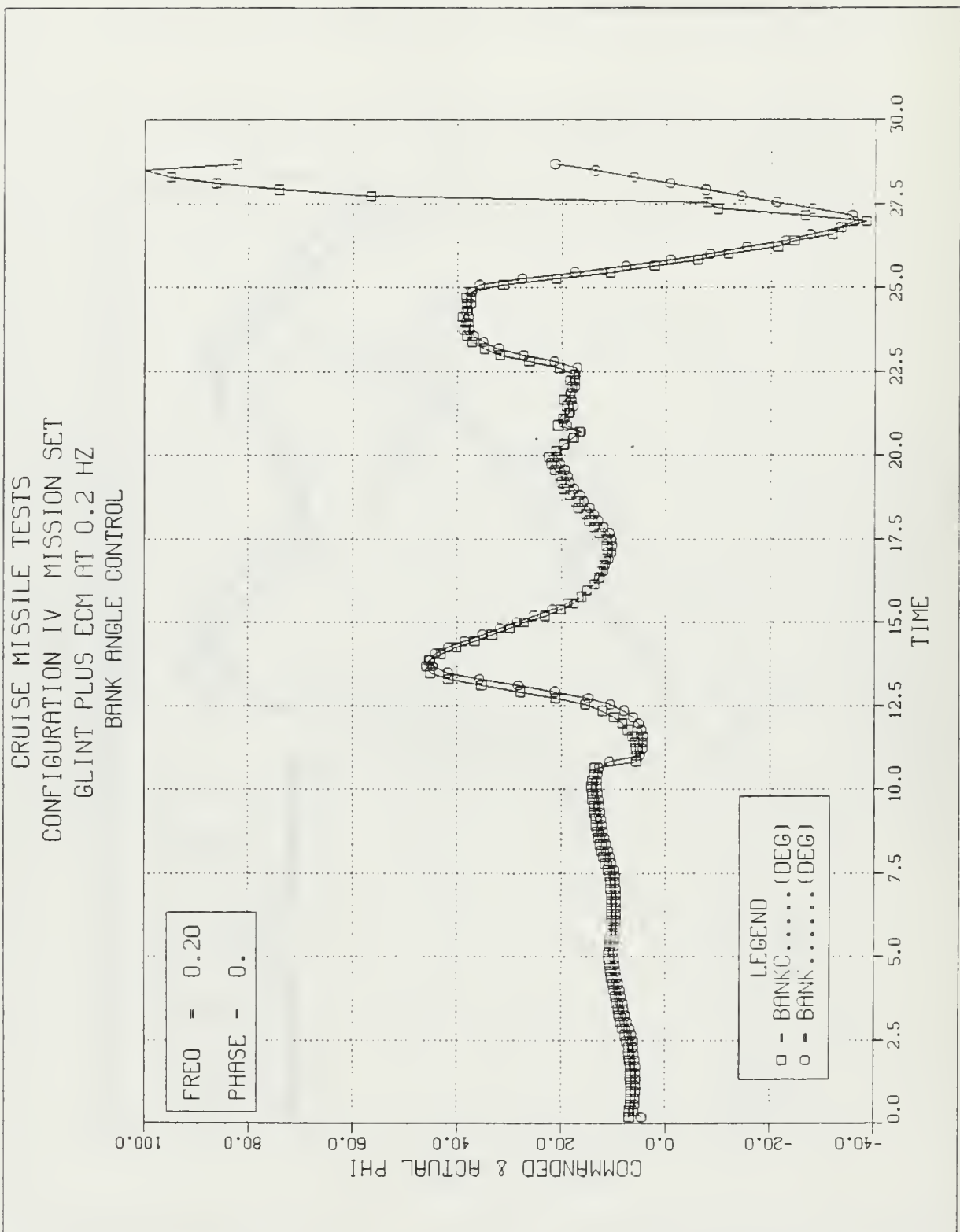


Figure A.71 Conf. IV Mission Set - Bank.

CRUISE MISSILE TESTS
 CONFIGURATION IV MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ROLL RATE CONTROL

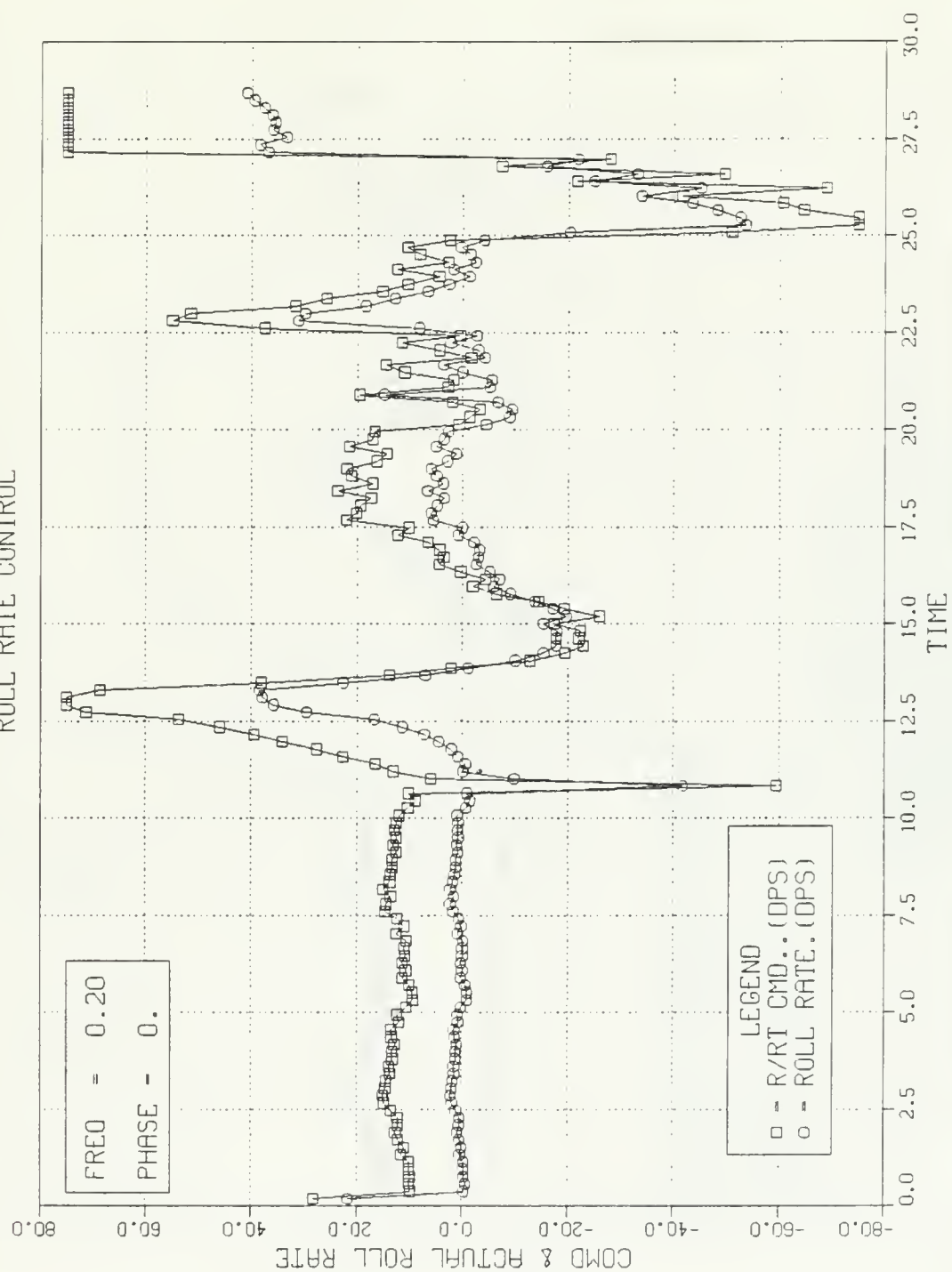


Figure A.72 Conf. IV Mission Set - Roll Rate.

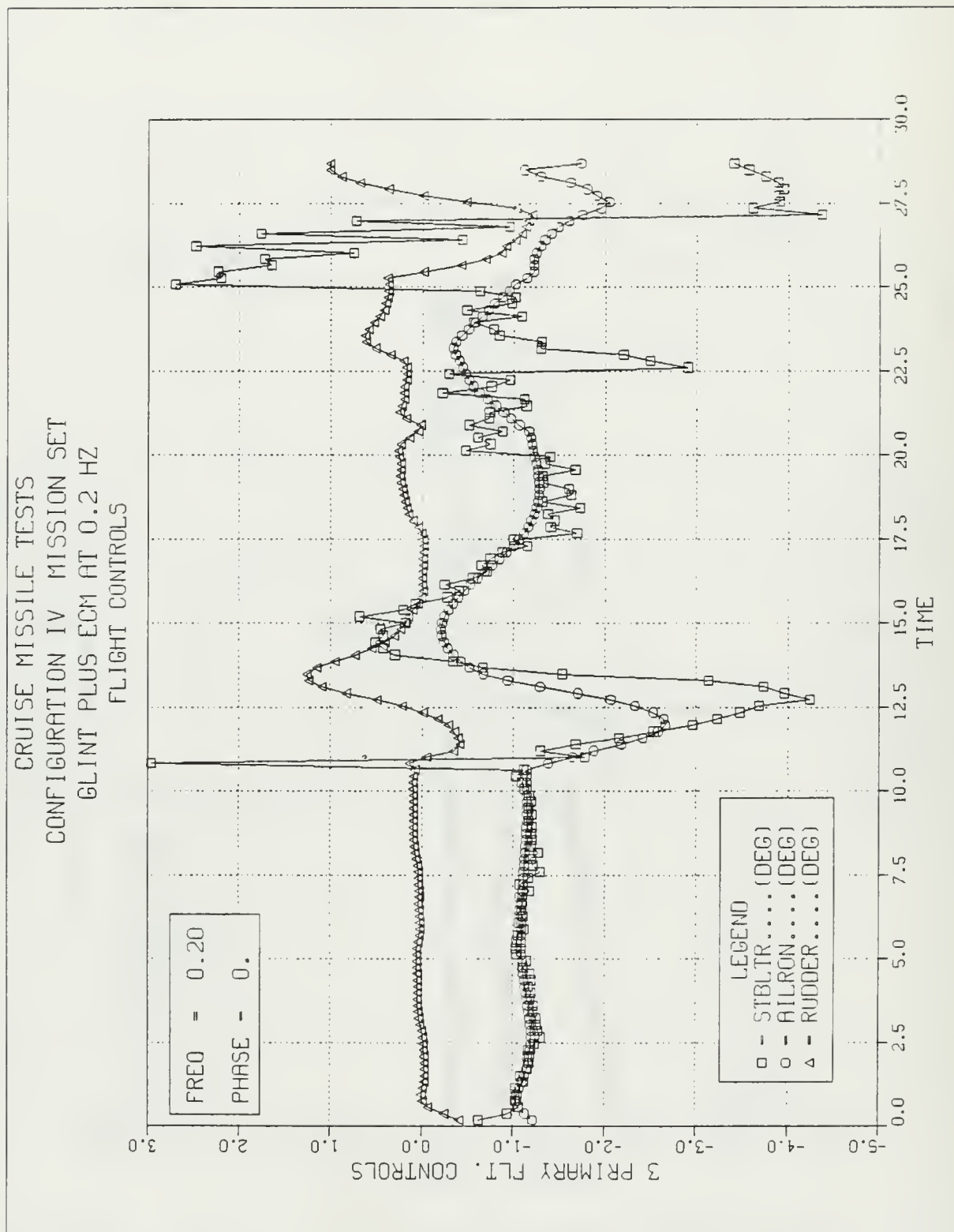


Figure A.73 Conf. IV Mission Set - Controls.

CRUISE MISSILE TESTS
 CONFIGURATION IV MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 ALTITUDE CONTROL

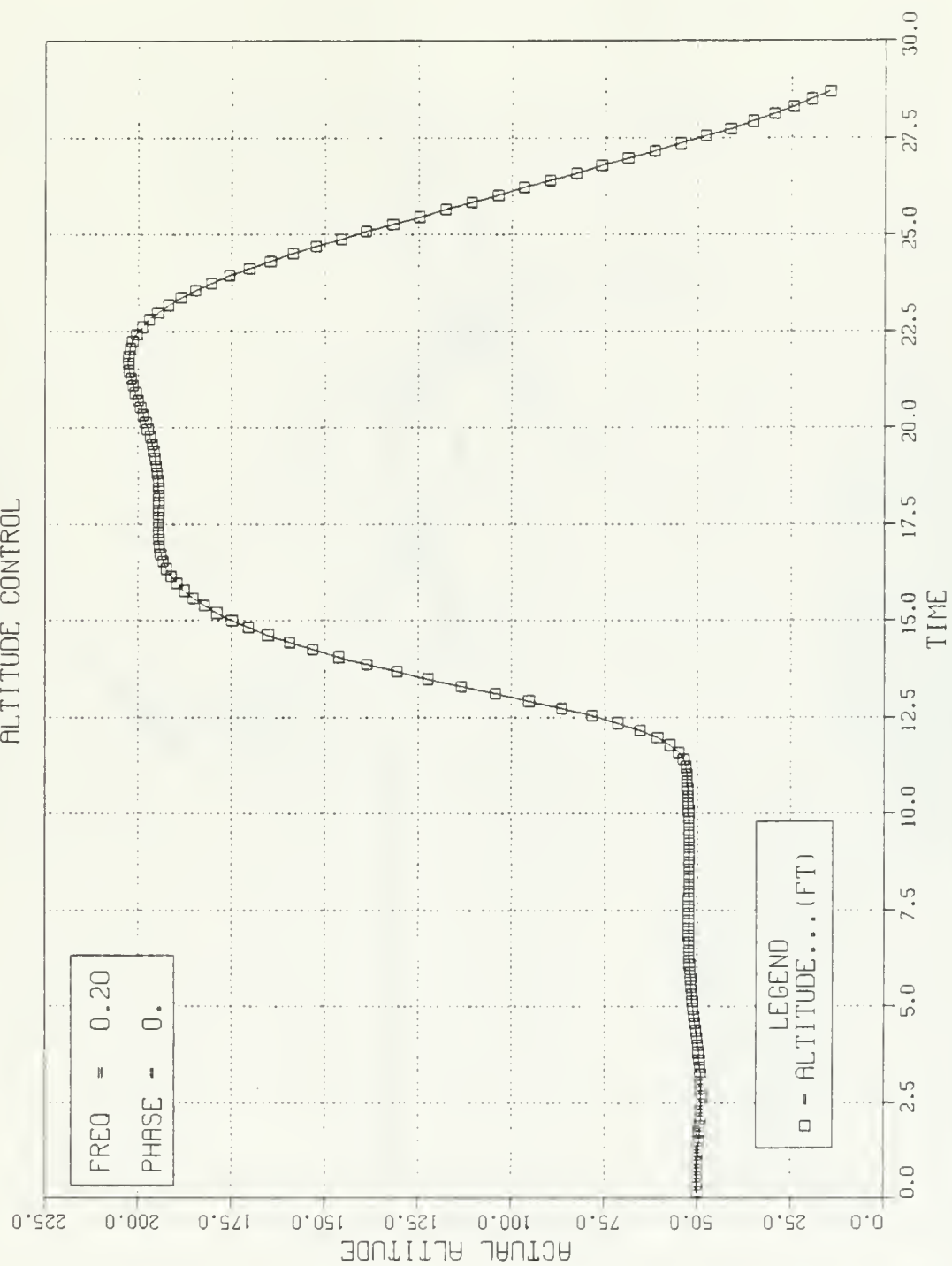


Figure A.74 Conf. IV Mission Set - Altitude.

CRUISE MISSILE TESTS
 CONFIGURATION IV MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 GEOGRAPHICAL TRACKS

FREQ	=	0.20
PHASE	=	0.

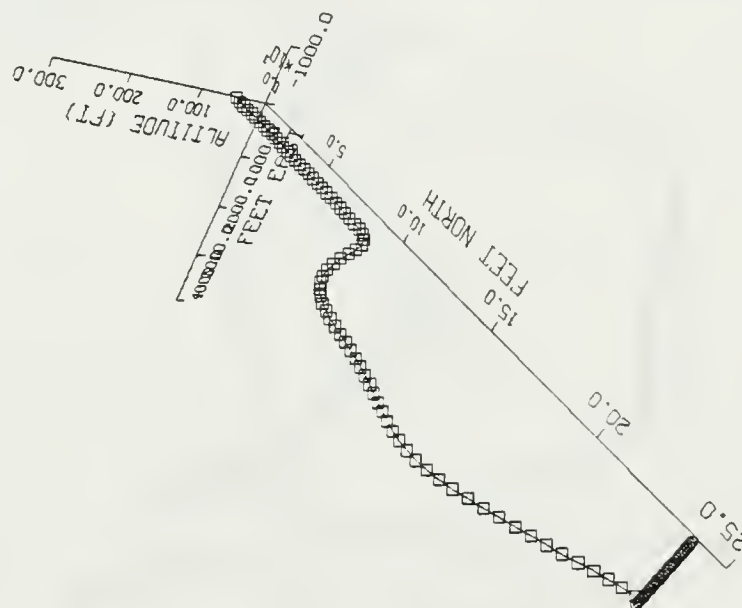


Figure A.75 Conf. IV Mission Set - Geo Plot.

CRUISE MISSILE TESTS
SEA-SKIMMER (STT) - NO GLINT
HI-FREQUENCY SCAN 0.0-21. HZ
NORMAL LOAD FACTOR

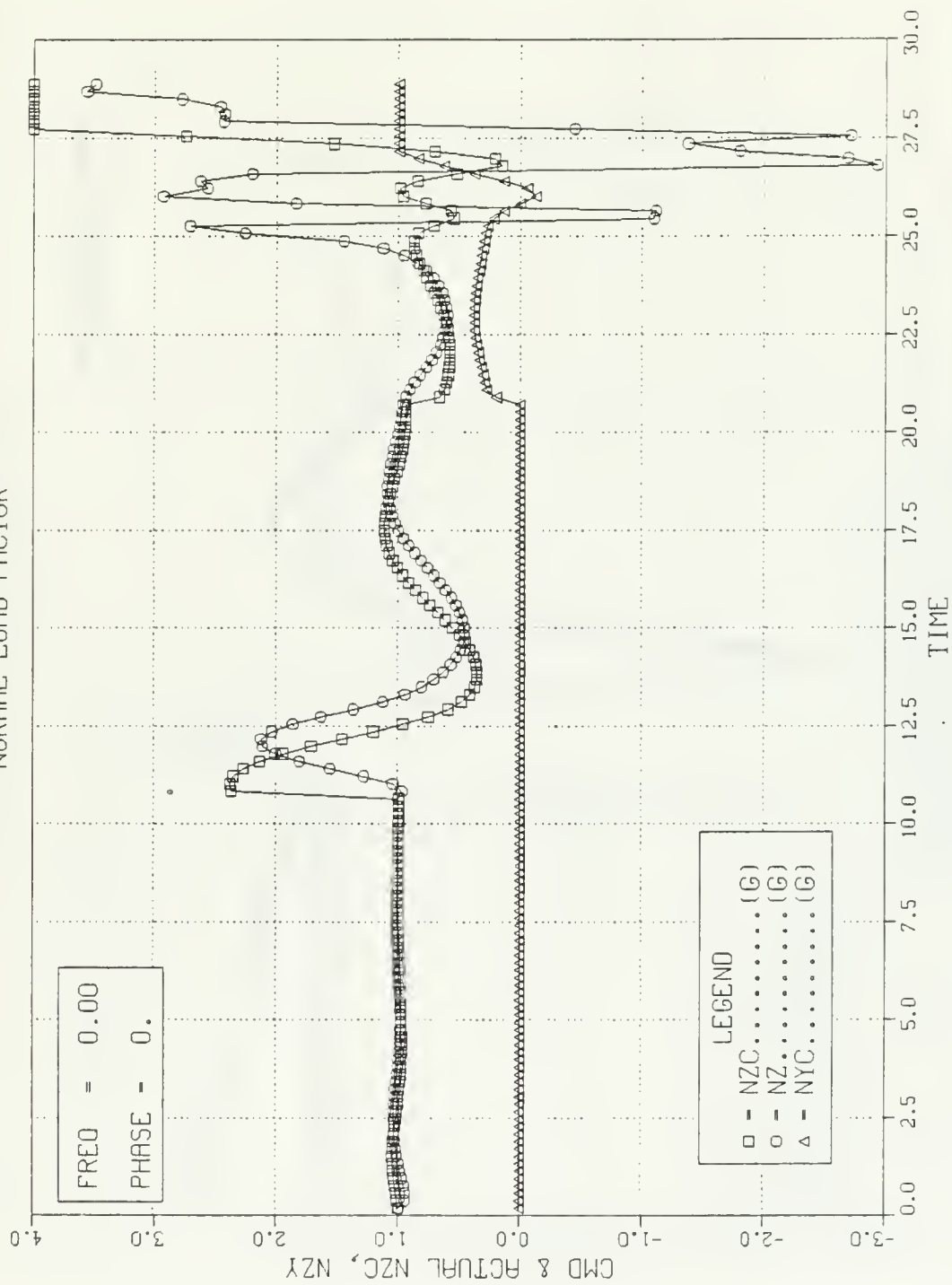


Figure A.76 Conf. V Mission Set - Load Factor.

CRUISE MISSILE TESTS
 SEA-SKIMMER (STT) - NO GLINT
 HI-FREQUENCY SCAN 0.0-21. HZ
 . BANK ANGLE CONTROL

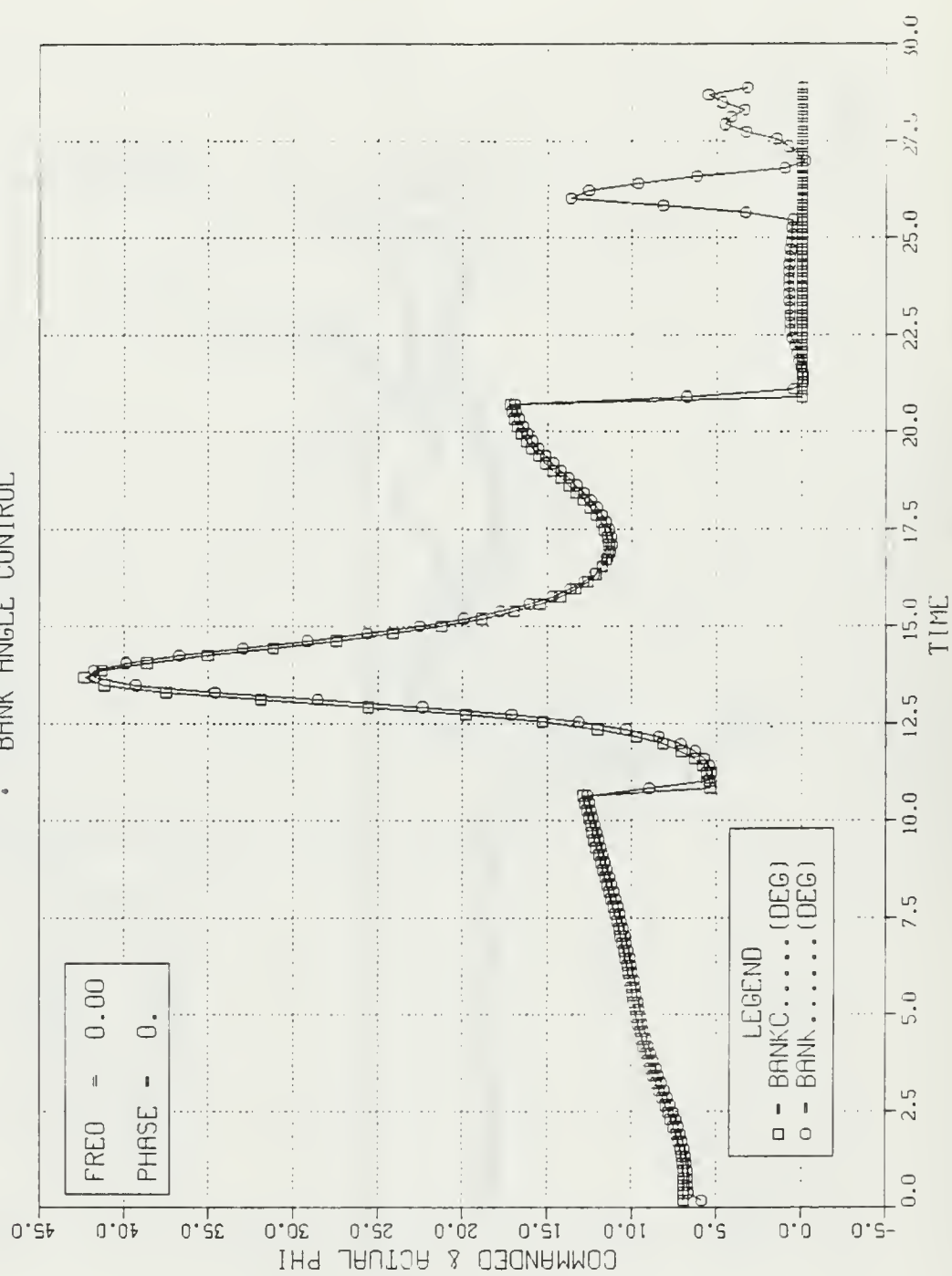


Figure A.77 Conf. V Mission Set - Bank.

CRUISE MISSILE TESTS
SEA-SKIMMER (STT) - NO GLINT
HI-FREQUENCY SCAN 0.0-21. HZ
ROLL RATE CONTROL

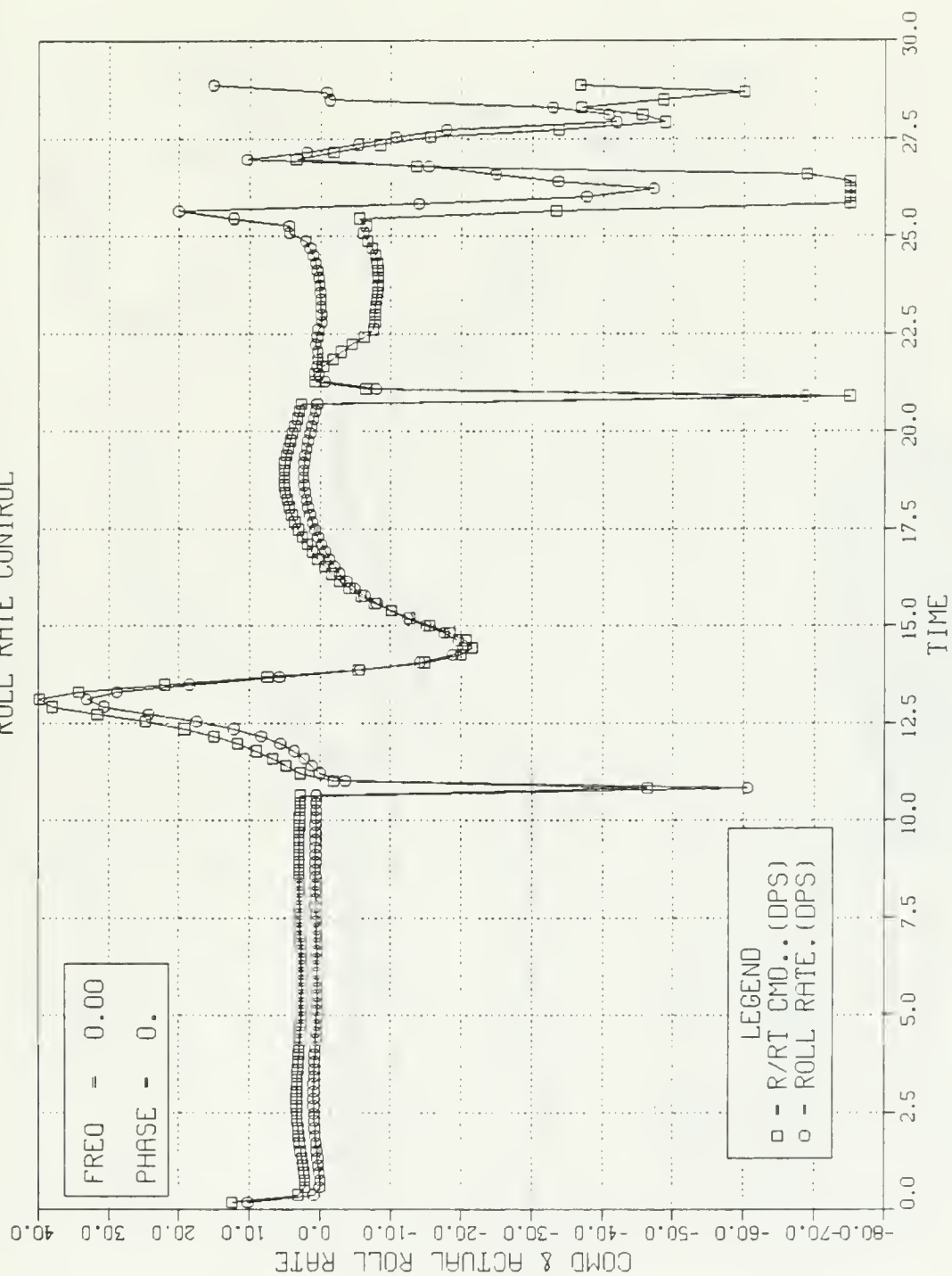


Figure A.78 Conf. V Mission Set - Roll Rate.

CRUISE MISSILE TESTS
SEA-SKIMMER (STT) - NO GLINT
HI-FREQUENCY SCAN 0.0-21. HZ
FLIGHT CONTROLS

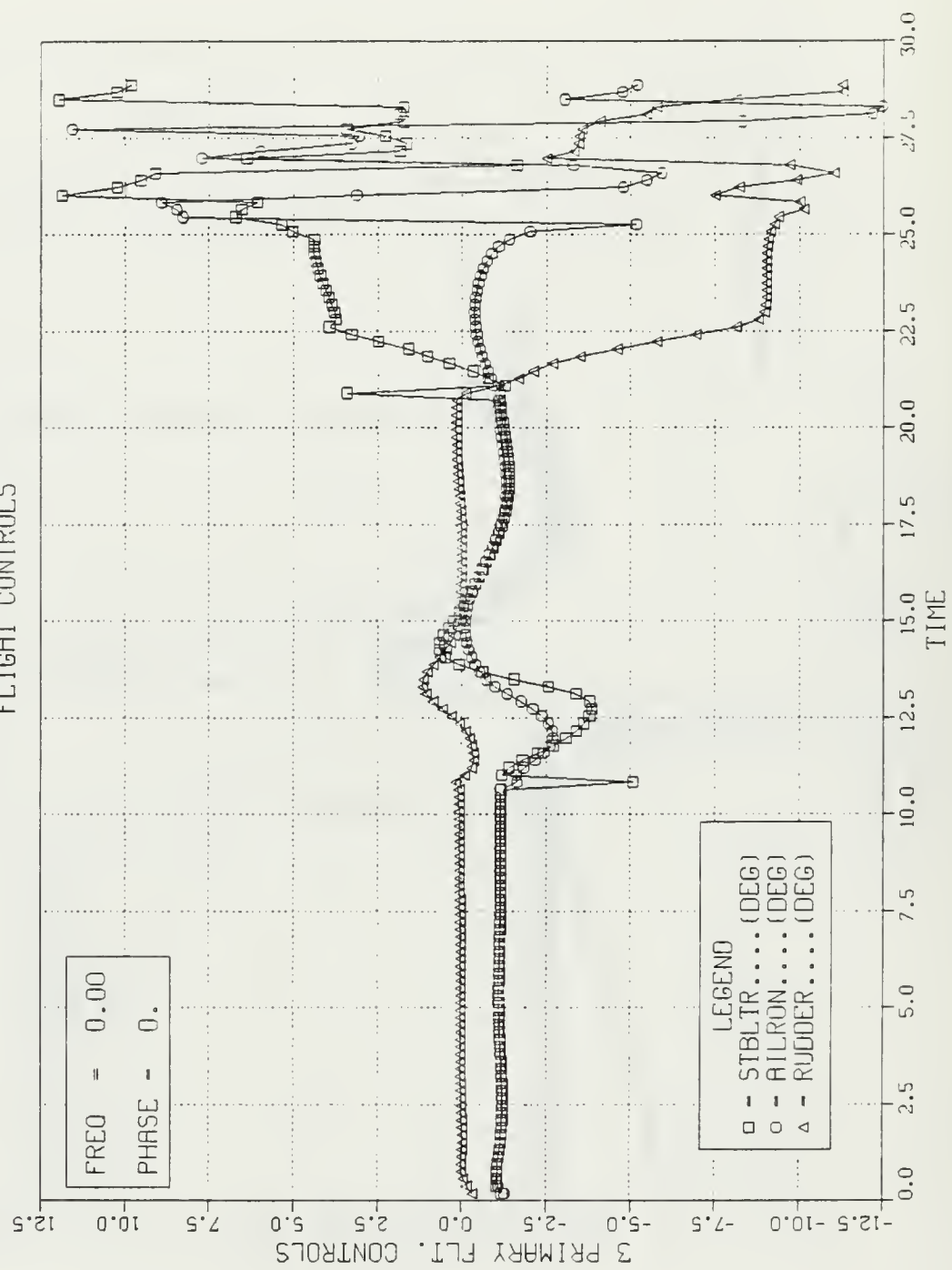


Figure A.79 Conf. V Mission Set - Controls.

CRUISE MISSILE TESTS
SEA-SKIMMER (STT) - NO GLINT
HI-FREQUENCY SCAN 0.0-21. HZ
ALTITUDE CONTROL

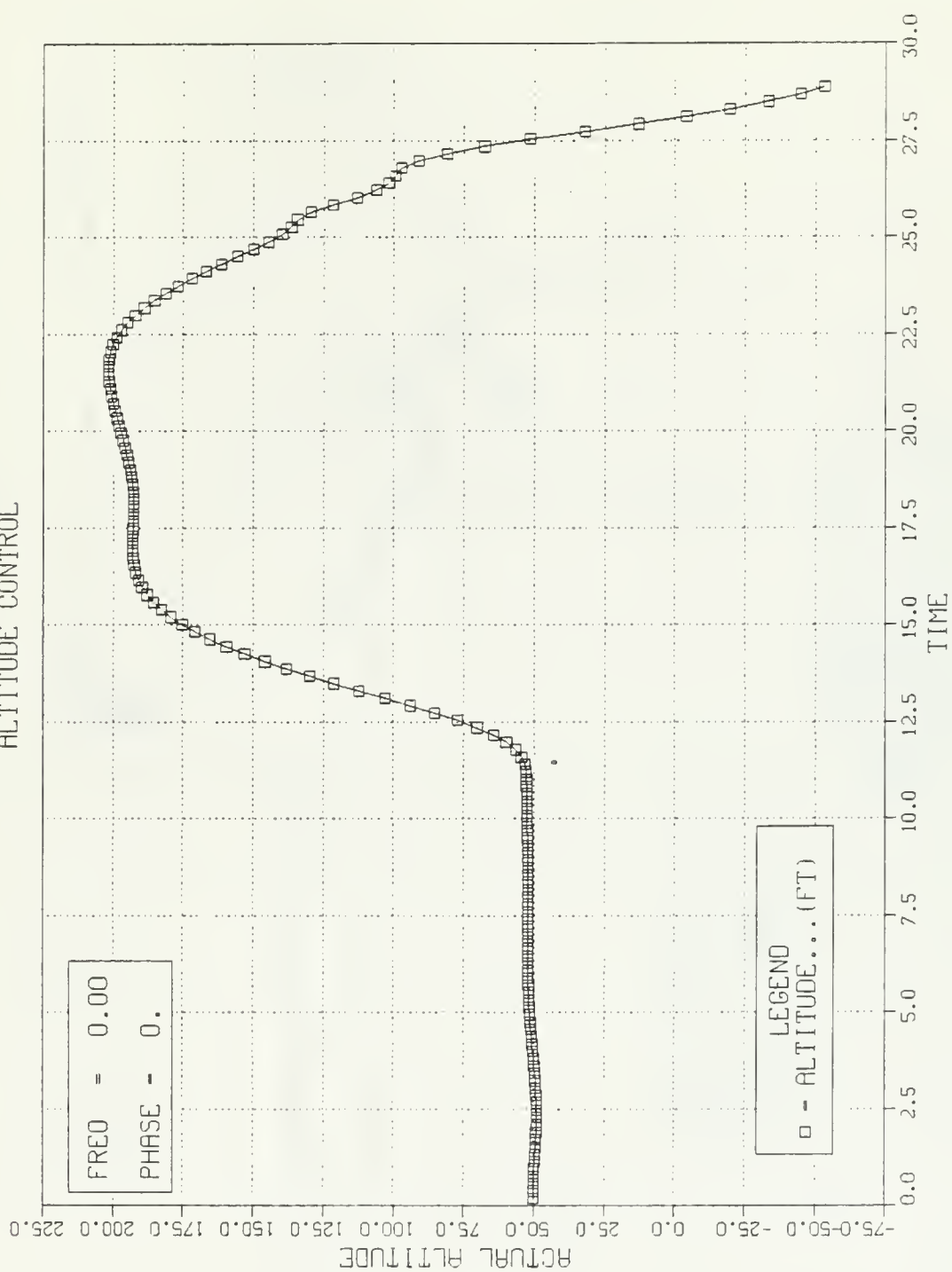


Figure A.80 Conf. V Mission Set - Altitude.

CRUISE MISSILE TESTS
 SEA-SKIMMER (STT) - NO GLINT
 HI-FREQUENCY SCAN 0.0-21. HZ
 GEOGRAPHICAL TRACKS

FREQ	=	0.00
PHASE	=	0.

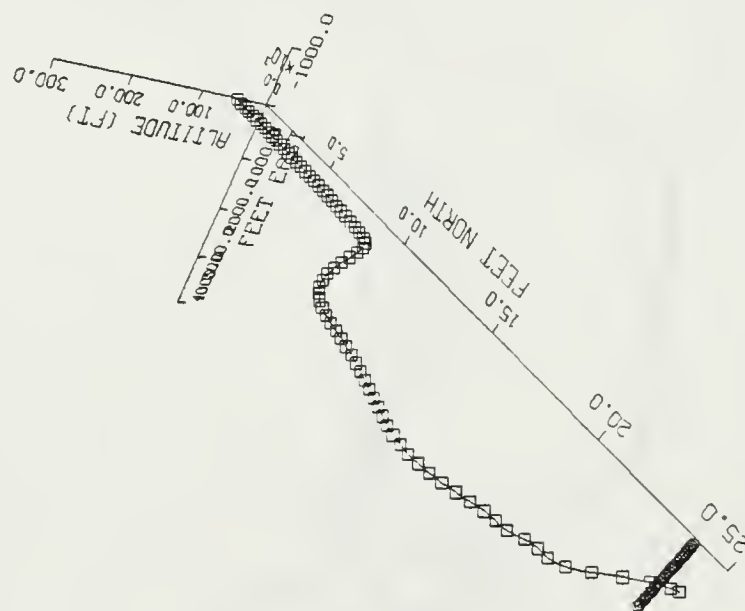


Figure A.81 Conf. V Mission Set - Geo Plot.

CRUISE MISSILE TESTS
 BALLISTIC (BTT) GUIDANCE
 NO GLINT OR ECM
 NORMAL LOAD FACTOR

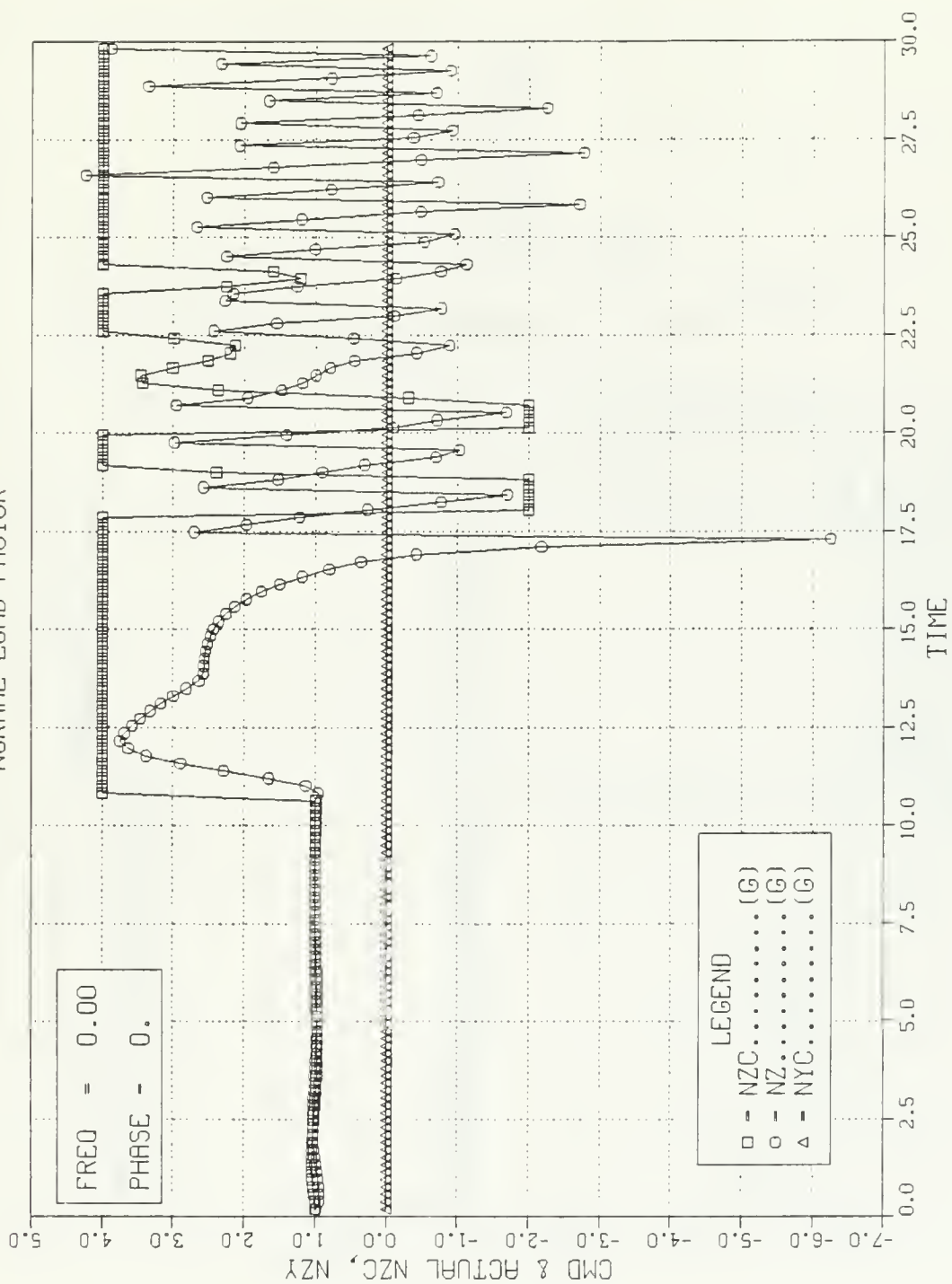


Figure A.82 Conf. VI Mission Set - Load Factor.

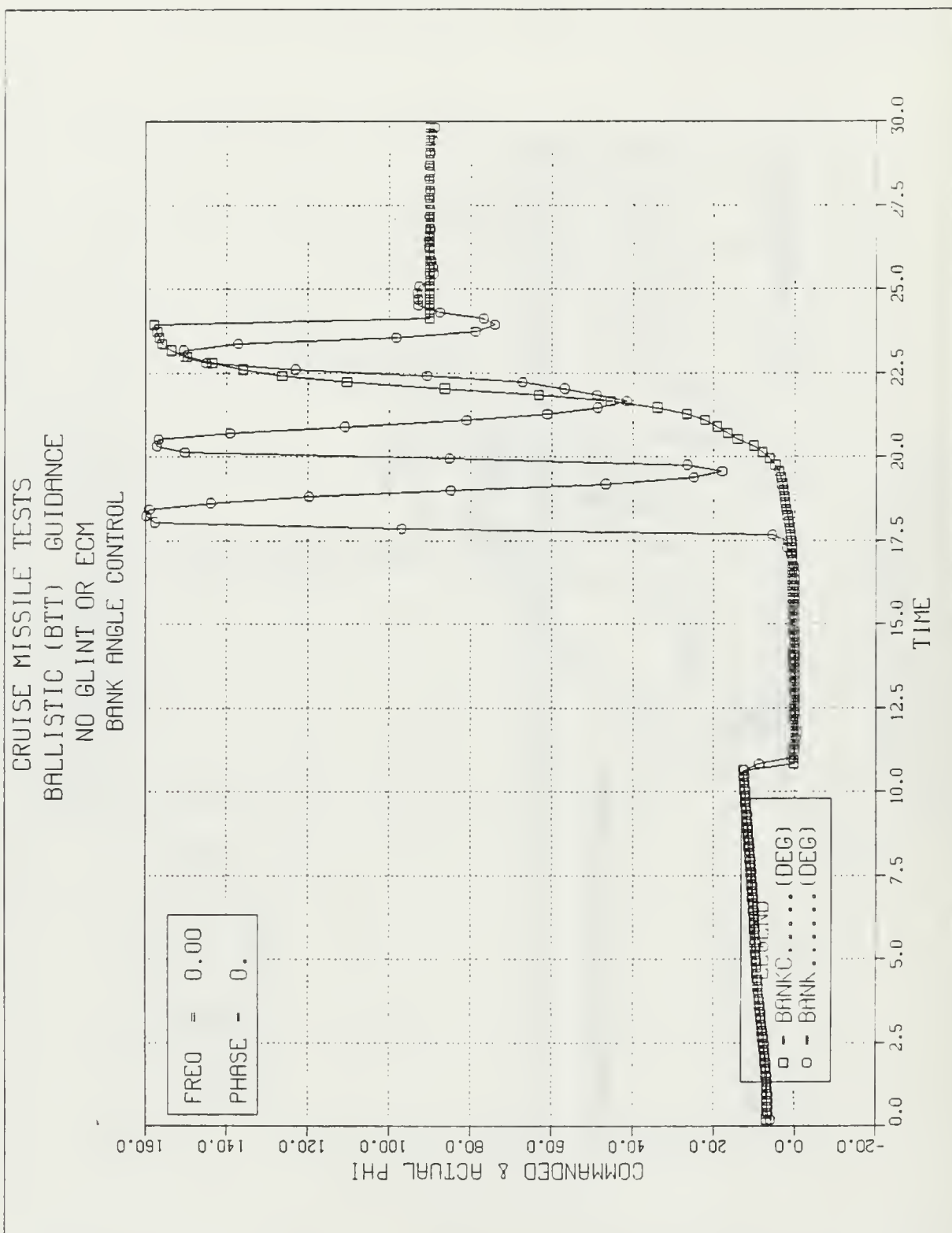


Figure A.83 Conf. VI Mission Set - Bank.

CRUISE MISSILE TESTS
 BALLISTIC (BTT) GUIDANCE
 NO GLINT OR ECM
 ROLL RATE CONTROL

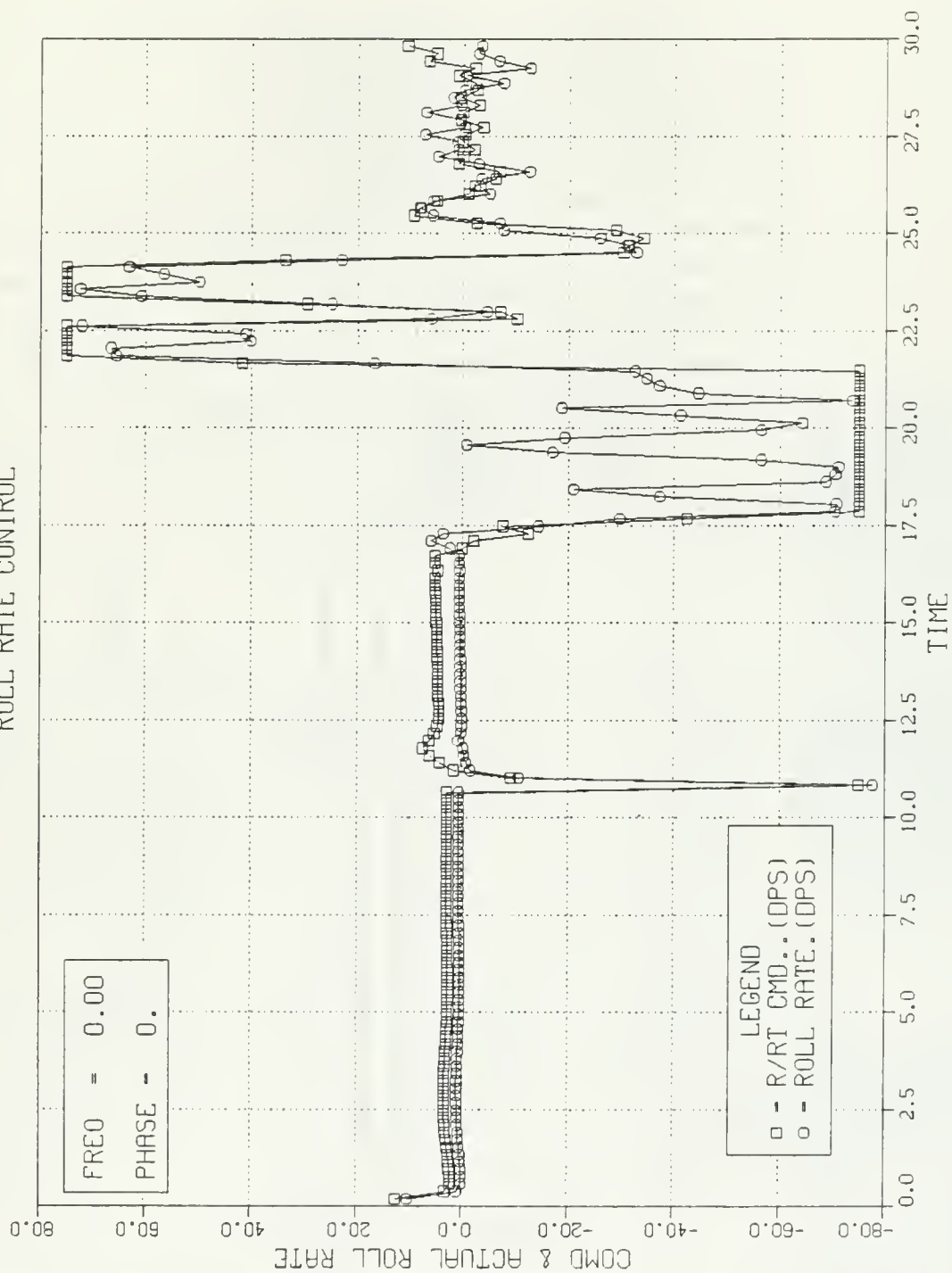


Figure A.84 Conf. VI Mission Set - Roll Rate.

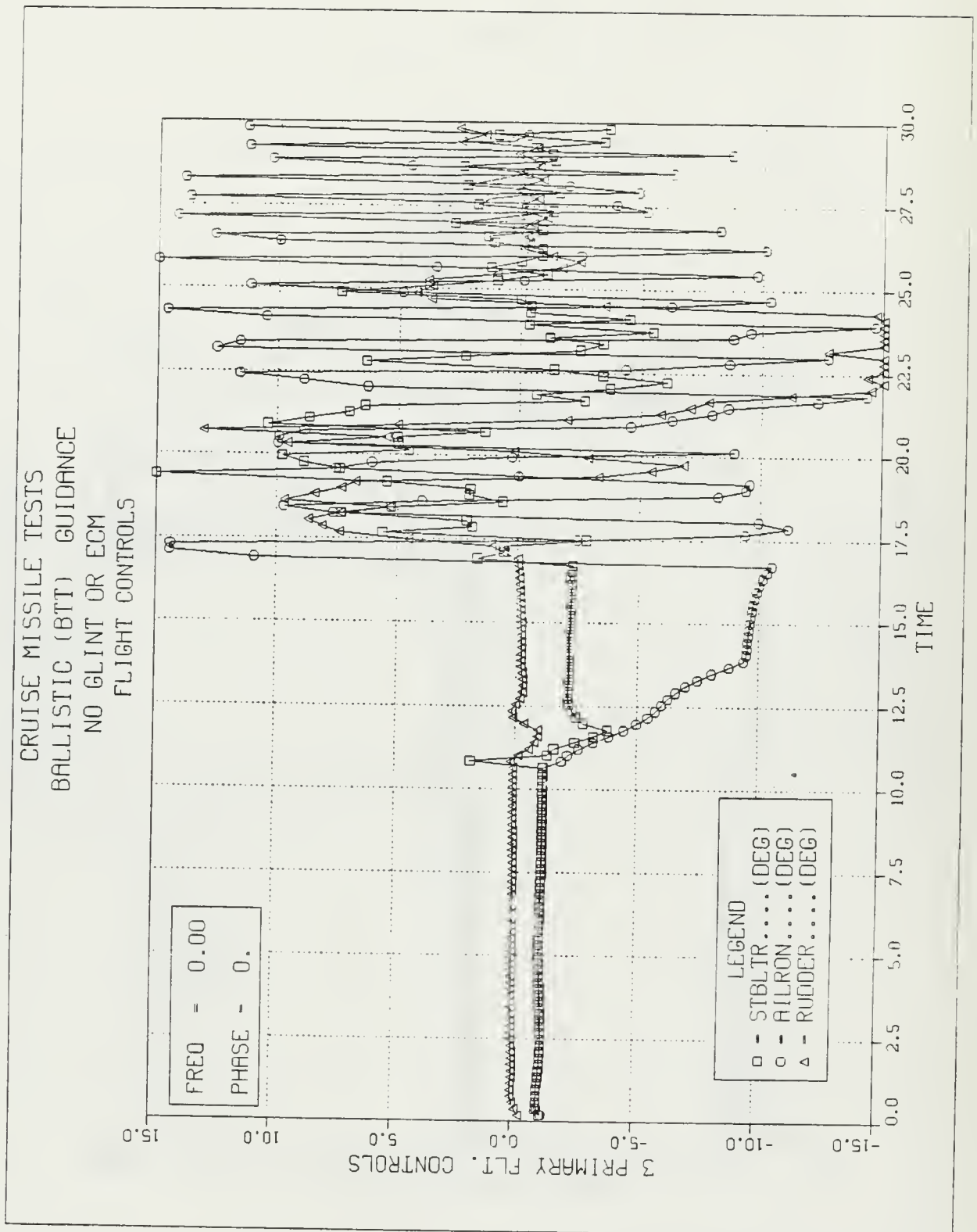


Figure A.85 Conf. VI Mission Set - Controls.

APPENDIX B

SIMULATION PROGRAM TABULAR DATA OUTPUT

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

SIMULATION TERMINATED DUE TO CPA
 *** BLINKER FREQUENCY= 0.20
 *** BLINKER PHASE = 0.

MISS DISTANCE	BANK	ROLLRATE	ERROR	FUNCTIONS	AZIMUTH	ELEVATION
42.87372	0.20466	0.11202	*	0.03046	*	0.00866

***** RANGES FOR ALL SAVED VARIABLES *****

	MINIMUM	MAXIMUM
TIME..... (SEC)	0.190000	29.061737
NZC..... (G)	0.289882	4.000000
NZ..... (G)	0.551692	3.750864
BANKC..... (DEG)	-115.634293	92.840149
BANK..... (DEG)	-115.765106	84.187943
R/RT CMD..... (DPS)	-74.999985	74.999985
RCLL RATE..... (DPS)	-73.526184	73.167145
ECM SHIFT..... (FT)	-75.000000	75.000000
GLINT SHIFT..... (FT)	-47.924805	47.070313
STBLTR..... (DEG)	-15.000000	7.934396
AILRCN..... (DEG)	-6.261881	0.000000

RUDCER... (DEG)
ALTITUDE... (FT)
XM... (FT NORTH)
YM... (FT EAST)
XT... (FT NORTH)
XM... (FT EAST)
RANGE... (FT)
PHASE MARKER

-3.446685
13.361130
159.440155
-3.526452
24000.000000
6.649995
116.888184
0.000000

2.952714
250.106537
23887.324200
17771.405030
24000.000000
1017.160640
23840.589800
4.000000

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 FZ
9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 1 OF 4

TIME... (SEC) NZC... (G) NZ... (G) BANKC... (DEG) BANK... (DEG)

0.190000
0.380000
0.570000
0.759999
0.949999
1.139999
1.329975
1.519961
1.709948
1.899934
2.089920
2.279906
2.469893
2.659879
2.849865
3.039851
3.229837
3.419824
3.609810
3.799796
3.989782
4.179765
4.369755
0.996454
1.002067
1.012286
1.022474
1.032748
1.043086
1.053439
1.063848
1.074217
1.084593
1.094911
1.105217
1.115517
1.125810
1.136095
1.146375
1.156652
1.166927
1.177203
1.187479
1.197755
1.208031
1.218307
1.228582
1.238858
1.249134
1.259410
1.269686
1.279962
1.290238
1.300514
1.310790
1.321066
1.331342
1.341618
1.351894
1.362170
1.372446
1.382722
1.393000
1.403276
1.413552
1.423828
1.434104
1.444380
1.454656
1.464932
1.475208
1.485484
1.495760
1.506036
1.516312
1.526588
1.536864
1.547140
1.557416
1.567692
1.577968
1.588244
1.598520
1.608796
1.619072
1.629348
1.639624
1.649900
1.660176
1.670452
1.680728
1.691004
1.701280
1.711556
1.721832
1.732108
1.742384
1.752660
1.762936
1.773212
1.783488
1.793764
1.804040
1.814316
1.824592
1.834868
1.845144
1.855420
1.865696
1.875972
1.886248
1.896524
1.906800
1.917076
1.927352
1.937628
1.947904
1.958180
1.968456
1.978732
1.989008
1.999284
1.009560
1.019836
1.030112
1.040388
1.050664
1.060940
1.071216
1.081492
1.091768
1.102044
1.112320
1.122596
1.132872
1.143148
1.153424
1.163700
1.173976
1.184252
1.194528
1.204804
1.215080
1.225356
1.235632
1.245908
1.256184
1.266460
1.276736
1.287012
1.297288
1.307564
1.317840
1.328116
1.338392
1.348668
1.358944
1.369220
1.379496
1.389772
1.390048
1.400324
1.410600
1.420876
1.431152
1.441428
1.451704
1.461980
1.472256
1.482532
1.492808
1.503084
1.513360
1.523636
1.533912
1.544188
1.554464
1.564740
1.575016
1.585292
1.595568
1.605844
1.616120
1.626396
1.636672
1.646948
1.657224
1.667500
1.677776
1.688052
1.698328
1.708604
1.718880
1.729156
1.739432
1.749708
1.759984
1.770260
1.780536
1.790812
1.801088
1.811364
1.821640
1.831916
1.842192
1.852468
1.862744
1.873020
1.883296
1.893572
1.903848
1.914124
1.924400
1.934676
1.944952
1.955228
1.965504
1.975780
1.986056
1.996332
2.006608
2.016884
2.027160
2.037436
2.047712
2.057988
2.068264
2.078540
2.088816
2.099092
2.109368
2.119644
2.129920
2.140196
2.150472
2.160748
2.171024
2.181300
2.191576
2.201852
2.212128
2.222404
2.232680
2.242956
2.253232
2.263508
2.273784
2.284060
2.294336
2.304612
2.314888
2.325164
2.335440
2.345716
2.355992
2.366268
2.376544
2.386820
2.397096
2.407372
2.417648
2.427924
2.438200
2.448476
2.458752
2.469028
2.479304
2.489580
2.499856
2.510132
2.520408
2.530684
2.540960
2.551236
2.561512
2.571788
2.582064
2.592340
2.602616
2.612892
2.623168
2.633444
2.643720
2.653996
2.664272
2.674548
2.684824
2.695100
2.705376
2.715652
2.725928
2.736204
2.746480
2.756756
2.767032
2.777308
2.787584
2.797860
2.808136
2.818412
2.828688
2.838964
2.849240
2.859516
2.869792
2.880068
2.890344
2.900620
2.910896
2.921172
2.931448
2.941724
2.952000
2.962276
2.972552
2.982828
2.993104
3.003380
3.013656
3.023932
3.034208
3.044484
3.054760
3.065036
3.075312
3.085588
3.095864
3.106140
3.116416
3.126692
3.136968
3.147244
3.157520
3.167796
3.178072
3.188348
3.198624
3.208900
3.219176
3.229452
3.239728
3.240004
3.250280
3.260556
3.270832
3.281108
3.291384
3.301660
3.311936
3.322212
3.332488
3.342764
3.353040
3.363316
3.373592
3.383868
3.394144
3.404420
3.414696
3.424972
3.435248
3.445524
3.455800
3.466076
3.476352
3.486628
3.496904
3.507180
3.517456
3.527732
3.538008
3.548284
3.558560
3.568836
3.579112
3.589388
3.599664
3.609940
3.620216
3.630492
3.640768
3.651044
3.661320
3.671596
3.681872
3.692148
3.702424
3.712700
3.722976
3.733252
3.743528
3.753804
3.764080
3.774356
3.784632
3.794908
3.805184
3.815460
3.825736
3.836012
3.846288
3.856564
3.866840
3.877116
3.887392
3.897668
3.907944
3.918220
3.928496
3.938772
3.949048
3.959324
3.969600
3.979876
3.990152
4.000428
4.010704
4.020980
4.031256
4.041532
4.051808
4.062084
4.072360
4.082636
4.092912
4.103188
4.113464
4.123740
4.134016
4.144292
4.154568
4.164844
4.175120
4.185396
4.195672
4.205948
4.216224
4.226500
4.236776
4.247052
4.257328
4.267604
4.277880
4.288156
4.298432
4.308708
4.318984
4.329260
4.339536
4.349812
4.360088
4.370364
4.380640
4.390916
4.401192
4.411468
4.421744
4.432020
4.442296
4.452572
4.462848
4.473124
4.483400
4.493676
4.503952
4.514228
4.524504
4.534780
4.545056
4.555332
4.565608
4.575884
4.586160
4.596436
4.606712
4.616988
4.627264
4.637540
4.647816
4.658092
4.668368
4.678644
4.688920
4.699196
4.709472
4.719748
4.720024
4.730300
4.740576
4.750852
4.761128
4.771404
4.781680
4.791956
4.802232
4.812508
4.822784
4.833060
4.843336
4.853612
4.863888
4.874164
4.884440
4.894716
4.904992
4.915268
4.925544
4.935820
4.946096
4.956372
4.966648
4.976924
4.987200
4.997476
5.007752
5.018028
5.028304
5.038580
5.048856
5.059132
5.069408
5.079684
5.089960
5.100236
5.110512
5.120788
5.131064
5.141340
5.151616
5.161892
5.172168
5.182444
5.192720
5.202996
5.213272
5.223548
5.233824
5.244100
5.254376
5.264652
5.274928
5.285204
5.295480
5.305756
5.316032
5.326308
5.336584
5.346860
5.357136
5.367412
5.377688
5.387964
5.398240
5.408516
5.418792
5.429068
5.439344
5.449620
5.459896
5.470172
5.480448
5.490724
5.501000
5.511276
5.521552
5.531828
5.542104
5.552380
5.562656
5.572932
5.583208
5.593484
5.603760
5.614036
5.624312
5.634588
5.644864
5.655140
5.665416
5.675692
5.685968
5.696244
5.706520
5.716796
5.727072
5.737348
5.747624
5.757900
5.768176
5.778452
5.788728
5.799004
5.809280
5.819556
5.829832
5.840108
5.850384
5.860660
5.870936
5.881212
5.891488
5.901764
5.912040
5.922316
5.932592
5.942868
5.953144
5.963420
5.973696
5.983972
5.994248
6.004524
6.014800
6.025076
6.035352
6.045628
6.055904
6.066180
6.076456
6.086732
6.097008
6.107284
6.117560
6.127836
6.138112
6.148388
6.158664
6.168940
6.179216
6.189492
6.199768
6.210044
6.220320
6.230596
6.240872
6.251148
6.261424
6.271700
6.281976
6.292252
6.302528
6.312804
6.323080
6.333356
6.343632
6.353908
6.364184
6.374460
6.384736
6.395012
6.405288
6.415564
6.425840
6.436116
6.446392
6.456668
6.466944
6.477220
6.487496
6.497772
6.508048
6.518324
6.528600
6.538876
6.549152
6.559428
6.569704
6.579980
6.590256
6.600532
6.610808
6.621084
6.631360
6.641636
6.651912
6.662188
6.672464
6.682740
6.693016
6.703292
6.713568
6.723844
6.734120
6.744396
6.754672
6.764948
6.775224
6.785500
6.795776
6.806052
6.816328
6.826604
6.836880
6.847156
6.857432
6.867708
6.877984
6.888260
6.898536
6.908812
6.919088
6.929364
6.939640
6.949916
6.960192
6.970468
6.980744
6.991020
7.001296
7.011572
7.021848
7.032124
7.042400
7.052676
7.062952
7.073228
7.083504
7.093780
7.104056
7.114332
7.124608
7.134884
7.145160
7.155436
7.165712
7.175988
7.186264
7.196540
7.206816
7.217092
7.227368
7.237644
7.247920
7.258196
7.268472
7.278748
7.289024
7.299300
7.309576
7.319852
7.330128
7.340404
7.350680
7.360956
7.371232
7.381508
7.391784
7.402060
7.412336
7.422612
7.432888
7.443164
7.453440
7.463716
7.473992
7.484268
7.494544
7.504820
7.515096
7.525372
7.535648
7.545924
7.556200
7.566476
7.576752
7.587028
7.597304
7.607580
7.617856
7.628132
7.638408
7.648684
7.658960
7.669236
7.679512
7.689788
7.690064
7.700340
7.710616
7.720892
7.731168
7.741444
7.751720
7.761996
7.772272
7.782548
7.792824
7.803100
7.813376
7.823652
7.833928
7.844204
7.854480
7.864756
7.875032
7.885308
7.895584
7.905860
7.916136
7.926412
7.936688
7.946964
7.957240
7.967516
7.977792
7.988068
7.998344
8.008620
8.018896
8.029172
8.039448
8.049724
8.050000
8.060276
8.070552
8.080828
8.091104
8.101380
8.111656
8.121932
8.132208
8.142484
8.152760
8.163036
8.173312
8.183588
8.193864
8.204140
8.214416
8.224692
8.234968
8.245244
8.255520
8.265796
8.276072
8.286348
8.296624
8.306900
8.317176
8.327452
8.337728
8.348004
8.358280
8.368556
8.378832
8.389108
8.399384
8.409660
8.419936
8.430212
8.440488
8.450764
8.461040
8.471316
8.481592
8.491868
8.502144
8.512420
8.522696
8.532972
8.543248
8.553524
8.563800
8.574076
8.584352
8.594628
8.604904
8.615180
8.625456
8.635732
8.646008
8.656284
8.666560
8.676836
8.687112
8.697388
8.707664
8.717940
8.728216
8.738492
8.748768
8.759044
8.769320
8.779596
8.789872
8.790148
8.800424
8.810700
8.820976
8.831252
8.841528
8.851804
8.862080
8.872356
8.882632
8.892908
8.903184
8.913460
8.923736
8.934012
8.944288
8.954564
8.964840
8.975116
8.985392
8.995668
9.005944
9.016220
9.026496
9.036772
9.047048
9.057324
9.067600
9.077876
9.088152
9.098428
9.108704
9.118980
9.129256
9.139532
9.149808
9.160084
9.170360
9.180636
9.190912
9.201188
9.211464
9.221740
9.232016
9.242292
9.252568
9.262844
9.273120
9.283396
9.293672
9.303948
9.314224
9.324500
9.334776
9.345052
9.355328
9.365604
9.375880
9.386156
9.396432
9.406708
9.416984
9.427260
9.437536
9.447812
9.458088
9.468364
9.478640
9.488916
9.499192
9.509468
9.519744
9.520020
9.530296
9.540572
9.550848
9.561124
9.571400
9.581676
9.591952
9.602228
9.612504
9.622780
9.633056
9.643332
9.653608
9.663884
9.674160
9.684436
9.694712
9.704988
9.715264
9.725540
9.735816
9.746092
9.756368
9.766644
9.776920
9.787196
9.797472
9.807748
9.818024
9.828300
9.838576
9.848852
9.859128
9.869404
9.879680
9.889956
9.890232
9.900508
9.910784
9.921060
9.931336
9.941612
9.951888
9.962164
9.972440
9.982716
9.992992
10.003268
10.013544
10.023820
10.034096
10.044372
10.054648
10.064924
10.075200
10.085476
10.095752
10.106028
10.116304
10.126580
10.136856
10.147132
10.157408
10.167684
10.177960
10.188236
10.198512
10.208788
10.219064
10.229340
10.239616
10.249892
10.260168
10.270444
10.280720
10.290996
10.301272
10.311548
10.321824
10.332100
10.342376
10.352652
10.362928
10.373204
10.383480
10.393756
10.404032
10.414308
10.424584
10.434860
10.445136
10.455412
10.465688
10.475964
10.486240
10.496516
10.506792
10.517068
10.527344
10.537620
10.547896
10.558172
10.568448
10.578724
10.589000
10.599276
10.609552
10.619828
10.630104
10.640380
10.650656
10.660932
10.671208
10.681484
10.691760
10.702036
10.712312
10.722588
10.732864
10.743140
10.753416
10.763692
10.773968
10.784244
10.794520
10.804796
10.815072
10.825348
10.835624
10.845900
10.856176
10.866452
10.876728
10.887004
10.897280
10.907556
10.917832
10.928108
10.938384
10.948660
10.958936
10.969212
10.979488
10.989764
10.990040
11.000316
11.010592
11.020868
11.031144
11.041420
11.051696
11.061972
11.072248
11.082524
11.092800
11.103076
11.113352
11.123628
11.133904
11.144180
11.154456
11.164732
11.175008
11.185284
11.195560
11.205836
11.216112
11.226388
11.236664
11.246940
11.257216
11.267492
11.277768
11.288044
11.298320
11.308596
11.318872
11.329148
11.339424
11.349700
11.359976
11.370252
11.380528
11.390804
11.401080
11.411356
11.421632
11.431908
11.442184
11.452460
11.462736
11.473012
11.483288
11.493564
11.503840
11.514116
11.524392
11.534668
11.544944
11.555220
11.565496
11.575772
11.586


```

***
19.5669556
19.568517
19.946747
19.136642
20.326538
20.516434
20.706325
20.896221
21.086121
21.276016
21.465912
21.655807
21.845703
22.035599
22.225494
22.415390
22.605286
22.795181
22.985077
23.174973
23.364868
23.554764
23.744659
23.934555
24.124451
***

4.000000
4.000000
4.000000
4.000000
4.000000
4.395334
4.645613
4.895900
5.146187
5.396474
5.646761
5.897048
6.147335
6.397622
6.647909
6.898196
7.148483
7.398770
7.649057
7.899344
8.149631
8.399918
8.650205
8.900492
9.150779
9.401066
9.651353
9.901640
10.151927
10.402214
10.652501
10.902788
11.153075
11.403362
11.653649
11.903936
12.154223
12.404510
12.654797
12.905084
13.155371
13.405658
13.655945
13.906232
14.156519
14.406806
14.657093
14.907380
15.157667
15.407954
15.658241
15.908528
16.158815
16.409102
16.659389
16.909676
17.159963
17.410250
17.660537
17.910824
18.161111
18.411398
18.661685
18.911972
19.162259
19.412546
19.662833
19.913120
20.163407
20.413694
20.663981
20.914268
21.164555
21.414842
21.665129
21.915416
22.165703
22.415990
22.666277
22.916564
23.166851
23.417138
23.667425
23.917712
24.168000
24.418287
24.668574
24.918861
25.169148
25.419435
25.669722
25.910009
26.160296
26.410583
26.660870
26.911157
27.161444
27.411731
27.662018
27.912305
28.162592
28.412879
28.663166
28.913453
29.163740
29.414027
29.664314
29.914601
30.164888
30.415175
30.665462
30.915749
31.166036
31.416323
31.666610
31.916897
32.167184
32.417471
32.667758
32.918045
33.168332
33.418619
33.668906
33.919193
34.169480
34.419767
34.660054
34.910341
35.160628
35.410915
35.661202
35.911489
36.161776
36.412063
36.662350
36.912637
37.162924
37.413211
37.663498
37.913785
38.164072
38.414359
38.664646
38.914933
39.165220
39.415507
39.665794
39.916081
40.166368
40.416655
40.666942
40.917229
41.167516
41.417803
41.668090
41.918377
42.168664
42.418951
42.669238
42.919525
43.169812
43.410099
43.660386
43.910673
44.160960
44.411247
44.661534
44.911821
45.162108
45.412395
45.662682
45.912969
46.163256
46.413543
46.663830
46.914117
47.164404
47.414691
47.664978
47.915265
48.165552
48.415839
48.666126
48.916413
49.166700
49.416987
49.667274
49.917561
50.167848
50.418135
50.668422
50.918709
51.168996
51.419283
51.669570
51.919857
52.170144
52.410431
52.660718
52.911005
53.161292
53.411579
53.661866
53.912153
54.162440
54.412727
54.663014
54.913301
55.163588
55.413875
55.664162
55.914449
56.164736
56.415023
56.665310
56.915597
57.165884
57.416171
57.666458
57.916745
58.167032
58.417319
58.667606
58.917893
59.168180
59.418467
59.668754
59.919041
60.169328
60.419615
60.669902
60.910189
61.160476
61.410763
61.661050
61.911337
62.161624
62.411911
62.662198
62.912485
63.162772
63.413059
63.663346
63.913633
64.163920
64.414207
64.664494
64.914781
65.165068
65.415355
65.665642
65.915929
66.166216
66.416503
66.666790
66.917077
67.167364
67.417651
67.667938
67.918225
68.168512
68.418799
68.669086
68.919373
69.169660
69.419947
69.670234
69.910521
70.160808
70.411095
70.661382
70.911669
71.161956
71.412243
71.662530
71.912817
72.163104
72.413391
72.663678
72.913965
73.164252
73.414539
73.664826
73.915113
74.165400
74.415687
74.665974
74.916261
75.166548
75.416835
75.667122
75.917409
76.167696
76.417983
76.668270
76.918557
77.168844
77.419131
77.669418
77.919705
78.169992
78.410279
78.660566
78.910853
79.161140
79.411427
79.661714
79.912001
80.162288
80.412575
80.662862
80.913149
81.163436
81.413723
81.664010
81.914297
82.164584
82.414871
82.665158
82.915445
83.165732
83.416019
83.666306
83.916593
84.166880
84.417167
84.667454
84.917741
85.168028
85.418315
85.668602
85.918889
86.169176
86.419463
86.669750
86.910037
87.160324
87.410611
87.660898
87.911185
88.161472
88.411759
88.662046
88.912333
89.162620
89.412907
89.663194
89.913481
90.163768
90.414055
90.664342
90.914629
91.164916
91.415203
91.665490
91.915777
92.166064
92.416351
92.666638
92.916925
93.167212
93.417499
93.667786
93.918073
94.168360
94.418647
94.668934
94.919221
95.169508
95.419795
95.660082
95.910369
96.160656
96.410943
96.661230
96.911517
97.161804
97.412091
97.662378
97.912665
98.162952
98.413239
98.663526
98.913813
99.164100
99.414387
99.664674
99.914961
100.165248
100.415535
100.665822
100.916109
101.166396
101.416683
101.666970
101.917257
102.167544
102.417831
102.668118
102.918405
103.168692
103.418979
103.669266
103.919553
104.169840
104.410127
104.660414
104.910701
105.160988
105.411275
105.661562
105.911849
106.162136
106.412423
106.662710
106.913000
107.163287
107.413574
107.663861
107.914148
108.164435
108.414722
108.665009
108.915296
109.165583
109.415870
109.666157
109.916444
110.166731
110.417018
110.667305
110.917592
111.167879
111.418166
111.668453
111.918740
112.169027
112.419314
112.669601
112.919888
113.160175
113.410462
113.660749
113.911036
114.161323
114.411610
114.661897
114.912184
115.162471
115.412758
115.663045
115.913332
116.163619
116.413906
116.664193
116.914480
117.164767
117.415054
117.665341
117.915628
118.165915
118.416202
118.666489
118.916776
119.167063
119.417350
119.667637
119.917918
120.168205
120.418492
120.668779
120.919066
121.169353
121.419640
121.669927
121.910214
122.160501
122.410788
122.661075
122.911362
123.161649
123.411936
123.662223
123.912510
124.162797
124.413084
124.663371
124.913658
125.163945
125.414232
125.664519
125.914806
126.165093
126.415380
126.665667
126.915954
127.166241
127.416528
127.666815
127.917102
128.167389
128.417676
128.667963
128.918250
129.168537
129.418824
129.669111
129.919398
130.169685
130.419972
130.660259
130.910546
131.160833
131.411120
131.661407
131.911694
132.161981
132.412268
132.662555
132.912842
133.163129
133.413416
133.663703
133.913990
134.164277
134.414564
134.664851
134.915138
135.165425
135.415712
135.666000
135.916287
136.166574
136.416861
136.667148
136.917435
137.167722
137.418009
137.668296
137.918583
138.168870
138.419157
138.669444
138.919731
139.160018
139.410305
139.660592
139.910880
140.161167
140.411454
140.661741
140.912028
141.162315
141.412602
141.662889
141.913176
142.163463
142.413750
142.664037
142.914324
143.164611
143.414898
143.665185
143.915472
144.165759
144.416046
144.666333
144.916620
145.166907
145.417194
145.667481
145.917770
146.168057
146.418344
146.668631
146.918920
147.169207
147.419494
147.669781
147.910070
148.160357
148.410644
148.660931
148.911218
149.161505
149.411792
149.662079
149.912366
150.162653
150.412940
150.663227
150.913514
151.163801
151.414088
151.664375
151.914662
152.164949
152.415236
152.665523
152.915810
153.166097
153.416384
153.666671
153.916960
154.167247
154.417534
154.667821
154.918108
155.168395
155.418682
155.668969
155.919256
156.169543
156.419830
156.660117
156.910404
157.160691
157.410978
157.661265
157.911552
158.161839
158.412126
158.662413
158.912700
159.162987
159.413274
159.663561
159.913850
160.164137
160.414424
160.664711
160.915000
161.165287
161.415574
161.665861
161.916148
162.166435
162.416722
162.667009
162.917296
163.167583
163.417870
163.668157
163.918444
164.168731
164.419018
164.669305
164.919592
165.169879
165.410166
165.660453
165.910740
166.161027
166.411314
166.661601
166.911888
167.162175
167.412462
167.662749
167.913036
168.163323
168.413610
168.663897
168.914184
169.164471
169.414758
169.665045
169.915332
170.165619
170.415906
170.666193
170.916480
171.166767
171.417054
171.667341
171.917628
172.167915
172.418202
172.668489
172.918776
173.169063
173.419350
173.669637
173.919924
174.160211
174.410498
174.660785
174.911072
175.161359
175.411646
175.661933
175.912220
176.162507
176.412794
176.663081
176.913368
177.163655
177.413942
177.664229
177.914516
178.164803
178.415090
178.665377
178.915664
179.165951
179.416238
179.666525
179.916812
180.167100
180.417387
180.667674
180.917961
181.168248
181.418535
181.668822
181.919109
182.169396
182.419683
182.669970
182.910257
183.160544
183.410831
183.661118
183.911405
184.161692
184.411979
184.662266
184.912553
185.162840
185.413127
185.663414
185.913701
186.163988
186.414275
186.664562
186.914850
187.165137
187.415424
187.665711
187.916000
188.166287
188.416574
188.666861
188.917150
189.167437
189.417724
189.668011
189.918300
190.168587
190.418874
190.669161
190.919450
191.169737
191.410024
191.660311
191.910598
192.160885
192.411172
192.661459
192.911746
193.162033
193.412320
193.662607
193.912894
194.163181
194.413470
194.663757
194.914044
195.164331
195.414620
195.664907
195.915196
196.165483
196.415770
196.666057
196.916346
197.166633
197.416922
197.667209
197.917498
198.167785
198.418074
198.668361
198.918650
199.168937
199.419226
199.669513
199.919802
200.160089
200.410378
200.660665
200.910954
201.161243
201.411532
201.661821
201.912110
202.162399
202.412688
202.662977
202.913266
203.163555
203.413844
203.664133
203.914422
204.164711
204.415000
204.665289
204.915578
205.165867
205.416156
205.666445
205.916734
206.167023
206.417312
206.667601
206.917890
207.168179
207.418468
207.668757
207.919046
208.169335
208.419624
208.669913
208.910202
209.160491
209.410780
209.661069
209.911358
210.161647
210.411936
210.662225
210.912514
211.162803
211.413092
211.663381
211.913670
212.163959
212.414248
212.664537
212.914826
213.165115
213.415404
213.665693
213.915982
214.166271
214.416560
214.666849
214.917138
215.167427
215.417716
215.668005
215.918294
216.168583
216.418872
216.669161
216.919450
217.169739
217.410028
217.660317
217.910606
218.160895
218.411184
218.661473
218.911762
219.162051
219.412340
219.662629
219.912918
220.163207
220.413496
220.663785
220.914074
221.164363
221.414652
221.664941
221.915230
222.165519
222.415808
222.666097
222.916386
223.166675
223.416964
223.667253
223.917542
224.167831
224.418120
224.668409
224.918698
225.168987
225.419276
225.669565
225.919854
226.160143
226.410432
226.660721
226.911010
227.161299
227.411588
227.661877
227.912166
228.162455
228.412744
228.663033
228.913322
229.163611
229.413900
229.664189
229.914478
230.164767
230.415056
230.665345
230.915634
231.165923
231.416212
231.666501
231.916790
232.167079
232.417368
232.667657
232.917946
233.168235
233.418524
233.668813
233.919102
234.169391
234.419680
234.669969
234.910258
235.160547
235.410836
235.661125
235.911414
236.161703
236.412000
236.662289
236.912578
237.162867
237.413156
237.663445
237.913734
238.164023
238.414312
238.664601
238.914890
239.165179
239.415468
239.665757
239.916046
240.166335
240.416624
240.666913
240.917202
241.167491
241.417780
241.668069
241.918358
242.168647
242.418936
242.669225
242.919514
243.169803
243.410092
243.660381
243.910670
244.160959
244.411248
244.661537
244.911826
245.162115
245.412404
245.662693
245.912982
246.163271
246.413560
246.663849
246.914138
247.164427
247.414716
247.665005
247.915294
248.165583
248.415872
248.666161
248.916450
249.166739
249.417028
249.667317
249.917606
250.167895
250.418184
250.668473
250.918762
251.169051
251.419340
251.669629
251.919918
252.160207
252.410496
252.660785
252.911074
253.161363
253.411652
253.661941
253.912230
254.162519
254.412808
254.663097
254.913386
255.163675
255.413964
255.664253
255.914542
256.164831
256.415120
256.665409
256.915698
257.165987
257.416276
257.666565
257.916854
258.167143
258.417432
258.667721
258.918010
259.168299
259.418588
259.668877
259.919166
260.169455
260.419744
260.660033
260.910322
261.160611
261.410900
261.661189
261.911478
262.161767
262.412056
262.662345
262.912634
263.162923
263.413212
263.663501
263.913790
264.164079
264.414368
264.664657
264.914946
265.165235
265.415524
265.665813
265.916102
266.166391
266.416680
266.666969
266.917258
267.167547
267.417836
267.668125
267.918414
268.168703
268.418992
268.669281
268.919570
269.169859
269.410148
269.660437
269.910726
270.161015
270.411304
270.661593
270.911882
271.162171
271.412460
271.662749
271.913038
272.163327
272.413616
272.663905
272.914194
273.164483
273.414772
273.665061
273.915350
274.165639
274.415928
274.666217
274.916506
275.166795
275.417084
275.667373
275.917662
276.167951
276.418240
276.668529
276.918818
277.169107
277.419396
277.669685
277.919974
278.160263
278.410552
278.660841
278.911130
279.161419
279.411708
279.661997
279.912286
280.162575
280.412864
280.663153
280.913442
281.163731
281.414020
281.664309
281.914598
282.164887
282.415176
282.665465
282.915754
283.166043
283.416332
283.666621
283.916910
284.167199
284.417488
284.667777
284.918066
285.168355
285.418644
285.668933
285.919222
286.169511
286.419800
286.660089
286.910378
287.160667
287.410956
```


***	11.399245	***	-74.999985	***	-67.783478	***	-75.000000	***	-24.087524
***	11.589231	***	-10.854013	***	-11.366899	***	-75.000000	***	42.173767
***	11.779218	***	0.305608	***	-1.175964	***	-75.000000	***	-10.717773

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 FZ
9-19-84

*** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 2 OF 4

TIME.....(SEC) R/RT CMD...(DPS) ROLL RATE...(DPS) ECM SHIFT...(FT) GLINT SHIFT(FT)

11.969204	1.725770	***	-0.077368	***	-75.000000	***	21.826172
12.159190	1.766047	***	0.153380	***	-75.000000	***	-22.363281
12.349176	1.522860	***	0.138551	***	-75.000000	***	-15.866780
12.539163	1.307849	***	0.090493	***	75.000000	***	-47.924805
12.729149	1.175968	***	0.044148	***	75.000000	***	45.671082
12.919135	1.126412	***	0.008935	***	75.000000	***	-43.750000
13.109121	1.140405	***	0.015377	***	75.000000	***	15.857461
13.299108	1.198962	***	-0.031489	***	75.000000	***	32.354405
13.489094	1.287829	***	-0.049077	***	75.000000	***	-27.539063
13.679080	1.425424	***	-0.068103	***	75.000000	***	-42.953164
13.869066	1.591445	***	-0.075865	***	75.000000	***	37.622070
14.059052	1.777146	***	-0.078154	***	75.000000	***	-5.277191
14.249039	1.954254	***	-0.075742	***	75.000000	***	2.807617
14.439025	2.131940	***	-0.069467	***	75.000000	***	-5.204102
14.629011	2.456958	***	-0.060213	***	75.000000	***	-0.720215
14.818997	2.443621	***	-0.048666	***	75.000000	***	33.416748
15.008984	2.566847	***	-0.035191	***	75.000000	***	-33.823735
15.198970	2.663178	***	-0.032106	***	75.000000	***	-33.227533
15.388956	2.731251	***	-0.020707	***	75.000000	***	-14.042664
15.578942	2.777195	***	0.006111	***	75.000000	***	31.372070
15.768929	2.784501	***	0.017965	***	75.000000	***	22.955322
15.958915	2.773720	***	0.028139	***	75.000000	***	43.412781
16.148833	2.742187	***	0.036394	***	75.000000	***	-34.065247
16.338730	2.653789	***	0.042625	***	75.000000	***	2.059605
16.528622	2.632695	***	0.046833	***	75.000000	***	1.255770
16.718521	2.556311	***	0.045088	***	75.000000	***	-12.655513
16.908417	2.489133	***	0.049957	***	75.000000	***	-28.857422
17.098312	2.414161	***	0.048846	***	75.000000	***	-24.087524

```

***
17.2478104
17.6677995
17.8577991
18.0477916
18.2377827
18.4277582
18.6177373
18.8077265
19.0077164
19.1977060
19.3876951
19.5776847
19.7676742
20.0076635
20.2576533
20.5076432
20.7576332
21.0076231
21.2576130
21.5076029
21.7575928
22.0075827
22.2575726
22.5075625
22.7575524
23.0075423
23.2575322
23.5075221
23.7575120
24.0075019
24.2574918
24.5074817
24.7574716
25.0074615
25.2574514
25.5074413
25.7574312
26.0074211
26.2574110
26.5074009
26.7573908
27.0073807
27.2573706
27.5073605
27.7573504
28.0073403
28.2573302
28.5073201
28.7573100
29.0073000
29.2572900
29.5072800
29.7572700
30.0072600
30.2572500
30.5072400
30.7572300
31.0072200
31.2572100
31.5072000
31.7571900
32.0071800
32.2571700
32.5071600
32.7571500
33.0071400
33.2571300
33.5071200
33.7571100
34.0071000
34.2570900
34.5070800
34.7570700
35.0070600
35.2570500
35.5070400
35.7570300
36.0070200
36.2570100
36.5070000
36.7569900
37.0069800
37.2569700
37.5069600
37.7569500
38.0069400
38.2569300
38.5069200
38.7569100
39.0069000
39.2568900
39.5068800
39.7568700
40.0068600
40.2568500
40.5068400
40.7568300
41.0068200
41.2568100
41.5068000
41.7567900
42.0067800
42.2567700
42.5067600
42.7567500
43.0067400
43.2567300
43.5067200
43.7567100
44.0067000
44.2566900
44.5066800
44.7566700
45.0066600
45.2566500
45.5066400
45.7566300
46.0066200
46.2566100
46.5066000
46.7565900
47.0065800
47.2565700
47.5065600
47.7565500
48.0065400
48.2565300
48.5065200
48.7565100
49.0065000
49.2564900
49.5064800
49.7564700
50.0064600
50.2564500
50.5064400
50.7564300
51.0064200
51.2564100
51.5064000
51.7563900
52.0063800
52.2563700
52.5063600
52.7563500
53.0063400
53.2563300
53.5063200
53.7563100
54.0063000
54.2562900
54.5062800
54.7562700
55.0062600
55.2562500
55.5062400
55.7562300
56.0062200
56.2562100
56.5062000
56.7561900
57.0061800
57.2561700
57.5061600
57.7561500
58.0061400
58.2561300
58.5061200
58.7561100
59.0061000
59.2560900
59.5060800
59.7560700
60.0060600
60.2560500
60.5060400
60.7560300
61.0060200
61.2560100
61.5060000
61.7559900
62.0059800
62.2559700
62.5059600
62.7559500
63.0059400
63.2559300
63.5059200
63.7559100
64.0059000
64.2558900
64.5058800
64.7558700
65.0058600
65.2558500
65.5058400
65.7558300
66.0058200
66.2558100
66.5058000
66.7557900
67.0057800
67.2557700
67.5057600
67.7557500
68.0057400
68.2557300
68.5057200
68.7557100
69.0057000
69.2556900
69.5056800
69.7556700
70.0056600
70.2556500
70.5056400
70.7556300
71.0056200
71.2556100
71.5056000
71.7555900
72.0055800
72.2555700
72.5055600
72.7555500
73.0055400
73.2555300
73.5055200
73.7555100
74.0055000
74.2554900
74.5054800
74.7554700
75.0054600
75.2554500
75.5054400
75.7554300
76.0054200
76.2554100
76.5054000
76.7553900
77.0053800
77.2553700
77.5053600
77.7553500
78.0053400
78.2553300
78.5053200
78.7553100
79.0053000
79.2552900
79.5052800
79.7552700
80.0052600
80.2552500
80.5052400
80.7552300
81.0052200
81.2552100
81.5052000
81.7551900
82.0051800
82.2551700
82.5051600
82.7551500
83.0051400
83.2551300
83.5051200
83.7551100
84.0051000
84.2550900
84.5050800
84.7550700
85.0050600
85.2550500
85.5050400
85.7550300
86.0050200
86.2550100
86.5050000
86.7549900
87.0049800
87.2549700
87.5049600
87.7549500
88.0049400
88.2549300
88.5049200
88.7549100
89.0049000
89.2548900
89.5048800
89.7548700
90.0048600
90.2548500
90.5048400
90.7548300
91.0048200
91.2548100
91.5048000
91.7547900
92.0047800
92.2547700
92.5047600
92.7547500
93.0047400
93.2547300
93.5047200
93.7547100
94.0047000
94.2546900
94.5046800
94.7546700
95.0046600
95.2546500
95.5046400
95.7546300
96.0046200
96.2546100
96.5046000
96.7545900
97.0045800
97.2545700
97.5045600
97.7545500
98.0045400
98.2545300
98.5045200
98.7545100
99.0045000
99.2544900
99.5044800
99.7544700
100.0044600
100.2544500
100.5044400
100.7544300
101.0044200
101.2544100
101.5044000
101.7543900
102.0043800
102.2543700
102.5043600
102.7543500
103.0043400
103.2543300
103.5043200
103.7543100
104.0043000
104.2542900
104.5042800
104.7542700
105.0042600
105.2542500
105.5042400
105.7542300
106.0042200
106.2542100
106.5042000
106.7541900
107.0041800
107.2541700
107.5041600
107.7541500
108.0041400
108.2541300
108.5041200
108.7541100
109.0041000
109.2540900
109.5040800
109.7540700
110.0040600
110.2540500
110.5040400
110.7540300
111.0040200
111.2540100
111.5040000
111.7539900
112.0039800
112.2539700
112.5039600
112.7539500
113.0039400
113.2539300
113.5039200
113.7539100
114.0039000
114.2538900
114.5038800
114.7538700
115.0038600
115.2538500
115.5038400
115.7538300
116.0038200
116.2538100
116.5038000
116.7537900
117.0037800
117.2537700
117.5037600
117.7537500
118.0037400
118.2537300
118.5037200
118.7537100
119.0037000
119.2536900
119.5036800
119.7536700
120.0036600
120.2536500
120.5036400
120.7536300
121.0036200
121.2536100
121.5036000
121.7535900
122.0035800
122.2535700
122.5035600
122.7535500
123.0035400
123.2535300
123.5035200
123.7535100
124.0035000
124.2534900
124.5034800
124.7534700
125.0034600
125.2534500
125.5034400
125.7534300
126.0034200
126.2534100
126.5034000
126.7533900
127.0033800
127.2533700
127.5033600
127.7533500
128.0033400
128.2533300
128.5033200
128.7533100
129.0033000
129.2532900
129.5032800
129.7532700
130.0032600
130.2532500
130.5032400
130.7532300
131.0032200
131.2532100
131.5032000
131.7531900
132.0031800
132.2531700
132.5031600
132.7531500
133.0031400
133.2531300
133.5031200
133.7531100
134.0031000
134.2530900
134.5030800
134.7530700
135.0030600
135.2530500
135.5030400
135.7530300
136.0030200
136.2530100
136.5030000
136.7529900
137.0029800
137.2529700
137.5029600
137.7529500
138.0029400
138.2529300
138.5029200
138.7529100
139.0029000
139.2528900
139.5028800
139.7528700
140.0028600
140.2528500
140.5028400
140.7528300
141.0028200
141.2528100
141.5028000
141.7527900
142.0027800
142.2527700
142.5027600
142.7527500
143.0027400
143.2527300
143.5027200
143.7527100
144.0027000
144.2526900
144.5026800
144.7526700
145.0026600
145.2526500
145.5026400
145.7526300
146.0026200
146.2526100
146.5026000
146.7525900
147.0025800
147.2525700
147.5025600
147.7525500
148.0025400
148.2525300
148.5025200
148.7525100
149.0025000
149.2524900
149.5024800
149.7524700
150.0024600
150.2524500
150.5024400
150.7524300
151.0024200
151.2524100
151.5024000
151.7523900
152.0023800
152.2523700
152.5023600
152.7523500
153.0023400
153.2523300
153.5023200
153.7523100
154.0023000
154.2522900
154.5022800
154.7522700
155.0022600
155.2522500
155.5022400
155.7522300
156.0022200
156.2522100
156.5022000
156.7521900
157.0021800
157.2521700
157.5021600
157.7521500
158.0021400
158.2521300
158.5021200
158.7521100
159.0021000
159.2520900
159.5020800
159.7520700
160.0020600
160.2520500
160.5020400
160.7520300
161.0020200
161.2520100
161.5020000
161.7519900
162.0019800
162.2519700
162.5019600
162.7519500
163.0019400
163.2519300
163.5019200
163.7519100
164.0019000
164.2518900
164.5018800
164.7518700
165.0018600
165.2518500
165.5018400
165.7518300
166.0018200
166.2518100
166.5018000
166.7517900
167.0017800
167.2517700
167.5017600
167.7517500
168.0017400
168.2517300
168.5017200
168.7517100
169.0017000
169.2516900
169.5016800
169.7516700
170.0016600
170.2516500
170.5016400
170.7516300
171.0016200
171.2516100
171.5016000
171.7515900
172.0015800
172.2515700
172.5015600
172.7515500
173.0015400
173.2515300
173.5015200
173.7515100
174.0015000
174.2514900
174.5014800
174.7514700
175.0014600
175.2514500
175.5014400
175.7514300
176.0014200
176.2514100
176.5014000
176.7513900
177.0013800
177.2513700
177.5013600
177.7513500
178.0013400
178.2513300
178.5013200
178.7513100
179.0013000
179.2512900
179.5012800
179.7512700
180.0012600
180.2512500
180.5012400
180.7512300
181.0012200
181.2512100
181.5012000
181.7511900
182.0011800
182.2511700
182.5011600
182.7511500
183.0011400
183.2511300
183.5011200
183.7511100
184.0011000
184.2510900
184.5010800
184.7510700
185.0010600
185.2510500
185.5010400
185.7510300
186.0010200
186.2510100
186.5010000
186.7599900
187.0099800
187.2599700
187.5099600
187.7599500
188.0099400
188.2599300
188.5099200
188.7599100
189.0099000
189.2598900
189.5098800
189.7598700
190.0098600
190.2598500
190.5098400
190.7598300
191.0098200
191.2598100
191.5098000
191.7597900
192.0097800
192.2597700
192.5097600
192.7597500
193.0097400
193.2597300
193.5097200
193.7597100
194.0097000
194.2596900
194.5096800
194.7596700
195.0096600
195.2596500
195.5096400
195.7596300
196.0096200
196.2596100
196.5096000
196.7595900
197.0095800
197.2595700
197.5095600
197.7595500
198.0095400
198.2595300
198.5095200
198.7595100
199.0095000
199.2594900
199.5094800
199.7594700
200.0094600
200.2594500
200.5094400
200.7594300
201.0094200
201.2594100
201.5094000
201.7593900
202.0093800
202.2593700
202.5093600
202.7593500
203.0093400
203.2593300
203.5093200
203.7593100
204.0093000
204.2592900
204.5092800
204.7592700
205.0092600
205.2592500
205.5092400
205.7592300
206.0092200
206.2592100
206.5092000
206.7591900
207.0091800
207.2591700
207.5091600
207.7591500
208.0091400
208.2591300
208.5091200
208.7591100
209.0091000
209.2590900
209.5090800
209.7590700
210.0090600
210.2590500
210.5090400
210.7590300
211.0090200
211.2590100
211.5090000
211.7589900
212.0089800
212.2589700
212.5089600
212.7589500
213.0089400
213.2589300
213.5089200
213.7589100
214.0089000
214.2588900
214.5088800
214.7588700
215.0088600
215.2588500
215.5088400
215.7588300
216.0088200
216.2588100
216.5088000
216.7587900
217.0087800
217.2587700
217.5087600
217.7587500
218.0087400
218.2587300
218.5087200
218.7587100
219.0087000
219.2586900
219.5086800
219.7586700
220.0086600
220.2586500
220.5086400
220.7586300
221.0086200
221.2586100
221.5086000
221.7585900
222.0085800
222.2585700
222.5085600
222.7585500
223.0085400
223.2585300
223.5085200
223.7585100
224.0085000
224.2584900
224.5084800
224.7584700
225.0084600
225.2584500
225.5084400
225.7584300
226.0084200
226.2584100
226.5084000
226.7583900
227.0083800
227.2583700
227.5083600
227.7583500
228.0083400
228.2583300
228.5083200
228.7583100
229.0083000
229.2582900
229.5082800
229.7582700
230.0082600
230.2582500
230.5082400
230.7582300
231.0082200
231.2582100
231.5082000
231.7581900
232.0081800
232.2581700
232.5081600
232.7581500
233.0081400
233.2581300
233.5081200
233.7581100
234.0081000
234.2580900
234.5080800
234.7580700
235.0080600
235.2580500
235.5080400
235.7580300
236.0080200
236.2580100
236.5080000
236.7579900
237.0079800
237.2579700
237.5079600
237.7579500
238.0079400
238.2579300
238.5079200
238.7579100
239.0079000
239.2578900
239.5078800
239.7578700
240.0078600
240.2578500
240.5078400
240.7578300
241.0078200
241.2578100
241.5078000
241.7577900
242.0077800
242.2577700
242.5077600
242.7577500
243.0077400
243.2577300
243.5077200
243.7577100
244.0077000
244.2576900
244.5076800
244.7576700
245.0076600
245.2576500
245.5076400
245.7576300
246.0076200
246.2576100
246.5076000
246.7575900
247.0075800
247.2575700
247.5075600
247.7575500
248.0075400
248.2575300
248.5075200
248.7575100
249.0075000
249.2574900
249.5074800
249.7574700
250.0074600
250.2574500
250.5074400
250.7574300
251.0074200
251.2574100
251.5074000
251.7573900
252.0073800
252.2573700
252.5073600
252.7573500
253.0073400
253.2573300
253.5073200
253.7573100
254.0073000
254.2572900
254.5072800
254.7572700
255.0072600
255.2572500
255.5072400
255.7572300
256.0072200
256.2572100
256.5072000
256.7571900
257.0071800
257.2571700
257.5071600
257.7571500
258.0071400
258.2571300
258.5071200
258.7571100
259.0071000
259.2570900
259.5070800
259.7570700
260.0070600
260.2570500
260.5070400
260.7570300
261.0070200
261.2570100
261.5070000
261.7569900
262.0069800
262.2569700
262.5069600
262.7569500
263.0069400
263.2569300
263.5069200
263.7569100
264.0069000
264.2568900
264.5068800
264.7568700
265.0068600
265.2568500
265.5068400
265.7568300
266.0068200
266.2568100
266.5068000
266.7567900
267.0067800
267.2567700
267.5067600
267.7567500
268.0067400
268.2567300
268.5067200
268.7567100
269.0067000
269.2566900
269.5066800
269.7566700
270.0066600
270.2566500
270.5066400
270.7566300
271.0066200
271.2566100
271.5066000
271.7565900
272.0065800
272.2565700
272.5065600
272.7565500
273.0065400
273.2565300
273.5065200
273.7565100
274.0065000
274.2564900
274.5064800
274.7564700
275.0064600
275.2564500
275.5064400
275.7564300
276.0064200
276.2564100
276.5064000
276.7563900
277.0063800
277.2563700
277.5063600
277.7563500
278.0063400
278.2563300
278.5063200
278.7563100
279.0063000
279.2562900
279.5062800
279.7562700
280.0062600
280.2562500
280.5062400
280.7562300
281
```


TIME.....(SEC)	R/RT CMC...(CPS)	ROLL RATE...(DPS)	ECM SHIFT...(FT)	GLINT SHIFT(FT)
24.314346	74.995985	65.562851	75.000000	-43.750000
24.504242	74.995985	65.786819	75.000000	-15.897461
24.654138	74.995985	65.964462	75.000000	-32.354409
24.840333	74.995985	66.055204	75.000000	-27.539063
25.073925	74.995985	66.085938	75.000000	-42.953164
25.263824	74.995985	66.059158	75.000000	-37.622070
25.453720	22.935425	22.956116	75.000000	-5.271912
25.643616	-5.669250	-6.440586	75.000000	-2.807617
25.833511	-10.200819	-10.561381	75.000000	-9.204102
26.023407	-13.224416	-14.461498	75.000000	-0.720215
26.213303	-17.424454	-17.331482	75.000000	-3.416748
26.403158	-1.460428	-13.733393	75.000000	-5.682373
26.593094	12.643291	-13.444024	75.000000	-33.227535
26.782990	3.271104	0.505555	75.000000	-14.042664
26.972885	-7.714266	-9.377487	75.000000	-13.372070
27.162781	40.710358	33.784058	75.000000	22.955322
27.352676	53.080215	44.795210	75.000000	43.412781
27.542572	66.124893	25.035751	75.000000	-34.065247
27.732468	74.995985	63.833176	75.000000	31.209960
27.922363	74.995985	62.675156	75.000000	31.255776
28.112255	74.995985	61.318130	75.000000	-12.655313
28.302155	74.995985	58.976955	75.000000	-28.857422
28.492050	74.995985	56.138641	75.000000	-24.087524
28.681946	74.995985	54.246460	0.000000	42.173767
28.871841	43.046890	24.955106	0.000000	-10.717773
29.061737	-38.403168	-41.171707	0.000000	21.826172

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 9-19-84

*** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AILRCN.....(DEG) RUDDER.....(DEG) ALTITUDE....(FT)

TIME.....(SEC)	STBLTR.....(DEG)	AIRLON.....(DEG)	RUDDER.....(DEG)	ALTITUDE....(FT)
9.119411	3.569754	-3.22716	0.192114	41.688568
9.309397	-3.802303	-3.288725	0.248152	41.337570
9.499383	-3.889286	-3.262568	0.364863	41.600983
9.689365	-3.815103	-3.148677	0.489636	42.873740
9.879355	-3.543250	-2.976035	0.613086	43.858743
10.069342	-3.206109	-2.761302	0.718114	45.777054
10.259328	-2.801994	-2.526126	0.790657	47.981018
10.449314	-2.403330	-2.292121	0.826747	50.369045
10.639300	-2.053359	-2.077678	0.831036	52.759927
10.829287	-2.769983	-2.031552	0.837751	55.198746
11.019273	3.203503	-1.638245	0.107612	57.602005
11.209255	3.445362	-1.337570	-0.511320	60.053918
11.399245	3.550609	-1.067041	-0.863214	62.670746
11.589231	-0.761881	-0.860477	-1.133111	65.250519
11.779218	-0.806800	-0.768132	-1.088782	67.735687

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

*** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AIRLON.....(DEG) RUDDER.....(DEG) ALTITUDE....(FT)

11.969204	-0.915540	-0.65329	-0.792145	70.043457
12.159190	-0.818488	-0.525124	-0.461040	72.077484
12.349176	-0.699540	-0.417514	-0.218913	73.742950
12.539163	-0.612691	-0.339986	-0.095435	74.960114
12.729149	-0.566952	-0.305909	-0.054526	75.877820
12.919135	-0.557567	-0.324278	-0.055930	75.877914
13.109121	-0.575181	-0.376057	-0.073167	75.567383
13.299108	-0.611483	-0.457703	-0.093069	74.777695
13.489094	-0.661711	-0.561647	-0.110690	73.558517
13.679080	-0.739960	-0.676090	-0.125492	71.971645
13.869066	-0.826459	-0.795570	-0.138116	70.086105
14.059052	-0.917423	-0.928560	-0.148669	67.978912
14.249038	-1.008072	-1.056622	-0.156873	65.730785
14.439025	-1.094344	-1.177841	-0.162443	63.421967
14.629011	-1.172998	-1.287473	-0.165273	61.128418
14.818999	-1.241513	-1.381750	-0.165445	58.919155

GLINT PLUS ECM AT 0.2 HZ 9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 4 OF 4

TIME.....(SEC) XM....(FT NORTH) YM.....(FT EAST) XT....(FT NORTH) XM....(FT EAST)

0.190000	159.440155	11275.4	09810	24000.0	6.499995
0.380000	1318.301758	1115.991460	-0.049694	24000.0	13.299998
0.570000	478.301758	637.728271	-0.113570	24000.0	15.299998
0.759995	797.151611	956.573486	-0.201762	24000.0	26.559997
0.949995	1115.991460	11275.4	-0.313580	24000.0	33.289996
1.139997	1115.991460	11275.4	-0.448021	24000.0	35.549118
1.329997	11275.4	637.728271	-0.603947	24000.0	46.158635
1.519996	11275.4	637.728271	-0.779674	24000.0	53.158635
1.709994	11434.820310	11275.4	-0.973391	24000.0	59.848160
1.899934	1594.328760	11275.4	-1.182681	24000.0	66.457681
2.089920	1753.032470	11275.4	-1.404678	24000.0	73.147207
2.279906	1913.032470	11275.4	-1.636795	24000.0	79.756707
2.469893	2072.426510	11275.4	-1.876554	24000.0	86.446228
2.659879	2231.814940	11275.4	-2.120413	24000.0	93.055745
2.849865	2391.157750	11275.4	-2.362842	24000.0	99.745270
3.039851	2550.574710	11275.4	-2.597082	24000.0	106.354779
3.229837	2709.944090	11275.4	-2.816305	24000.0	113.044296
3.419824	2869.307860	11275.4	-3.014330	24000.0	119.693381
3.609810	3028.665530	11275.4	-3.185804	24000.0	126.343333
3.799796	3188.016360	11275.4	-3.332030	24000.0	133.952385
3.989782	3347.361330	11275.4	-3.499740	24000.0	141.251885
4.179765	3506.700270	11275.4	-3.652645	24000.0	148.941406
4.369741	3666.032710	11275.4	-3.808789	24000.0	156.550927
4.559727	3825.359620	11275.4	-3.954332	24000.0	164.240448
4.749713	3984.681400	11275.4	-4.103370	24000.0	172.899905
4.939699	4143.994370	11275.4	-4.251335	24000.0	180.594990
5.129686	4303.257810	11275.4	-4.398205	24000.0	188.299556
5.319672	4462.531250	11275.4	-4.546663	24000.0	196.003167
5.509658	4621.804690	11275.4	-4.695534	24000.0	203.715585
5.699645	4781.078120	11275.4	-4.844940	24000.0	211.427075
5.889631	4940.351560	11275.4	-4.995940	24000.0	219.138584
6.079617	5099.625000	11275.4	-5.147527	24000.0	226.850105
6.269603	5258.898440	11275.4	-5.299145	24000.0	234.561626
6.459589	5418.171870	11275.4	-5.450763	24000.0	242.273147
6.649575	5577.445310	11275.4	-5.602381	24000.0	250.084668


```

** ** ** ** **
6.839576 736.703120 0.485856 24000.000000 39.0365147
7.029562 5895.902340 1.105633 24000.000000 46.684174
7.219548 6055.101560 1.785213 24000.000000 52.6333496
7.409534 6214.300780 2.594645 24000.000000 59.9831548
7.599521 6373.500000 3.660096 24000.000000 63.632568
7.789507 6532.699220 5.144712 24000.000000 72.2831641
7.979493 6691.023440 7.235577 24000.000000 79.9312641
8.169479 6851.023440 10.115355 24000.000000 85.9310553
8.359466 7010.148440 14.135207 24000.000000 92.5810713
8.549452 7169.210940 19.605545 24000.000000 99.2801275
8.739438 7328.160160 26.823133 24000.000000 105.5297857
8.929424 7486.953120 36.051483 24000.000000 112.1791959
9.119411 7645.527340 47.457543 24000.000000 119.8288571
9.309397 7803.820310 61.294495 24000.000000 125.4782711
9.499383 7961.785160 77.494766 24000.000000 131.1770846
9.689369 8119.371090 96.093333 24000.000000 137.1277344
9.879355 8276.554690 116.994876 24000.000000 143.4267568
10.069342 8433.335940 139.994876 24000.000000 149.726416
10.259328 8589.730470 164.924744 24000.000000 156.0258330
10.449314 8745.746090 191.672058 24000.000000 162.3254888
10.639300 8901.429690 219.995642 24000.000000 168.6249026
10.829287 9056.800780 249.667542 24000.000000 174.924316
11.019273 9211.929690 280.360840 24000.000000 181.2239755
11.209259 9366.850620 311.764160 24000.000000 187.5233389
11.399245 9521.742190 343.555176 24000.000000 193.8230471
11.589231 9676.562500 375.463623 24000.000000 200.1227461
11.779218 9831.382810 407.341797 24000.000000 206.422461

```

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 9-19-84

** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 4 OF 4

TIME... (SEC) XM... (FT NORTH) YM... (FT EAST) XT... (FT NORTH) XM... (FT EAST)

```

** ** ** **
11.969204 * 9986.203120 * 439.127930 * 24000.000000 * 418.922119
12.159190 * 10141.023400 * 470.755654 * 24000.000000 * 425.571533
12.349176 * 10295.843700 * 502.336670 * 24000.000000 * 432.220947
12.539163 * 10450.683600 * 533.751709 * 24000.000000 * 438.877005

```


TIME.....(SEC)	XM... (FT NORTH)	YM... (FT EAST)	XT... (FT NORTH)	XM... (FT EAST)	DATA SET NUMBER	UF
21.845703	18066.9	10200	1770.7	707280	24000.0	000000
22.035595	18221.2	03100	1767.5	811790	24000.0	000000
22.225494	18375.4	29700	1762.4	311400	24000.0	000000
22.415390	18529.6	09400	1755.4	13820	24000.0	000000
22.605286	18683.7	22700	1746.5	58110	24000.0	000000
22.795181	18837.7	46100	1735.8	56970	24000.0	000000
22.985077	18991.0	44500	1725.4	93900	24000.0	000000
23.174973	19145.4	02300	1709.4	31880	24000.0	000000
23.364868	19299.0	07800	1693.8	09570	24000.0	000000
23.554764	19452.4	37500	1676.7	30710	24000.0	000000
23.744659	19605.6	95300	1658.2	95170	24000.0	000000
23.934555	19758.7	85200	1638.6	00340	24000.0	000000
24.124451	19911.6	99200	1617.7	746830	24000.0	000000

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

*** BLINKER FREQUENCY= 0.20

TIME.....(SEC) XM... (FT NORTH) YM... (FT EAST) XT... (FT NORTH) XM... (FT EAST)

24.314346	20064.4	60900	1555.8	48880	24000.0	000000
24.504242	20217.0	89800	1573.0	31490	24000.0	000000
24.694138	20369.6	17200	1549.4	32370	24000.0	000000
24.884033	20522.0	62500	1525.1	58730	24000.0	000000
25.073924	20674.4	41400	1500.4	484370	24000.0	000000
25.263824	20826.8	12500	1475.4	40190	24000.0	000000
25.453720	20979.1	83600	1450.2	01660	24000.0	000000
25.643616	21131.5	78100	1424.8	48630	24000.0	000000
25.833511	21284.0	23400	1399.4	23830	24000.0	000000
26.023407	21436.5	27300	1373.9	27490	24000.0	000000
26.213303	21589.0	078100	1348.3	37400	24000.0	000000
26.403198	21741.6	71900	1322.6	15970	24000.0	000000
26.593094	21894.3	39800	1296.7	26810	24000.0	000000
26.782990	22047.0	39100	1270.6	28660	24000.0	000000
26.972885	22199.7	81200	1244.2	85160	24000.0	000000
27.162781	22352.5	66400	1217.6	80910	24000.0	000000
27.352676	22505.3	50600	1190.8	84520	24000.0	000000
27.542572	22658.2	85200	1164.0	029050	24000.0	000000

27.732468
27.911225
28.130215
28.345205
28.481946
28.671841
28.871737

22811.2361700
22914.343700
23117.585900
23271.027300
23424.718700
23578.683600
23732.902300
23887.324200

11137.286223
11085.108890
1060.465970
1037.558840
1017.097900
999.782715
986.245850

*24000.000000
*24000.000000
*24000.000000
*24000.000000
*24000.000000
*24000.000000
*24000.000000

970.627153
977.282715
983.928955
990.527519
997.221680
1003.867920
1010.514400
1017.160640

TASM SIMULATION PROGRAM NCMENCLATURE

[illegible]

U,V,W	BODY AXIS	VELOCITIES	(FT/SEC)
UDDCT,VDDT,WDGT	BODY AXIS	LINEAR ACCELERATIONS	
PP,C,R	BODY AXIS	ANGULAR VELOCITIES	(RAD/SEC)
PRCCLRT,PTCHRT,YAWRT	BODY AXIS	ANGULAR VELOCITIES	(DEG/SEC)
PDCT,QDOT,RDOT	BODY AXIS	ANGULAR ACCELERATIONS	
X,Y,Z	BODY AXIS	AERODYNAMIC FORCES	(LBS)
L,L,L	LIFT, DRAG	AERODYNAMIC FORCES	(LBS)
MA,NA	BODY AXIS	AERODYNAMIC MOMENTS	(FT-LBS)
PHI,THETA,SY	EULER ANGLES	(RAD)	
BANK,PITCH,HEADNG	"	(DEG)	
PHICOT,THETAD,SYDOT	"	RATE OF CHANGE OF	
ALFA,BETA	ANGLE OF ATTACK, SIDESLIP	(RAD)	
ACA,SICESL	"	"	(DEG)
ALFADT,BETADT	RATE OF CHANGE OF ALFA, BETA	(RAD)	
GAMMA	FLIGHT PATH ANGLE	(DEG)	
FLTPTH	"	(DEG)	
Y,NZ	LATERAL ACCELERATION, LOAD FACTOR	(G'S)	
XY,N,YM,ALTUDE	EARTH COORDINATES OF MISSILE	(FT)	
XMCT,YMDOT,HMDOT	(KM-NORTH, YM-EAST)		
VT	RATES OF CHANGE OF XM, YM, ALTITUDE		
CHCRD,SPAN	TOTAL MISSILE VELOCITY	(FT/SEC)	
CHCRD2,SPAN2	MEAN AERODYNAMIC CHORD, SPAN	(FT)	
	HALF CHORD, HALF SPAN		

WT,M,G	GROSS WEIGHT, MASS, ACCEL DUE TO GRAVITY
T,S	THRUST, WING AREA
RFC	AIR DENSITY
QS	DYNAMIC PRESSURE X WING AREA
C--	AERODYNAMIC COEFFICIENTS
DC--	INCREMENTS IN "
IXX,IYY,IZZ,IXZ	MOMENTS AND PRODUCTS OF INERTIA
IA- IK	FUNCTIONS OF "
ELE,AIRL,RUD	STANDARD CONTROL DEFLECTIONS (DEG)
STBLTR,AIRLON,RUDDER	CONTROL DEFLECTIONS WITH LIMITS
	APPLIED (DEG)
RSTABL,LSTABL	TASM UNLIMITED CONTROL DEFLECTIONS (DEG)
RSTAB,LSTAB	TASM LIMITED CONTROL DEFLECTIONS (DEG)
---	INITIAL CONDITION

AUTCFILOTT

K---	AUTOPILLOT GAINS
CGARM-	ACCELEROMETER LOCATION WRT CG
E---	COMPARATOR ERRORS
---	LIMITED VALUES
---	SERVO INPUTS
---	SERVO OUTPUTS
---	COMMANDED VALUES
---	FILTERED SENSOR VARIABLE
FNCCF-,FDCOF-	NOTCH FILTER COEFFICIENTS

GUIDANCE

AZC,AYC	COMMANDED VERTICAL AND HORIZONTAL
XT,YT,HT	ACCELERATIONS IN EARTH AXES (G'S)
XR,YR,HR	EARTH COORDINATES OF TARGET (FT)
	POSITION OF THE TARGET WRT MISSILE IN
XRECM,YRECM,HRECM	EARTH COORDINATES (FT)
	POSITION OF RADAR TARGET (XR,YR,HR WITH ECM
	AND GLINT ADDED WRT MISSILE (FT)
XDCTR,YDCTR,HDCTR	RATES OF CHANGE CF XRECM,YRECM,HRECM (FT/S)
	(RELATIVE VELOCITY OF TGT WRT MISSILE)
XECM,YECM,HECM	INCR. IN TARGET RADAR POSITION DUE TO ECM
XGLNT,YGLNT,HGLNT	INCR. IN TARGET RADAR POSITION DUE TO GLINT
RANGE	RANGE TO TARGET (FT)
RNGECM,RGECMT	RANGE TO RADAR TARGET (TGT WITH ECM+GLINT)
TSPEED	TARGET SPEED (FT/SEC)
SYT,THETAT	HEADING, ELEV. TGT
HEADT,ELEV	HEADING, ELEV. TGT
VTANAZ,VTANEL	CUMULATIVE RELATIVE VELOCITY
	TU, LUS IN AZIMUTH AND ELEVATION (FT/SEC)
TRAKAZ,TRAKEL	COMPONENT OF MISSILE VELOCITY VECTOR IN

SIGAZ, SIGEL
 DSIGAZ, DSIGEL
 SIGDAZ, SIGDEL
 DSGCAZ, DSGDEL
 SIGDAF, SIGDEF
 DSGCAF, DSGDEF
 LAMCAZ, LAMDEL
 FREQ
 SHIFTY, SHIFT
 BRNTHR
 KNFAZ, KNFEL
 AZIMUTH AND ELEVATION (FT/SEC)
 EARTH AZIMUTH, ELEVATION LOS ANGLES (RAD)
 EARTH AZIMUTH, ELEVATION LOS ANGLES (DEG)
 RATES OF CHANGE OF EARTH REFERENCED LOS
 (RAD/SEC)
 SAME AS ABOVE (DEG/SEC)
 FILTERED SIGDAT, SIGDET (RAD/SEC)
 FILTERED DSGCAT, DSGDET (DEG/SEC)
 PROPORTIONAL NAVIGATION CONSTANTS
 FREQUENCY OF ECM BLINKING
 DISTANCE OF ECM BLINKER FROM TARGET AIM
 POINT (FT)
 BURN-THROUGH RANGE
 AZIMUTH AND ELEVATION NAVIGATION FILTER
 CONSTANTS

APPENDIX D

MAIN PROGRAM LISTING FOR TACTICAL CRUISE MISSILE SIMULATION

TRANSLATED BY
CDR BARTON P. ANDERSON, USN

NAVY POSTGRADUATE SCHOOL
DEPARTMENT OF AERONAUTICAL ENGINEERING
MCNTEREY, CA 93943

TRANSLATED FROM CSMP PROGRAM BY
DR. MARLE HEWETT
LCDR KENT WATTERSON, USN

PROGRAM TCMC

CONTROLS THE OVERALL EXECUTION OF THE SIMULATION. CALLS THE
NECESSARY SUBROUTINES, DETERMINES WHEN THE DATA MUST BE STORED
FOR OUTPUT AND WHEN THE RUN HAS COMPLETED DUE TO CPA OR FINTIM.

9-10-84

IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NOUT,PCOUNT,NFAZE

COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS

COMMON /A/ TIME , FINTIM,DT ,CPUT ,NCUT ,NPTS ,CPA ,PCOUNT,
G , IXX , IYY , IZZ , IXXZ , IIA , IIB , IIC , IS ,
ID , IE , IF , IG , IJ , IK ,
CHORD2,CHORD ,SPAN2,SPAN ,NFAZE

COMMON BLOCK /H/: ECM/GLINT PARAMETERS

```

C
COMMON /H/  FREQ      ,SHIFTH  ,BRNTHR ,
             XECM      ,HECM     ,XGLNT  ,
             YGLNT     ,XTECM    ,YTECM   ,
             HTECM     ,          ,
*
*
*
*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****
COMMON /F/  PH1      ,PH2      ,PH3      ,PH4      ,
             OFFSET  ,ALTATT   ,SGDZPU  ,MISDST  ,
             LAMCAZ  ,LAMDEL   ,KNFAZ   ,KNFEL   ,
             NZC     ,PHIC     ,GAMMAC   ,PCLIM   ,
             PC      ,QC       ,RC       ,RANGE   ,
             SIGAZ   ,SIGEL    ,SIGCAF   ,SIGDEF  ,
             SYT     ,THETAT   ,XT       ,YT      ,
             HT      ,NYC      ,POPRNG  ,          ,
*
*
*
*****
COMMON BLOCK /I/: CUTPUT ARRAY
*****
COMMON /I/  PTS(300,20)
*****
*****
**  INITIALIZE ALL VARIABLES
*****
PLCTTING SURFACE
CALL TEK618
CALL CCMPRS
CALL SWISSM
1 CALL INIT
**  BEGIN DYNAMIC SIMULATION
*****
*****
10 IF (CPA.GE.1.0) GO TO 100
   TIME=TIME+DT
   IF (TIME.GE.FINTIM) CPA=2.0
   PCCUNT = PCCUNT+1
*****
*****
**  FROM MISSION PROFILE/GUIDANCE, GENERATE NZC,PHIC

```

```

C      CALL MISSN1
C
C      *** GENERATE CONTROL MOVEMENTS: STBLTR, AILRON, RUDDER
C      CALL APILOT
C
C      *** GENERATE MISSILE MCTION AND POSITION
C      CALL AERO
C
C      *** GENERATE APPARENT RADAR TARGET POSITION & MCTION
C      CALL TGTNAV
C
C      *** STCRE REQUIRED PLOT DATA IN THE PTS ARRAY.
C      IF (PCOUNT.LT.NCOUT) GO TO 50
C      CALL PREPAR
C      PCOUNT = 0.0
C      50 CONTINUE
C      GC TO 10
C      100 CONTINUE
C      *** END DYNAMIC SIMULATION *****
C      *** INVOKE DISPLA AND TABULAR OUTPUT ROUTINES
C      CALL CLTPUT(NPTS,CPA)
C      ***** TESTPATCH TO BYPASS ITERATIONS (KTEST = 1)
C      KTEST = 0
C      IF (KTEST.EQ.1) GC TO 150
C      ***** ENDTEST
C      *** ITERATE THE PHASE VARIABLE IN THE ECM PACKAGE
C      NFAZE = NFAZE + 1
C      IF (NFAZE.LE.4) GO TO C 1
C      NFAZE = 1
C

```



```

C
**      AOA1      PITCHR1      ROLLR1      YAWR1      ,
**      XT1      ,YT1      ,HT1      ,TSPEED      ,
C
COMMON /F/ PH1 OFF SET      PH3      PH4      ,
*      LAMDAZ      ,ALTAIT      ,SGDZPU      ,MISDST      ,
*      NZC      ,LAMDEL      ,KNFAZ      ,KNFEL      ,
*      PC      ,PHIC      ,GAMMAC      ,PC LIM      ,
*      SIGAZ      ,QC      ,RC      ,RANGE      ,
*      SYT      ,SIGEL      ,SIGDEF      ,
*      HT      ,THETAT      ,YT      ,
C
COMMON /H/ FREQ      SHIFTY      SHIFTH      BRNTHR      ,
*      XECM      ,YECM      ,HECM      ,XGLNT      ,
*      YGLNT      ,HGLNT      ,XTECM      ,
C
COMMON /I/ PTS(300,20)
C
EXECUTABLE STMTS *****
C
** COMPUTEL CONSTANTS
C
PI I= 18C.0/PI
IA = IXX*IZZ-IXZ**2
IB = IZZ/IA
IC = IXX/IA
ID = IXX*(IYY-IXX-IZZ)/IA
IE = (IZZ**2-IYY*IZZ+IXZ**2)/IA
IF = I/ IYY
IG = (IXX-IZZ)/IYY
IH = IXX/IYY
II = IXX/IA
IJ = (IXX*IYY-IXX**2-IXZ**2)/IA
IK = (IXX+IZZ-IYY)*IXZ/IA
C
PLIM = RRLIM/PI I
C
*****
C
PARAMETERS TO BE INITIALIZED FOR EACH RUN FOLLOW.
*****
C
TIME = C.0
CPA = 0
PCCUNT = 0
NOUT = INT(CPDT/DT)
IF (AMGC(CPDT,DT)).GE.0.5) NOUT=NOUT+1
*****

```

```

C      NP TS = C
      DO 100 I=1,300
      DC 50 J=1,20
      PTS(I,J) = 0.0
      CCNT INLE
      50 CONTINUE
      100 CONTINUE
C      U = L1
      W = L1*TAN(AOAL/PII)
      V = SQR(U1**2+W**2)*TAN(SIDES1/PII)
      VT = SQR(U**2+V**2+W**2)
      QS = 12.0*RHO*(VT**2)/2.0
C      P = RCLLRI/PII
      Q = FTCHRI/PII
      R = YAWRI/PII
C      PDCT = 0.0
      QDCT = 0.0
      RDOT = 0.0
C      THETA = PITCH1/PII
      PHI = BANK1/PII
      SY = HEDNG1/PII
      GAMMA = 0.0
      NZ = 1.0
C      XM = XM1
      YM = YM1
      ALTUDE = ALTUD1
C      AOA = ACAL
      ALFA = ACAL/PII
      ALFADT = 0.0
C      SIDESL = SIDES1
      BETA = SIDES1/PII
      BETADT = 0.0
C      XT = XT1
      YT = YT1
      HT = HT1
      RANGE = SQR((XT-XM)**2+(YT-YM)**2+(HT-ALTUDE)**2)
C      PH1 = 0
      PH2 = C

```



```

**          YGLNT      ,HGLNT      ,XTECM      ,YTECM      ,
**          FTECM
C C C C C
*****
COMMON BLOCK / I/: OUTPUT ARRAY
*****
COMMON / I/ PTS(300,20),PLTN(6,7),XN(6,7),YN(6,7),TITLE(8,4),
*          LEG(4,20)
C C C C C
*****
INITIALIZE THE DATA
*****
COMMON ELCCCK / A/: MISCELLANEOUS CONSTANTS
*****
DATA      TIME      ,FINTIM ,DT      ,CPA      /
*          /0.0      ,30.0      ,0.01      ,0.20      ,0
DATA      C          ,T          ,RHU      ,PI      ,WT      ,MASS
*          /32.17      ,242.3      ,.002377      ,3.141593      ,2200.      ,68.38      /
DATA      IXX      ,IYY      ,IZZ      ,IXZ      ,S          /
*          /27.8      ,1507.0      ,1512.0      ,11.7      ,12.0      ,
DATA      CHURD2,CHORD      ,SPAN2      ,SPAN      ,NFAZE      /
*          /0.707      ,1.414      ,4.2425      ,8.485      ,1
C C C C C
*****
COMMON ELCCCK / B/: AERODYNAMIC COEFFICIENT TABLES
*****
** STATIC AERODYNAMIC CCEFFICIENTS
* 1. LIFT COEFFICIENT DATA
A. CLBAS VS. AOA (BASIC LIFT CCEFFICIENT AS A FUNCTION
CF ANGLE OF ATTACK)
DATA LFT1/ -12.0,-0.32, -11.0,-0.29, -10.0,-0.46, -9.0,-0.57,
*          -8.0,-0.70, -7.0,-0.69, -6.0,-0.65, -5.0,-0.58,

```



```

* * * * *
-4.0,-0.50, -3.0,-0.42, -2.0,-0.30, -1.0,-0.18,
0.0,-0.08, 1.0,0.04, 2.0,0.15, 3.0,0.25,
4.0,0.36, 5.0,0.47, 6.0,0.58, 7.0,0.69,
8.0,0.80, 9.0,0.87, 10.0,0.78, 11.0,0.70,
12.0,0.64, 22*9999.0/

```

C C C C C

B. DCLSTE VS. STBLTR (INCREMENT IN LIFT COEFFICIENT
DUE TO SYMMETRIC STABILATOR DEFLECTION)

```

DATA LFT2/ -15.0,-100, -14.0,-0.97, -13.0,-0.94, -12.0,-0.90,
-11.0,-0.84, -10.0,-0.78, -9.0,-0.71, -8.0,-0.65,
-7.0,-0.59, -6.0,-0.48, -5.0,-0.40, -4.0,-0.32,
-3.0,-0.24, -2.0,-0.16, -1.0,-0.08, 0.0,0.00,
1.0,0.04, 2.0,0.16, 3.0,0.24, 4.0,0.33,
5.0,0.41, 6.0,0.49, 7.0,0.57, 8.0,0.65,
9.0,0.73, 10.0,0.80, 11.0,0.86, 12.0,0.92,
13.0,0.96, 14.0,0.98, 15.0,1.00, 10*9999. /
* * * * *

```

C C C C C C C

* 2. DRAG COEFFICIENT DATA

A. CDBAS VS. CLBAS (BASIC DRAG COEFFICIENT AS A FUNCTION
OF BASIC LIFT COEFFICIENT)

```

DATA DRG1/ -9, -0.80, -8, -0.61, -7, -0.50, -6, -0.42,
-5, -0.35, -4, -0.31, -3, -0.26, -2, -0.23,
-1, -0.22, 0, -0.22, 0.1, -0.23, 0.2, -0.24,
0.3, -0.25, 0.4, -0.31, 0.5, -0.36, 0.6, -0.42,
0.7, -0.49, 0.8, -0.57, 0.9, -0.68, 1.0, -0.80,
32*9999. /
* * * * *

```

C C C C C

B. LCDSTE VS. STBLTR (INCREMENT IN DRAG COEFFICIENT
DUE TO SYMMETRIC STABILATOR DEFLECTION)

```

DATA DRG2/ -15.0,-0.106, -14.0,-0.091, -13.0,-0.077, -12.0,-0.05,
-10.0,-0.044, -9.0,-0.036, -8.0,-0.028, -7.0,-0.022,
-6.0,-0.016, -5.0,-0.011, -4.0,-0.007, -3.0,-0.003,
-2.0,-0.001, -1.0,0.001, 0.0,0.001, 1.0,0.001,
2.0,0.004, 3.0,0.007, 4.0,0.011, 5.0,0.016,
6.0,0.023, 7.0,0.030, 8.0,0.039, 9.0,0.049,
10.0,0.060, 11.0,0.073, 12.0,0.089, 13.0,0.106,
14.0,0.126, 15.0,0.146, 22*9999. /
* * * * *

```

C C C C C

C. DCDSTA VS. AILRON (INCREMENT IN DRAG COEFFICIENT
DUE TO ASYMMETRIC STABILATOR DEFLECTION)

```

DATA DRG3/ -15., .0120, -14., .0102, -13., .0085, -12., .0071,
-10., .0048, -9., .0038, -8., .0030, -7., .0023,
-6., .0016, -5., .0011, -4., .0007, -3., .0003,
-2., .0001, -1., .0000, 0., .0000, 1., .0000,
2., .0001, 3., .0003, 4., .0007, 5., .0011,
6., .0017, 7., .0023, 8., .0030, 9., .0038,
10., .0048, 11., .0055, 12., .0071, 13., .0085,
14., .0100, 15., .0120, 12*9999./
** ** ** ** **

```

CCCC

D. DCDSTR VS. RUDDER (INCREMENT IN DRAG COEFFICIENT DUE TO RUDDER DEFLECTION)

```

DATA DRG4/ -15., .0059, -14., .0054, -13., .0048, -12., .0043,
-10., .0032, -9., .0027, -8., .0022, -7., .0017,
-6., .0013, -5., .0009, -4., .0006, -3., .0003,
-2., .0002, -1., .0001, 0., .0000, 1., .0001,
2., .0001, 4., .0006, 5., .0009, 6., .0013,
7., .0017, 8., .0022, 9., .0027, 10., .0032,
11., .0037, 12., .0043, 13., .0048, 14., .0054,
15., .0059, 12*9999./
** ** ** ** **

```

CCCCCCCC

* 3. PITCHING MOMENT COEFFICIENT DATA

A. CMBAS VS. ACA (BASIC PITCHING MOMENT COEFFICIENT AS A FUNCTION OF ANGLE OF ATTACK)

```

DATA PTCH1/ -10., 1.13, -8., 0.80, -6., 0.50, -4., 0.31,
-2., 0.16, 0., 0.08, 2., -0.03, 4., -0.13,
6., -0.22, 8., -0.32, 10., -0.46, 12., -0.62,
48*9999./
** ** **

```

CCCC

B. DCMSTE VS. STBLTR (INCREMENT IN PITCHING MOMENT COEFFICIENT DUE TO SYMMETRIC STABILATOR DEFLECTION)

```

DATA PTCH2/ -15., .90, -14., .88, -12., .78, -10., .68,
-8., .56, -6., .42, -4., .27, -2., .12,
0., .00, 2., -.10, 4., -.20, 6., -.32,
8., -.45, 10., -.58, 12., -.69, 14., -.78,
15., -.80, 38*9999./
** ** **

```

CCCCCCCC

* 4. SIDESLIP COEFFICIENT DATA

A. CYBAS VS. SIDESL AND AGA (BASIC SIDE FORCE COEFFICIENT AS A FUNCTION OF SIDESLIP AND ANGLE OF ATTACK. THE IN- DEPENDENT VARIABLE IS SIDESLIP, THE PARAMETER IS ANGLE OF ATTACK).

C

```

DATA SIC1/  0.0,      -8.0,      -6.0,      4.0,      8.0,      9999.
            -8.0,      0.148,      0.149,      0.140,      0.137,      9999.
            -6.0,      0.111,      0.110,      0.100,      0.077,      9999.
            -4.0,      0.073,      0.072,      0.063,      0.060,      9999.
            -2.0,      0.034,      0.034,      0.025,      0.022,      9999.
            0.0,      -0.002,      -0.003,      -0.013,      -0.020,      9999.
            2.0,      -0.040,      -0.042,      -0.050,      -0.060,      9999.
            4.0,      -0.077,      -0.078,      -0.085,      -0.096,      9999.
            6.0,      -0.114,      -0.116,      -0.127,      -0.129,      9999.
            8.0,      -0.151,      -0.153,      -0.162,      -0.162,      9999.
*
*
*
*
*
*
*
*

```

CCCCC

B. CRBAS VS. SIDESL AND ACA (BASIC ROLL COEFFICIENT AS A FUNCTION OF SIDESLIP AND PARAMETER ANGLE OF ATTACK)

```

DATA SIC2/  0.0,      -8.0,      2.0,      6.0,      10.0,      9999.
            -8.0,      0.048,      0.046,      0.040,      0.044,      9999.
            -6.0,      0.038,      0.036,      0.028,      0.030,      9999.
            -4.0,      0.026,      0.022,      0.015,      0.020,      9999.
            -2.0,      0.014,      0.010,      0.004,      0.008,      9999.
            0.0,      0.004,      0.004,      0.004,      0.002,      9999.
            2.0,      0.005,      0.014,      0.020,      0.014,      9999.
            4.0,      0.016,      0.026,      0.032,      0.025,      9999.
            6.0,      0.030,      0.038,      0.042,      0.036,      9999.
            8.0,      0.044,      0.052,      0.057,      0.048,      9999.
*
*
*
*
*
*
*
*

```

CCCCC

C. CNBAS VS. SIDESL AND ACA (BASIC YAW COEFFICIENT AS A FUNCTION OF SIDESLIP AND PARAMETER ANGLE OF ATTACK)

```

DATA SIC3/  0.0,      -8.0,      0.0,      6.0,      8.0,      9999.
            -8.0,      0.034,      0.037,      0.042,      0.042,      9999.
            -6.0,      0.025,      0.028,      0.033,      0.033,      9999.
            -4.0,      0.016,      0.019,      0.022,      0.023,      9999.
            -2.0,      0.007,      0.009,      0.012,      0.014,      9999.
            0.0,      0.010,      0.011,      0.004,      0.004,      9999.
            2.0,      0.019,      0.009,      0.007,      0.007,      9999.
            4.0,      0.019,      0.018,      0.016,      0.016,      9999.
            6.0,      0.028,      0.026,      0.024,      0.024,      9999.
            8.0,      0.036,      0.034,      0.032,      0.032,      9999.
*
*
*
*
*
*
*
*

```

CCCCCCC

* 5. DIRECTIONAL CONTROL COEFFICIENT DATA

A. CCYSTR VS. RUDDER AND ACA (INCREMENT IN SIDE FORCE
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER
ANGLE OF ATTACK)

C

```

DATA DREC1/ 0.0,      -8.0,      2.0,      6.0,      8.0,      999.
-15.0,      -0.90,      -0.97,      -0.95,      -1.02,      999.
-10.0,      -0.60,      -0.62,      -0.62,      -0.69,      999.
-5.0,      -0.32,      -0.36,      -0.37,      -0.42,      999.
0.0,      -0.04,      -0.02,      -0.03,      -0.03,      999.
5.0,      -0.40,      -0.42,      -0.38,      -0.04,      999.
10.0,      -0.70,      -0.66,      -0.62,      -0.66,      999.
15.0,      -1.00,      -0.98,      -0.92,      -0.96,      999.
*
12*99955./

```

C C C C C C

B. CCNSTR VS. RUDDER AND AGA (INCREMENT IN YAWING MOMENT
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER
ANGLE OF ATTACK)

```

DATA DREC2/ 0.0,      -8.0,      2.0,      6.0,      8.0,      999.
-15.0,      -0.70,      -0.68,      -0.62,      -0.65,      999.
-10.0,      -0.50,      -0.49,      -0.48,      -0.48,      999.
-5.0,      -0.26,      -0.24,      -0.22,      -0.18,      999.
0.0,      -0.00,      -0.00,      -0.00,      -0.00,      999.
5.0,      -0.22,      -0.20,      -0.18,      -0.14,      999.
10.0,      -0.52,      -0.48,      -0.47,      -0.46,      999.
15.0,      -0.80,      -0.79,      -0.74,      -0.75,      999.
*
12*99955./

```

C C C C C C

C. DCRSTR VS. RUDDER AND AGA (INCREMENT IN ROLLING MOMENT
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER
ANGLE OF ATTACK)

```

DATA DREC3/ 0.0,      -8.0,      2.0,      4.0,      6.0,      8.0,
-15.0,      -0.50,      -0.38,      -0.32,      -0.22,      0.0,
-10.0,      -0.34,      -0.29,      -0.26,      -0.20,      0.0,
-5.0,      -0.18,      -0.18,      -0.18,      -0.14,      0.0,
0.0,      -0.04,      -0.00,      -0.03,      -0.08,      0.0,
5.0,      -0.24,      -0.12,      -0.04,      -0.05,      0.0,
10.0,      -0.48,      -0.28,      -0.16,      -0.16,      0.0,
15.0,      -0.70,      -0.53,      -0.40,      -0.12,      0.0,
*
12*99955./

```

C C C C C C C C

* 6. LATERAL CONTROL COEFFICIENT DATA

A. CCYSTA VS. AIRLON AND AGA (INCREMENT IN SIDE FORCE
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND
PARAMETER ANGLE OF ATTACK)


```

DATA LTRL1/ 0.0, -8.0, , -1.0, , 4.0, , 10.0, , 9999.,
-15.0, -015, , -019, , -017, , -000, , 9999.,
-10.0, -013, , -014, , -010, , -002, , 9999.,
-5.0, -010, , -009, , -002, , -010, , 9999.,
0.0, -007, , -002, , -007, , -018, , 9999.,
5.0, -002, , -003, , -014, , -026, , 9999.,
10.0, -005, , -009, , -020, , -033, , 9999.,
15.0, -010, , -014, , -025, , -042, , 9999.,
12*99999./

```

CCCCC

B. CCNSTA VS. AIRLON AND ADA (INCREMENT IN YAWING MOMENT
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND
PARAMETER ANGLE OF ATTACK)

```

DATA LTRL2/ 0.0, -8.0, , -4.0, , 0.0, , 4.0, , 8.0, ,
-15.0, -0075, , -0050, , -0075, , -0120, ,
-10.0, -0040, , -0030, , -0050, , -0085, ,
-5.0, -0015, , -0020, , -0025, , -0060, ,
0.0, -0020, , -0010, , -0008, , -0020, ,
5.0, -0070, , -0030, , -0025, , -0050, ,
10.0, -0120, , -0045, , -0040, , -0120, ,
15.0, -0175, , -0070, , -0070, , -0175, ,
12*99999./

```

CCCCC

C. UCRSTA VS. AIRLON AND ADA (INCREMENT IN ROLLING MOMENT
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND
PARAMETER ANGLE OF ATTACK)

```

DATA LTRL3/ 0.0, -8.0, , -4.0, , 0.0, , 4.0, , 8.0, ,
-15.0, -0087, , -0090, , -0100, , -0092, ,
-10.0, -0060, , -0066, , -0068, , -0084, ,
-5.0, -0030, , -0033, , -0034, , -0036, ,
0.0, -0004, , -0004, , -0004, , -0030, ,
5.0, -0012, , -0024, , -0030, , -0020, ,
10.0, -0030, , -0058, , -0072, , -0047, ,
15.0, -0050, , -0080, , -0092, , -0067, ,
12*99999./

```

CCCCC

** 2. DYNAMIC STABILITY DERIVATIVES

```

DATA CLADT ,CCADT ,CMADT ,
/2.00 ,0.10 , -10.0 , /,
CL2 ,CDC ,CMC , /,
/5.0 ,0.1 , -15.0 , /,
CFBDT ,CYR ,CNBT , /,

```

```

* * * * *
/0.0      /0.4      /0.15      /,
CPR       CYP       CNR       /,
/0.2      /-0.1      /-0.2      /,
CPR       CYBDT     CNP       /,
/-C.4     /-0.1     /-0.01    /

```

CCCCCCCC

```

* * * * *
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
* * * * *

```

*** CONTROL SYSTEM PARAMETERS

```

DATA      KPTCHR      KROLLR      KYAWRT      KBANK
* * * * * /0.28      /0.10      /0.40      /10.8
          KGAMMA      /KALT      /CGARML      /CGARML
* * * * * /1.0       /0.3       /0.0       /0.0
          RRTLIM      /KNY       /KNZ        /,
* * * * * /75.0      /0.35      /0.05/    /,

```

CCCCCCCC

```

* * * * *
COMMON BLOCK /E/: INITIAL CONDITIONS
* * * * *

```

*** MISSILE INITIAL CONDITIONS

```

DATA      XM1         YM1         ALTUD1
* * * * * /0.0        /0.0        /50.0
          PITCH1      BANK1       HEDNG1
* * * * * /3.00       /0.0        /0.0
          AOA1         PTCHR1     ROLLR1
* * * * * /3.00       /0.0        /0.0

```

C

C

CCCC

*** TARGET INITIAL CONDITIONS

```

DATA      XT1         YTI         HT1
* * * * * /24000.0    /0.0       /10.0
          TSPEED

```

CCCC

```

* * * * *
COMMON BLOCK /F/: GUIDANCE PARAMETERS
* * * * *

```



```

C C C C C
*** PROPORTIONAL NAVIGATION & NAV FILTER CONSTANTS (AZIMUTH & ELEV.)
*
DATA      LAMDAZ      ,LAMDEL      ,KNFAZ      ,KNFEL      /
  /3.15      ,3.85      ,0.8      ,0.50 /
C C C C C
*** MISSION PHASE FLAGS & DECISION PARAMETERS
*
DATA      PH1      ,PH2      ,PH3      ,PH4      /
  /0      ,0      ,0      ,0 /
*
DATA      CFFSET      ,ALTATT      ,SGD2PU      ,MISDST      /
  /10.0      ,200.0      ,1.12      ,0.0 /
C C C C C
***
COMMON ELCK /H/: ECM/GLINT PARAMETERS
***
DATA      FREQ      ,SHIFT      ,SHIFTH      ,BRNTHR      /
  /0.00      ,75.0      ,10.0      ,250.0 /
*
END
C C C C C
***
SUBROUTINE MISSN
***
MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
CONTRCL LGOPS. NYC IS ASSUMED TO ALWAYS BE ZERO EXCEPT DURING
ATTACK. NZC IS LIMITED TO +4.0 AND -2.0 G'S.
***
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NCLT,PCJUNT,NFAZE
C C C C C
***
COMMON ELCK /A/: MISCELLANEOUS CONSTANTS
***
COMMON /A/ TIME      ,FINTIM,DT      ,CPDT      ,NCLT      ,NPTS      ,CPA      ,PCJUNT,
  ,T      ,RHO      ,PII      ,PASS      ,WT      ,S
*

```

```

** *
** *
** *
IXX      ,IYY      ,IZZ      ,IXZ      ,IA      ,IB      ,QS      ,
ID        ,IE        ,IF        ,IG        ,IH      ,II      ,IK      ,
CHORD2,CHORD ,SPAN2,SPAN ,NFAZE

```

CCCCC

```

*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****

```

```

COMMON /C/ KPTCHR      ,KROLLR      ,KYAWRT      ,KBANK      ,
KGAMMA      ,KALT      ,CGARML      ,CGARMLN      ,
RRTLIM      ,PLIM      ,KNY      ,KNZ      ,
AILLRN      ,STBLTR      ,RUCCER      ,
BSERO      ,NZSERO      ,NYSERO

```

CCCCC

```

*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

```

```

COMMON /D/ ALFA      ,BETA      ,VT      ,HMDOT      ,
U      ,V      ,W      ,
PHI      ,GAMMA      ,THETA      ,SY      ,
CD      ,CY      ,CL      ,CR      ,
CM      ,CN      ,P      ,Q      ,
R      ,ALFADT      ,BETADT      ,PDOT      ,
QDOT      ,RDOT      ,ALFADT      ,ALTUDE      ,
XM      ,YM      ,NZ      ,XMDCT      ,YMDCT

```

CCCCC

```

*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****

```

```

COMMON /F/ PH1      ,PH2      ,PH3      ,PH4      ,
CFFSET      ,ALATT      ,SGDZPU      ,MISDST      ,
LAMDAZ      ,LAMDEL      ,KNFAPZ      ,KNFEL      ,
NZC      ,PHIC      ,GAMMAC      ,PCCLIM      ,
PC      ,QC      ,RC      ,RANGE      ,
SIGAZ      ,SIGEL      ,SIGDAF      ,SIGDEF      ,
SYT      ,THETAT      ,XT      ,YT      ,
FT      ,NYC      ,PDPNG

```

CCCCC

```

*****
COMMON BLOCK /G/: OUTPUT PARAMETERS
*****

```

```

COMMON /G/ AUA      ,SIDESL      ,BANK      ,FLTPHC      ,
BANKC      ,PITCH      ,ROLLRT      ,RULKTC      ,
PTCHRT      ,YAWRT      ,HEADNG      ,FLTPTH

```



```

C      C      EANK ANGLE HCLD (60 DEG)
      AYC      = 0.0
      PFIC      = 60.0/PI I
      NZC      = AZC/COS(PHI)
      GC TO 100
      PF2      = 1
19
C      C      C      COURSE HCLD ON OFFSET HEADING TO POPUP
      C      C      C      ***
20      ABDSCZ = ABS(CSGGAZ)
      IF(AEDSDZ.GT.SGDZPU) GO TO 29
      C      C      C      ALTITUDE HCLD
      ALTIC      = 50.0
      ALTUDF      = KALT*(ALTC-ALTUDF)/VT
      GAMMAC      = GAMMA
      GAMMAF      = GAMMA
      AZC      = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
      C      C      C      BANK ANGLE HCLD (0 DEG)
      AYC      = 0.0
      PFIC      = 0.0
      NZC      = AZC/COS(PHI)
      GC TO 100
      PF3      = 1
29
C      C      C      PULLUP TO ATTACK ALTITUDE
      C      C      C      PROFCRTICUAL NAVIGATION IN AZIMUTH
      C      C      C      ***
30      IF(ALTUDE.GT.ALTAIT) GO TO 39
      C      C      C      VERTICAL FLIGHT PATH ANGLE HCLD (8.5 DEG)
      ALTIC      = 0.0
      GAMMAC      = 8.5/PI I
      GAMMAF      = GAMMA
      AZC      = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
      C      C      C      PROFCRTICUAL NAVIGATION IN AZIMUTH
      AYC      = LAMDZ*VT*SIGDAF/G
      NZC      = AZC*COS(PHI)+AYC*SIN(PHI)
      PFIC      = ATAN2(AYC,AZC)
      GC TO 100
      PF4      = 1
39

```

```

**      ATTACK
**      PROFCRTICNAL NAVIGATION IN AZIMUTH AND ELEVATION
40      ALTIC      = 0.0
      GAMMAC      = 0.0
      GAMMAF      = GAMMA
      AYC          = LAMCAZ*VT*SIGDAF/G
      AZC          = LAMDEL*VT*SIGDEF/G+COS(GAMMAF)
      NZC          = AZC*COS(PHI)+AYC*SIN(PHI)
      NYC          = 0.0

      BANK ANGLE CCMMAND ROUTINE INSURES ROLL
      IN SHORTEST DIRECTION

      PHIC      = ATAN2(AYC,AZC)
      CELPHI    = PHIC-PHI
      CFHIAB    = ABS(CELPHI)
      IF(OPHIAB.LT.PI) GO TO 100
      IF(PHIC.GE.0.0) GC TO 90
      PHIC      = PHIC+2.0*PI
      GC TO 100
      PHIC      = PHIC-2.0*PI
      PHIC
100 CONTINUE
**      NZ COMMAND LIMITED TO -2 & +4 G'S
      NZC      = LIMIT(-2.0,4.0,NZC)

      RETURN
      END

**      SUBROUTINE APILOT
**      LIMIT, FEALPL
**      MODELS THE INNER LCOP AUTOPILOT AND CONTROL MIXER. CALCULATES
      REQUIRES THE ELEVATOR, AILERON & RUDDER REQUIRED, MIXES THESE TO GET
      THE FIN STABILATOR COMMANDS, APPLIES THE FIN LIMITS OF +-15 DEG.
      AND ADJUSTS THE THREE CONTROL OUTPUTS TO ACCOUNT FOR THE LIMITS.
      IMPLICIT REAL(A-Z)
      INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NOUT,PCOUNT,NFAZE

```


CCCCC

COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS

COMMON /A/ TIME , FINITIM,DT , GPDT , NCUT , NPTS , CPA , PCOUNT,
G , T , RHO , PI , PII , WT , S ,
IXX , IYY , IZZ , IXZ , IA , IC ,
ID , IE , IF , IG , IH , IJ , QS ,
CHORD2,CHORD , SPAN2,SPAN , NFAZE , IK ,

CCCCCCC

COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS

COMMON /C/ KPTCHR , KRCLLR , KYAWRT , KBANK ,
KGAMMA , KALT , CGARML , CGARMN ,
RRTLIM , PLIM , KNY , KNZ ,
AILRON , STBLTR , RUDDER ,
BSERO , NZSERO , NYSERO

CCCCCCC

COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS

COMMON /C/ ALFA , BETA , VT , HMDOT ,
U , V , W , THETA , SY ,
PHI , GAMMA , CL , CR ,
CD , CY , CN , P , Q ,
CM , CN , ALFADT , BETADT , PDOT ,
R , RDOT , NZ , ALTUDE ,
QDOT , YM , XMDCT , YMDCT

CCCCCCC

COMMON BLOCK /F/: GUIDANCE PARAMETERS

COMMON /F/ PH1 OFF SET , PH2 , PH3 , PH4 ,
LAMDZ , ALTATT , SGDZPU , MI SDST ,
NCDZ , LAMDAZ , KNFEL , KNFEL ,
NZC , PHIC , GAMMAC , PCLIM ,
PC , QC , RC , RANGE ,
SIGAZ , SIGEL , SIGCAF , SIGDEF ,
SYT , THETAT , XT , YT ,

```

*          HT          ,NYC          ,POPRNG
C EXECUTABLE STMTS *****
C
C INNER LCCF AUTOPILOT
C
C NORMAL ACCELERATION COMMAND SYSTEM
C
C NZCLIM = LIMIT(-2.0,4.0,NZC)
C NZZ = NZ+CGARMN*CCOT/G
C ENZ = NZCLIM-NZZ
C ENZKNZ = ENZ*KNZ
C QC = ENZKNZ*DT
C NZSERI = QC-KPTCHR*C
C NZSEFC = REALPL(NZSERO,0.025,NZSERI,DT)
C
C ELE = -PII*NZSERO
C
C BANK ANGLE COMMAND SYSTEM
C
C EPHI = PHIC-PHI
C PC = KBANK*EPHI
C PCLIM = LIMIT(-PLIM,PLIM,PC)
C EP = PCLIM-P
C BSERI = EP*KROLLR
C BSERC = REALPL(BSERO,0.025,BSERI,DT)
C
C AIL = -PII*BSERO
C
C TURN COORDINATOR
C
C IF(PT4.EG.1) GO TO 30
C   NYC = 0.0
C CONTINUE
C NY = NY+CGARM*ROOT/G
C ENY = NYC-NY
C RC = ENY*KNY*DT
C NYSEFI = RC-KYAWRT*R
C NYSEFC = REALPL(NYSERO,0.025,NYSERI,DT)
C
C RUD = -PII*NYSERC
C CONTRCLS MIXER AND LIMITS
C
C LSTABI = ELE-AIL
C RSTABI = ELE+AIL
C LSTAB = LIMIT(-15.0,15.0,LSTABI)

```



```

** ** ** ** **
** ** ** ** **
** ** ** **  TABLE1, SUPRES
** ** ** **  TABLE2, SUPRES
** ** ** **  TABLE LOOKUP ROUTINES (TABLE1,2) TO CONSTRUCT THE AERO-
** ** ** **  DYNAMIC COEFFICIENTS FOR THE MISSILE GIVEN THE CONTROL
** ** ** **  INPUTS, ANGLE OF ATTACK, SIDESLIP AND ANGULAR RATES P, Q, R, ADT, BDT.
** ** ** **  THE MISSILE CALCULATES MOMENTS, FORCES, RATES, ANGLES AND RETURNS WITHIN
** ** ** **  THE COMMON BLOCKS. CUT-OFF-RANGE WARNINGS ARE SUPPRESSED AFTER
** ** ** **  20 CONSECUTIVE CALLS CUT OF RANGE.
** ** ** **  *****
** ** **  IMPLICIT REAL(A-Z)
** ** **  INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NCLT,PCOUNT,NFAZE
** ** **  *****
** ** **  ***** MISCELLANEOUS CONSTANTS *****
** ** **  *****
** ** **  COMMON /A/ TIME , FINTIM,DT ,OPDT ,NCLT ,NPTS ,CPA ,PCOUNT,
** ** **  G ,T ,RHO ,PI ,MASS ,WT ,S ,
** ** **  IXX ,IYY ,IZZ ,IXZ ,IYA ,IYB ,IC ,
** ** **  ID ,IE ,IF ,IG ,IHA ,IHB ,IJ ,IK ,
** ** **  CHORD2,CHORD ,SPAN2,SPAN ,NFAZE
** ** **  *****
** ** **  ***** AERODYNAMIC COEFFICIENT TABLES *****
** ** **  *****
** ** **  COMMON /B/ LFT1(2,36) ,LFT2(2,36) ,DRG1(2,36) ,DRG2(2,36) ,
** ** **  DRG3(2,36) ,DRG4(2,36) ,PTCH1(2,36) ,PTCH2(2,36) ,
** ** **  SID1(6,10) ,SID2(6,10) ,SIC3(6,10) ,DREL1(6,10) ,
** ** **  DREC2(6,10) ,DREC3(6,10) ,LTR1(6,10) ,LTR2(6,10) ,
** ** **  LTR3(6,10) ,CLADT ,CDACT ,CMADT ,
** ** **  CLQ ,CDQ ,CMQ ,CRBDT ,CRBDT ,
** ** **  CYR ,CNBDT ,CRP ,CYECT ,CNP
** ** **  *****
** ** **  ***** CONTROL SYSTEM PARAMETERS *****
** ** **  *****
** ** **  COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
** ** **  *****
** ** **  COMMON /C/ KPTCHR ,KRGLLR ,KYAWRT ,KBANK ,
** ** **  KGAMMA ,KALT ,CGARML ,CGARML ,
** ** **  RRTLIM ,PLIM ,KNY ,KNZ
** ** **  *****

```

```

**
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
**
COMMON /C/ ALFA
      U
      PHI
      CD
      CM
      R
      QDOT
      XM
      BETA
      V
      GAMMA
      CY
      CN
      ALFADT
      RDOT
      YM
      VT
      W
      THETA
      CL
      P
      BETADT
      NZ
      XMDCT
      HMDOT
      SY
      CR
      Q
      PDOT
      ALTUDE
      YMDCT
**

SIDESL = PII*BETA
AOA = PII*ALFA
CLEAS = TABLE1(LFTI1,ACA)
DCLSTE = TABLE1(LFTI2,STBLTR)
CDBAS = TABLE1(DRGI1,CLBAS)
DCDSTE = TABLE1(DRGI2,STBLTR)
DCCSTA = TABLE1(DRGI3,AILRON)
DCCSTR = TABLE1(DRGI4,RUDDER)
CMBAS = TABLE1(PTCHI1,AOA)
DCMSTE = TABLE1(PTCHI2,STBLTR)
CYBAS = TABLE2(SIDI1,ACA,SIDESL)
CRBAS = TABLE2(SIDI2,ACA,SIDESL)
CNBAS = TABLE2(SIDI3,ACA,SIDESL)
DCYSTR = TABLE2(DRECI1,AOA,RUDDER)
DCNSTR = TABLE2(DRECI2,AOA,RUDDER)
DCRSTR = TABLE2(DRECI3,AOA,RUDDER)
DCYSTA = TABLE2(LTRL1,AOA,AILRCN)
DCNSTA = TABLE2(LTRL2,AOA,AILRCN)
DCRSTA = TABLE2(LTRL3,AOA,AILRCN)
AERCDYNAMIC COEFFICIENTS
CL = CLEAS+DCLSTE+CHORD2*(CLADT*ALFADT+CLQ*Q)/VT
CD = CCEAS+DCCDSTE+CCDSTA+DCCDSTR+CHORD2*(CYR*P+CYBDT*BETAUT)/VT
CY = CCEAS+CCYSTA+CCYSTA+SPAN2*(CMADT*ALFADT+CMQ*Q)/VT
CM = CMEAS+DCMSTE+CHORD2*(CNBDT*BETAUT+CNRR*P+CNPP)/VT
CN = CNEAS+DCNSTA+DCNSTA+SPAN2*(CRBDT*BETAUT+CRKR*P+CKP)/VT

```



```

C C C C C
AERODYNAMIC FORCES AND MOMENTS
L = CL*CS
D = CD*CS
LA = SPAN*CR*QS
MA = CFCRD*CM*QS
NA = SPAN*CN*QS
X = L*SIN(ALFA)-D*COS(ALFA)
Y = CY*QS
Z = -L*CCS(ALFA)-D*SIN(ALFA)

C C C
NORMAL & LATERAL ACCELERATIONS
NZ = -Z/(MASS*G)
NY = Y/(MASS*G)

C C C C C
** COMMENCE INTEGRATION OF EQUATIONS OF MOTION
EULER ANGLES
PHIDOT = P+TAN(THETA)*(Q*SIN(PHI)+R*COS(PHI))
THETAD = G*COS(PHI)-R*SIN(PHI)
SYDDOT = (Q*SIN(PHI)+R*COS(PHI))/COS(THETA)
PHI = PHI + PHIDOT*DT
THETA = THETA + THETAD*DT
SY = SY + SYDDOT*DT

C C C
LINEAR ACCELERATIONS AND VELOCITIES
UDOT = -G*SIN(THETA)+V*R-W*Q+X/MASS+T/MASS
VDDOT = G*SIN(PHI)*COS(THETA)-U*R+W*P+Y/MASS
WDDOT = G*CCS(PHI)*COS(THETA)+U*Q-V*P+Z/MASS
U = U + UDDOT*DT
V = V + VDDOT*DT
W = W + WDDOT*DT
VT = SQRT(U**2+V**2+W**2)
VTDOT = SQRT(UDOT**2+VDDOT**2+WDDOT**2)

C C C
ANGULAR ACCELERATIONS AND VELOCITIES
PDCT = IE*LA+IC*NA-ID*P*Q-IE*R*Q
QDDOT = IF*MA-IG*P*R-IH*(P**2-R**2)
RDDOT = IC*LA+II*NA-IJ*P*Q-IK*R*Q
P = P + PDCT*DT
Q = Q + QDDOT*DT

```

```

C C C
R = R + RDOT*DT
ANGLES CF ATTACK, SIDESLIP, AND FLIGHT PATH
ALFADT = (ATAN(W/U)-ALFA)/DT
BETADT = (ASIN(V/VT)-BETA)/DT
ALFA = ATAN(W/U)
BETA = ASIN(V/VT)
GAMMA = ASIN(HMDOT/VT)

C C C
MISSILE POSITION IN INERTIAL SPACE
*
XMDOT = U*COS(SY)*COS(THETA)+V*(COS(SY)*SIN(THETA)*SIN(PHI)
      -SIN(SY)*COS(PHI))+W*(COS(SY)*SIN(THETA)*COS(PHI)+
      SIN(SY)*SIN(PHI))
*
YMDOT = U*SIN(SY)*COS(THETA)+V*(SIN(SY)*SIN(THETA)*SIN(PHI)
      +COS(SY)*COS(PHI))+W*(SIN(SY)*SIN(THETA)*COS(PHI)-
      COS(SY)*SIN(PHI))
*
HMDOT = U*SIN(THETA)-V*COS(THETA)*SIN(PHI)-W*COS(THETA)*COS(PHI)
HORDDOT = SQRT(XMDOT**2+YMDOT**2)
XM = XM + XMDOT*DT
YM = YM + YMDOT*DT
ALTUDE = ALTUDE + HMDOT*DT

C C C
RETURN
END

C C C
9-07-84
FUNCTION TABLE1 (ARRAY,IP)
TABLE LOCKUP WITH LINEAR INTERPOLATION FOR A FUNCTION
OF ONE VARIABLE, Y=F(X). MAXIMUM NUMBER OF POINTS THE
LIMITED TO 30 BY THE DIMENSION STANMENT. 9999.0 THE ALL
FIRST ARRAY ENTRY (ARRAY(1,1)) EXACTLY 9999. THE INDEPEND
UNUSED ARRAY ELEMENTS MUST BE EXACTLY 9999. THE INDEPEND
VARIABLES ARE SUPPRESSED AFTER 20 CONSECUTIVE CALLS (ABOUT 5 UT'S)
WARNINGS ARE SUPPRESSED AFTER 20 CONSECUTIVE CALLS (ABOUT 5 UT'S)
*****

C C C
REAL ARRAY(2,30),IP,C,TABLE1
INTEGER I,J,K,N,SUPRES
DATA J,K,N /3*0/
K = K+1
IF (.NOT. IP.LT. ARRAY(1,1)) GO TO 10
TABLE1=ARRAY(2,1)

```



```

C      REAL A(6,10), IP, IV, CP, CV, LFT, RGT, TABLE2
C      INTEGER I, LI, UI, J, K, N, SUPRES
C      DATA J, K, N /3*0/

C      K = K+1
C      IF(.NOT. IP.LT. A(2,1)) GO TO 10
C      CP = 0.
C      LI = 2
C      UI = 2
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1001) IP, A(2,1)
C      GO TO 55

C      10  DC 50 I=2,6
C      IF(.NOT. A(I,1).EQ.9999.0) GO TO 20
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1002) IP, A(I-1,1)
C      CP = 0.
C      LI = I-1
C      UI = I-1
C      GO TO 55

C      20  IF(IP-A(I,1)) 30,40,50
C      IP < A(I,1)
C      30  CP = (IP-A(I-1,1))/(A(I,1)-A(I-1,1))
C      LI = I-1
C      UI = I
C      GO TO 55

C      IF = A(I,1)
C      40  CP = 0
C      LI = I
C      UI = I
C      GO TO 55

C      END IF
C      CCNTINUE
C      END IF

C      55 IF(.NOT. IV.LT. A(1,2)) GO TO 60
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1003) IV, A(1,2)
C      TABLE2=A(LI,2)+CP*(A(UI,2)-A(LI,2))
C      RETURN

C      60  DC 100 I=2,10
C      IF(.NOT. A(1,I).EQ.9999.0) GO TO 70
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1004) IV, A(1,I-1)
C      TABLE2=A(LI,I-1)+CP*(A(UI,I-1)-A(LI,I-1))
C      RETURN

```

```

7C      IF(IV-A(1,I)) 80,90,100
C      IV < A(1,I)
80      CV = (IV-A(1,I-1))/(A(1,I)-A(1,I-1))
      LFT = A(1,I-1)+CP*(A(1,I)-A(1,I-1))
      RGT = A(1,I)+CP*(A(1,I)-A(1,I-1))
      TABLE2 = LFT+CV*(RGT-LFT)
      RETURN
C      IV = A(1,I)
90      TABLE2 = A(1,I)+CP*(A(1,I)-A(1,I))
      RETURN
C      IF
100      END IF
      CCNTINCE
C      WRITE(6,1005)
C      RETURN
C      FORMAT STATEMENTS FOR SUBROUTINE TABLE2 *****
1001  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER BELOW DATA.',
*      'INPUT PARAMETER =',F10.2,
*      'USED LOWEST PARAMETER =',F10.2)
1002  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER ABOVE DATA.',
*      'INPUT PARAMETER =',F10.2,
*      'USED HIGHEST PARAMETER =',F10.2)
1003  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. BELOW DATA.',
*      'INPUT INDEP. VAR. =',F10.2,
*      'USED LOWEST INDEP. VAR. =',F10.2)
1004  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. ABOVE DATA.',
*      'INPUT INDEP. VAR. =',F10.2,
*      'USED HIGHEST INDEP. VAR. =',F10.2)
1005  FORMAT('0','SUBROUTINE TABLE2: ERROR. SUBROUTINE DID NOT END.')
      END
C
C
C ***** 9-05-84 *****
C ***** FUNCTION SUPRES(J,K,N) *****
C ***** DETERMINES TO SUPPRESS WARNINGS FROM TABLE1 OR TABLE2 AFTER THEY *****
C ***** HAVE BEEN CALLED ABOUT 20 TIMES IN A ROW. (ABOUT 5 DT INTERVALS.) *****
C ***** INTEGER J,K,N, SUPRES *****
C      IF(K-J.EG.1)GO TO 10
      N = 0
      K = 0
      J = 0
      GC TO 15

```



```

* * *
R      QUOT      XM      ,ALFADT      ,BETADT      ,PDOT      ,
      ,RDOT      ,YM      ,NZ      ,ALTUDE      ,
      ,YM      ,XMDCT      ,YMDOT      ,

```

CCCCC

```

*****
COMMON BLOCK /E/: INITIAL CONDITIONS
*****

```

```

COMMON /E/  XM1  PITCH1  ,YMI      ,ALTUDI      ,UI      ,
      ,AOA1      ,BANK1      ,HEDNGI      ,SI DESI      ,
      ,XTI      ,PITCHR1      ,KOLLRI      ,YAWRI      ,
      ,XTI      ,YTI      ,HTI      ,TSPEED      ,

```

CCCCC

```

*****
COMMON ELCK /F/: GUIDANCE PARAMETERS
*****

```

```

COMMON /F/  PH1  CFFSET      ,PH2      ,PH3      ,PH4      ,
      ,LAMDAZ      ,ALTATT      ,SGCZPU      ,MISDST      ,
      ,NZC      ,LAMDEL      ,KNFAZ      ,KNFEL      ,
      ,PC      ,PHIC      ,GAMMAC      ,PCFLIM      ,
      ,SIGAZ      ,QC      ,RC      ,RANGE      ,
      ,SYT      ,SIGEL      ,SIGDAF      ,SIGDEF      ,
      ,FT      ,THETAT      ,XT      ,YT      ,

```

CCCCC

```

*****
COMMON ELCK /H/: ECM/GLINT PARAMETERS
*****

```

```

COMMON /H/  FREQ      ,SHIFTY      ,SHIFTH      ,BRNTHR      ,
      ,XECM      ,VECM      ,HECM      ,XGLNT      ,
      ,YGLNT      ,HGLNT      ,XTECM      ,YTECM      ,

```

CCCCC

EXECUTABLE STATEMENTS:

*** TARGET ACTION

```

XI = XI1
YT = YT1+TSPEED*TIME
HT = HT1

```

RELATIVE RANGE TO TARGET

CC


```

105 CONTINUE
C
  POPRNG = PHASE*PII
  IF (RANGE.LT.BRNTHR) GO TO 350
  XECMW = SIN(2*PI*FREQ*TIME+PHASE)
  XECM = SQWV(XECMW,SHIFTX)
C
  YECMW = SIN(2*PI*FREQ*TIME+PHASE)
  YECM = SQWV(YECMW,SHIFTY)
C
  HECMW = SIN(2*PI*FREQ*TIME+PHASE)
  HECM = SQWV(HECMW,SHIFTH)
  GC TO 400
350 CONTINUE
  XECM = 0.0
  YECM = 0.0
  HECM = 0.0
400 CONTINUE
C
  XTECM = XI+XECM+XGLNT
  YTECM = YT+YECM+YGLNT
  HTECM = HT+HECM+HGLNT
C
  *** RELATIVE RANGE AND RANGE RATE TO RADAR TARGET
C
  XRECM = XTECM-XM
  YRECM = YTECM-YM
  HRECM = HTECM-ALTUCE
  RNRECM = SQRT(XRECM**2+YRECM**2)
  RGECMT = SQRT(XRECM**2+YRECM**2+HRECM**2)
C
  XDCTR = -XMDOT
  YDCTR = TSPEED-YMCDOT
  HDCTR = -HMDOT
  HORDTR = SQRT(XDCTR**2+YDCTR**2)
C
  *** SEEKER LCS AND LCS RATE CALCULATIONS
C
  SYT = ATAN2(YRECM,XRECM)
  TRAKAZ = ATAN2(YMDCT,XMDOT)
  SIGAZ = SYT-TRAKAZ
C
  VTANAZ = -XDCTR*SIN(SYT)+YDCTR*CGS(SYT)
  SIGLAZ = VTANAZ/RNGECM
  SIGDAF = REALPL(SIGDAF,KNFAZ,SIGDAZ,DT)
C

```

```

C      THETAT = ATAN2 (HRECM, RNGECHM)
C      HURDOT = SQRT (XMDOIT**2 + YMDOT**2)
C      TRAKEL = ATAN2 (HMDCT, HCRDOT)
C      SIGEL  = THETAT - TRAKEL
C
C      VTANEL = HDOTR * COS (THETAT) + HORDTR * SIN (THETAT)
C      SIGDEL = VTANEL / RGECHM
C      SIGDEF = REALPL (SIGDEF, KNFEL, SIGDEL, DT)
C
C      RETURN
C      END
C
C      8-01-84
C      SUBROUTINE RNG (RAND)
C      ***
C      *** GENERATES A RANDOM NUMBER BETWEEN -1.0 & 1.0
C      ***
C      IMPLICIT REAL (A-Z)
C      DATA SEED / 4.0 /
C
C      RAND = (SEED + 3.14159) ** 5.04
C      RAND = (RAND - IFIX (RAND) - 0.5) * 2.0
C      SEED = RAND
C
C      RETURN
C      END
C
C      9-07-84
C      FUNCTION SQW (WAVE, AMPL)
C      ***
C      *** GENERATES A SQUARE WAVE FROM A SIN WAVE
C      ***
C      IMPLICIT REAL (A-Z)
C
C      IF (WAVE .GT. 0.0) SQW = AMPL
C      IF (WAVE .LT. 0.0) SQW = -AMPL
C      IF (WAVE .EQ. 0.0) SQW = 0.0
C
C      RETURN
C      END
C
C      8-20-84

```



```

C      * * *      SIGAZ      ,SIGDAF      ,SIGDEF      ,
      * * *      SYT        ,XT        ,YT        ,
      * * *      HT        ,POPRNG      ,
C      COMMON /G/  AOA      ,BANK      ,FLTPHC      ,
      * * *      BANC      ,ROLLRT      ,ROLKTC      ,
      * * *      PTCCHR      ,HEACNG      ,FLTPTH      ,
      * * *      HEADRT      ,DSIGAZ      ,DSIGEL      ,
      * * *      DSGDAZ      ,ERFBK      ,ERFRR      ,
      * * *      ERF AZ      ,
C      COMMON /H/  FREQ      ,SHIFTH      ,BRNTHR      ,
      * * *      XECM      ,HECM      ,XGLNT      ,
      * * *      YGLNT      ,XTECM      ,YTECM      ,
      * * *      HTECM      ,
C      COMMON /I/  PTS(300,20),PLTN(6,7),XN(6,7),YN(6,7),TITLE(6),
      *      LEG(4,20)
C      EXECUTABLE STMTS *****
C      RACIAN TO DEGREE CONVERSIONS FOR OUTPUT
C      AOA      = ALFA*PI I
C      SIDESL    = BETA*PI I
C      BANK      = PHI*PI I
C      FLTPHC    = GAMMAC*PI I
C      BANC      = PHIC*PI I
C      PITCH     = THETA*PI I
C      ROLLRT    = P*PI I
C      ROLKTC    = PCLIM*PI I
C      PTCCHR    = Q*PI I
C      YAWRT     = R*PI I
C      HEADNG    = SY*PI I
C      FLTPTH    = GAMMA*PI I
C      HEADT     = SYT*PI I
C      ELEVT     = THETA*PI I
C      DSIKAZ    = SIGAZ*PI I
C      DSIGEL    = SIGEL*PI I
C      DSGCAZ    = SIGDAF*PI I
C      DSGDEL    = SIGDEF*PI I
C      * * *      CREATE THE MISSION PHASE MARKER (MARK)
C      MARK = C.O
C      IF (PH1.EQ.1)MARK = 1.O
C      IF (PH2.EQ.1)MARK = 2.O

```

```

C      IF (PH3.EQ.1)MARK = 3.0
C      IF (PH4.EQ.1)MARK = 4.0
C      NPTS = NPTS+1
C      K = NPTS+2
C      *** COMPUTE THE ERROR FUNCTIONS
C      IF (MARK.EQ.4) GO TC 50
C      ERRBK = 0.0
C      ERRRR = 0.0
C      ERRRAZ = 0.0
C      ERREL = 0.0
C      GC TC 100
C      50 CONTINUE
C      ERRBK = ERRBK + ABS(BANKC-BANK) *DT
C      ERRRR = ERRRR + ABS(RCLRTC-ROLLRT) *DT
C      ERRRAZ = ERRRAZ + ABS(DSGDAZ) *DT
C      ERREL = ERREL + ABS(DSGDEL) *DT
C      100 CONTINUE
C      ERFBK = ERFBK/TIME
C      ERRFR = ERRRR/TIME
C      ERFAZ = ERRRAZ/TIME
C      ERFEL = ERREL/TIME
C      *** SELECT THE VARIABLES TO BE STORED
C      KEEP(1) = TIME
C      GRAPH 1 = NZC
C      KEEP(2) = NZ
C      KEEP(3) = NZ
C      GRAPH 2 = EANKC
C      KEEP(4) = BANK
C      KEEP(5) = BANK
C      GRAPH 3 = ROLRTC
C      KEEP(6) = ROLLRT
C      KEEP(7) = ROLLRT
C      GRAPH 4 = YECM
C      KEEP(8) = YECM
C      KEEP(9) = YGLNT
C      GRAPH 5 = AILRON
C      KEEP(10) = AILRON

```

```

KEEP(11) = STBLR
KEEP(12) = RUDDER

GRAPH 6
KEEP(13) = ALTUDE

GRAPH 7
KEEP(14) = XM
KEEP(15) = YM
KEEP(16) = XT
KEEP(17) = YT

SPARES
KEEP(18) = RANGE
KEEP(19) = MARK
KEEP(20) = NYC

*** STORE MINIMUM AND MAXIMUM VALUES OF EACH VARIABLE
DO 20 I=1,20
  IF (NPPTS.GT.1) GO TO 10
  PTS(1,I) = KEEP(1)
  PTS(2,I) = KEEP(1)
  10  CONTINUE
  PTS(1,I) = AMIN1(PTS(1,I),KEEP(I))
  PTS(2,I) = AMAX1(PTS(2,I),KEEP(I))
  20 CONTINUE

*** STORE VALUES OF EACH VARIABLE WITH THE TIME
DO 30 I=1,20
  PTS(K,I) = KEEP(I)
  30 CONTINUE

*** CHECK FOR ARRAY OVERFLOW AND TERMINATE AT 255 POINTS
IF (NPPTS.GE.295) CPA = 3.0

RETURN
END

```

```

*** **
*** ** SUBROUTINE OUTPUT(NPTS,CPA)
*** **
*** ** HEADER, PLOT1, PLOT2, PLOT21, PLOT3
*** **
*** **
9-07-84
*** **
*** **
*** **

```


ARE THE NUMBERS (BETWEEN 1 AND 20) CF THE DEPENDENT
VARIABLES TO BE PLOTTED AGAINST TIME.

DATA	NEV	/	0	2	3	2C	0
*				2	3	0	
*			0	4	5	0	
*			0	6	7	0	
*			0	8	9	0	
*			0	10	11	0	
*			0	13	0	0	
*			0	0	0	0	

** LOAD THE MESSAGES AND VARIABLES TO APPEAR IN THE UPPER
LEFT HAND CORNER OF EACH GRAPH.

DATA MESS1 /:FREQ = '//
DATA MESS2 /:PHASE = '//

EXECUTABLE STMTS:

VAR1 = FREQ
VAR2 = PUPRNG

***** READ TITLE CAPTIONS FOR GRAPHS AND PRINTOUT *****
***** FROM FILE NO.2: LABELS DATA *****

IF (FLAG.EQ.1.0) GO TO 18

** READ IN OVERALL TITLE LINES (4 LINES OF 32 CHARACTERS)

5 READ(2,5)((TITLE(J,I),J=1,8),I=1,4)
FORMAT(20X,8A4)

** READ IN EACH GRAPH TITLE & ITS AXIS LABELS (24 CHARACTERS EACH)

DO 10 J=1,7
READ(2,12)(PLTN(I,J),I=1,6)
READ(2,12)(XN(I,J),I=1,6)
READ(2,12)(YN(I,J),I=1,6)

10 CONTINUE
12 FORMAT(20X,6A4)

** READ IN THE LEGEND LABEL FOR EACH OF THE 20 STORED VARIABLES
(16 CHARACTERS EACH)

15 READ(2,15)((LEG(I,J),I=1,4),J=1,20)
FORMAT(20X,4A4)

```

C      FLAG = 1.0
C      CONTINUE
C
C      ***** WRITE PRIMARY DATA OUTPUT *****
C      ***** TO FILE 6 (TERMINAL) AND THEN FILE 9 (TCMC DATA) *****
C
C      DO 100 K=1,2
C      IF(K.EQ.1)KFILE=6
C      IF(K.EQ.2)KFILE=9
C
C      ***** TITLES *****
C
C      20      WRITE(KFILE,20)((TITLE(I,J),I=1,8),J=1,4)
C      FORMAT('1',4(20X,8A4//))
C
C      ***** INDICATE HOW THE SIMULATION TERMINATED *****
C
C      30      GC TC(30,40,50),CPA
C
C      35      WRITE(KFILE,35)
C      FORMAT(1X,'SIMULATION TERMINATED DUE TO CPA')
C      GO TO 60
C
C      40      WRITE(KFILE,45)
C      45      FORMAT(1X,'SIMULATION TERMINATED DUE TO FINTIME')
C      GO TO 60
C
C      50      WRITE(KFILE,55)
C      55      FORMAT(1X,'SIMULATION TERMINATED DUE TO FULL ARRAY')
C
C      60      CONTINUE
C
C      ***** VALUE OF THE ITERATED PARAMETER *****
C
C      65      WRITE(KFILE,65) FREQ
C      FORMAT(1X,'*** BLINKER FREQUENCY= ',F8.2)
C
C      67      WRITE(KFILE,67) PCPRNG
C      67      FORMAT(1X,'*** BLINKER PHASE = ',F6.0//)
C
C      ***** LIST THE PRIMARY DATA OUTPUTS *****
C
C      75      WRITE(KFILE,75) MISDST,ERFBK,ERFR,ERFAZ,ERFEL
C      FORMAT(1X,'MISS ***** DISTANCE * ***** ERROR FUNC
C      *TIONS ***** / ***** BANK *****')

```

```

* ROLL RATE * AZIMUTH * ELEVATION *'//
* 5(3X,F10.5,2X,'*')//)
C C C
** LIST THE VARIABLE RANGES
C
80 WRITE(KFILE,80)
FCFMAT(18X,'***** RANGES FOR ALL SAVED VARIABLES *****'
//30X,' MINIMUM
WRITE(KFILE,90)((LEG(I,J),I=1,4),PTS(1,J),PTS(2,J)),J=1,20)
FCFMAT(11X,4A4,4X,F12.6,3X,F12.6)
C 100 CONTINUE
C C C
***** TABULAR DATA OUTPUT *****
C C C
DO 200 I=1,4
J=(I-1)*4+2
K=J+3
WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
WRITE(9,65) FREQ
WRITE(9,125) I
FCFMAT(50X,' DATA SET NUMBER ',I1,' [F 4'//)
WRITE(9,135)((LEG(L,1),L=1,4),((LEG(L,M),L=1,4),M=J,K)
FCFMAT(2X,20A4//)
C
NN=NPTS+2
DC 150 N=3,NN
START NEW PAGE EVERY 65 LINES
L=MOD(N,65)
IF(L.NE.0) GC TO 140
WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
WRITE(9,65) FREQ
WRITE(9,125) I
WRITE(9,135)((LEG(L,1),L=1,4),M=J,K)
((LEG(L,M),L=1,4),M=J,K)
*
140 CONTINUE
WRITE(9,145) PTS(N,1),(PTS(N,L),L=J,K)
145 FCFMAT(1X,5('*,F12.6,3X))
150 GCNTINUE
200 CONTINUE
C C C C C
***** PRODUCE GRAPHIC OUTPUT USING DISPLA SUEROUTINES *****

```



```

DO 50 J=1,3
DC 30 I=1,8
      HC(I) = TITLE(I,J)
30  CONTINUE
      CALL HEADIN(HC ,32 , 1.1 ,4)
50  CONTINUE
DO 60 I=1,6
      HC(I) = PLTN(I,KP)
      XNM(I) = XN(I,KP)
      YNM(I) = YN(I,KP)
60  CONTINUE
      CALL HEADIN(HD ,24 , 1.0 ,4)
      CALL XNAME( XNM ,24)
      CALL YNAME( YNM ,24)
      RETURN
ENC
*** FILE: FLCT1 ***
*** CONTAINS ALL S/R'S THAT INTERFACE WITH CISSPLA EXCEPT HEADER ***
***
*** SUBROUTINE PLOT1(MESS1,MESS2,VARI,VAR2) ***
***
*** INITIALIZES DISSPLA FOR A NEW PAGE AND GRAPH ***
***
IMPLICIT REAL(A-H,C-Z),INTEGER(I-N)
DIMENSION MESS1(2),MESS2(2)
CALL NCCHEK
CALL GRACE(0.,647)
CALL BLCWUP(0.,8.5)
CALL PAGE(1.,8.5)
CALL HWREQ('AUTO')
CALL HWSCAL('SCREEN')
CALL NCERDR
CALL PFYSOR(1.,.75)
CALL AREA2C(9.,6.5)
CALL SWISSM
*** PUT THE MESSAGES INTO THE GRAPHS
CALL MSGAG(MESS1,8,0.2,0.0)

```



```

C      CALL REALNC(VAR1,2,'ABUT','ABUT')
C      CALL MESSAG(MESS2,8,0.2,5.6)
C      CALL REALNC(VAR2,0,'ABUT','ABUT')
C      CALL BLFEC(0.1,5.5,1.8,0.8,0.01)

C      RETURN
C      END
C
C      *****8-26-84*****
C      *****SUBROUTINE PLOT2(PTS,LEG,DV,IV,NPTS)*****
C      *****LOADS THE LEGEND ARRAY WITH CURVE LABELS; GETS THE POINTS FOR*****
C      *****EACH CURVE FROM THE PTS ARRAY; PLOTS EACH CURVE. IV,DV ARE IN-*****
C      *****DEPENDENT, DEPENDENT VARIABLE INDEXES. THEY GIVE THE COLUMN IN*****
C      *****THE PTS ARRAY WHERE THEIR VALUES ARE FOUND. LEG IS THE PACKED*****
C      *****ARRAY CCNTAINING THE LABELS FOR EACH VAR. S. *****
C      *****ELEMENT ARRAY CCNTAINING THE INDEXES FOR UP TO 4 DEP VAR. S. *****
C      *****
C      IMPLICIT REAL (A-H,C-Z), INTEGER(1-N)
C      INTEGER DV(4),IPACK(100),LEG(4,20),LBL(5)
C      DIMENSION PTS(300,20),XP(300),YP(300)
C
C      DATA MCNEY /'$/
C
C      *****FIRST FIND OUT HOW MANY CURVES THERE ARE*****
C
C      I=1
C      5 IF (DV(I).EQ.0)GO TO 10
C      MCNV = I
C      IF (I.EQ.4)GO TO 10
C      I = I+1
C      GO TO 5
C      1C CONTINUE
C
C      *****NEXT PACK THE LEGEND ARRAY AND RANGE THE Y-AXIS*****
C
C      DO 30 I=1,MCNV
C      K = DV(I)
C      IF (I.GT.1) GO TO 15
C      YMIN = PTS(1,K)
C      YMAX = PTS(2,K)
C      GO TO 20
C      30 CONTINUE
C      YMIN = AMIN1(YMIN,PTS(1,K))
C      YMAX = AMAX1(YMAX,PTS(2,K))
C      15

```

```

C      20      CCNTINUE
C      DC 25 J=1,4
C      LBL(J) = LEG(J,K)
C      25      CCNTINUE
C      LBL(5) = MONEY
C      CALL LINES(LBL,IPACK,I)
C      30      CONTINUE
C      *** RANGE THE INDEPENDENT VARIABLE(S)
C      XMIN = PTS(1,IV)
C      XMAX = PTS(2,IV)
C      *** NOW PLOT THE CURVES
C      CALL GRAF(XMIN,SCALE,XMAX,YMIN,SCALE,YMAX)
C      DO 90 I=1,MCRV
C      DC 80 J=1,NPTS
C      XP(J) = PTS(J+2,IV)
C      YP(J) = PTS(J+2,DV(I))
C      80      CCNTINUE
C      CALL CURVE(XP,YP,NPTS,1)
C      90      CONTINUE
C      PLOT THE GRID & LEGEND AND FINISH THE GRAPH
C      CALL PLCT21(IPACK,MCRV)
C      RETURN
C      END
C      7-25-84
C      *** SUBROUTINE PLOT21(IPACK,MCRV)
C      *** PLOTS THE LEGEND & THE GRID AND ENDS THIS GRAPH
C      ***
C      IMPLICIT INTEGER(I-N)
C      DIMENSION IPACK(100)
C      XW=XLEGND(IPACK,MCRV)
C      YW=YLEGND(IPACK,MCRV)
C      CALL LEGEND(IPACK,MCRV,0.5,0.5)
C      CALL BLFEC(0.4,0.4,0.4,XW+0.2,YW+0.2,.01)
C      CALL DC1

```


APPENDIX E

LISTING FOR SUBROUTINE MISSN1

9-07-84

***** SUBROUTINE MISSN1 *****

***** SEA SKIMMER GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE *****
 WITH NC CFFSET TURN. AFTER POPUP, GUIDANCE IS STANDARD PRO-
 PORTIONAL. POPUP USES ONLY ALTITUDE COMMAND VICE GAMMAC.

MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
 OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
 CONTRCL LOOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED
 TO +4.C AND -2.0 G'S.

IMPLICIT REAL(A-Z)
 INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE

***** COMMON ELCK /A/: MISCELLANEOUS CONSTANTS *****

COMMON /A/ TIME , FINTIM,DT ,CPDT ,NCLT ,NPTS ,CPA ,PCOUNT,
 G ,T ,RHO ,PI ,PII ,MASS ,WT ,S ,
 IXX ,IYY ,IZZ ,IXZ ,IA ,IB ,US ,
 ID ,IE ,IF ,IG ,IH ,IJ ,IK ,
 CHORD2,CHORD ,SPAN2,SPAN ,NFAZE

***** COMMON ELCK /C/: CCNTRL SYSTEM PARAMETERS *****

COMMON /C/ KPTCHR ,KRCLLR ,KYAWRT ,KBANK ,
 KGAMMA ,KALT ,CGARML ,CGARMIN ,
 RRTLLIM ,PLIM ,KNY ,KNZ ,
 AILRON ,STBLTR ,RUDDER ,
 BSERO ,NZSEKO ,

***** COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS *****

9-06-84

LISTING FOR SUBROUTINE MISSN2

```

9-07-84
*****
SUBROUTINE MISSSN2
*****
BALLISTIC GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE
WITH NC OFFSET TURN. AFTER POPUP, MISSILE RCLLS TO 90 DEGREES
ANGLE CF BANK AND USES LATERAL AND VERTICAL PROPORTIONAL NAV.
*****
MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
CONTRCL LGOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED
TO +4.0 AND -2.0 G'S.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NOUT,PCOUNT,NFAZE
*****
COMMON /A/ TIME , FINTIM,DT , CPDT , NCUT , NPTS , CPA ,PCOUNT,
* * * * * G , T , RHO , PI ,PII ,MASS ,WT ,S ,
* * * * * IXX , IY , IZZ , IXZ , IA , IB , IC ,CS ,
* * * * * ID , IE , IF , IG , IH , II , IJ , IK ,
* * * * * CHORD2, CHORD , SPAN2, SPAN , NFAZE
*****
COMMON /C/ KPTCHR , KROLLR , KYAWRT , KBANK ,
* * * * * KGAMMA , KALT , CGARML , CGARMN ,
* * * * * RRTLIM , PLIM , KNY , KNZ ,
* * * * * AIRLON , STBLTR , RUCCER ,
* * * * * BSERO , NZSERO , NYSERO
*****
COMMON /C/ ALFA , BETA , VT , HMDOT ,
* * * * * L , V , THETA ,
* * * * * PHI , GAMMA , CL , SY ,
* * * * * CD , CY , CL , CR ,
* * * * * CM , CN , P , Q ,
* * * * * R , ALFADT , BETADT , PDOT ,
* * * * * CDOT , RDGT , NZ , ALTUDE ,
* * * * * XM , YM , XMDCT , YMDCT
*****
COMMON /F/ PH1 OFFSET , PH2 , PH3 , PH4 ,
* * * * * , ALTATT , SGU2PU , MI SDUST
*****

```

```

C      * * * * *
C      LAMDAZ      ,LAMDEL      ,KNFAZ      ,KNFEL
C      NZC         ,PHIC        ,GAMMAC      ,PCCLIM
C      PC          ,QC          ,RC          ,RANGE
C      SIGAZ       ,SIGEL       ,SIGDAF      ,SIGDEF
C      SYT         ,THETAT      ,XT         ,YT
C      HT         ,NYC         ,POPRNG      ,Y
C
C      COMMON /G/  AOA         ,SIDESL      ,FLTPHC
C      BANKC       ,PITCH       ,ROLLRTRC  ,ROLTRIC
C      PTCHRT      ,YAWRT       ,HEADNG     ,FLTPTH
C      HEADT       ,ELEVT       ,DSIGAZ     ,DSIGEL
C      CSGDAZ      ,ERFEL       ,ERFBK     ,ERFRR
C      ERF AZ
C
C      EXECUTABLE *****
C      SET POPLF RANGE AND A PARABOLIC ALTITUDE TRACK
C
C      POPRNG = 15000
C      VH = SCRT(XMDOT**2+YMDOT**2)
C      ALTATT = HMDOT*RANGE/VH + (G/2.)*(RANGE/VT)**2 + 10.
C
C      MISSION PHASE LOGIC AND GUIDANCE COMMANDS
C
C      1 IF (PH4.EQ.1) GO TO 40
C      IF (PH1.EQ.1) GO TO 30
C
C      ** INGRESS FROM INITIAL CONDITION TO PCPUP MANEUVER
C
C      IF (RANGE.LT.POPRNG) GO TO 9
C
C      ALTITUDE HOLD
C
C      ALTC = 50.0
C      ALTUDF = ALTUDE
C      GAMMAC = KALT*(ALTC-ALTUDF)/VT
C      GAMMAF = GAMMA
C      AZC = COS(GAMMAF)*KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C      PFCPCRTIONAL NAVIGATION IN AZIMUTH
C
C      AYC = LAMDAZ*VT*SIGDAF/G
C      PFIC = ATAN2(AYC,AZC)
C      NZC = AZC*CDS(PHI)+AYC*SIN(PHI)
C      GC TO 100
C      PHI = 1
C
C      5

```

```

**      PULLLF TC ATTACK ALTITUDE
C      PROFCRTICNAL NAVIGATION IN AZIMUTH
C
C      ***** PATCH TC RETAIN BTT GUIDANCE TO IMPACT (KTEST=1)
C      KTEST = 1
C      IF(KTEST.EQ.1) GO TO 32
C      ***** ENDPATCH
C      3C      IF(ALTITUDE.GE.ALTTATT) GO TO 39
C
C      32      CONTINUE
C      CCMMAND BALLISTIC ATTACK ALTITUDE
C
C      ALTIC = ALTTATT
C      ALTUDF = ALTITUDE
C      GAMMAC = KALTI*(ALTC-ALTUDF)/VT
C      GAMMAF = GAMMA
C      AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C      PROPORTIONAL NAVIGATION IN AZIMUTH
C
C      AYC = LAMDAZ*VT*SIGDAF/G
C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      PHIC = ATAN2(AYC,AZC)
C      GC TO 100
C      PF4 = 1
C
C      39
C
C      **      ATTACK
C      PROFCRTICNAL NAVIGATION IN AZIMUTH AND ELEVATION
C
C      CCMMAND ATTACK ALTITUDE & ROLL TC 90 DEG BANK.
C
C      4C      PHIC = PI/2.
C      ALTIC = ALTTATT
C      ALTUDF = ALTITUDE
C      GAMMAC = KALTI*(ALTC-ALTUDF)/VT
C      GAMMAF = GAMMA
C      AZC = KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C      PROPORTIONAL NAVIGATION IN AZIMUTH
C
C      AYC = LAMDAZ*VT*SIGDAF/G
C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      NYC = AYC*COS(PHI)-AZC*SIN(PHI)
C      NYC = 0.0
C
C      10C CONTINUE
C      *****
C      *****
C      *****

```

```

C      NZ COMMAND LIMITED TO -2 8 +4 G'S; NYC TO +- 0.5 G.
C
C      NZC= LIMIT(-2.0, 4.0,NZC)
C      NYC= LIMIT(-0.5, 0.5,NYC)
C
C      RETURN
C      ENC

```

LIST OF REFERENCES

1. Watterson, Kent B., Bank-To-Turn Cruise Missile Terminal Guidance and Control Law Comparison, Thesis, Navy Postgraduate School, Monterey, California, 1983.
2. IBM Company, Continuous System Modelling Program III (CSMP III) Program Reference Manual, Program Number 5734-XS9, December 1975.
3. Speclchart, F.H., and Green, W. L., A Guide to Using CSMP-The Continuous System Modeling Program, Prentice-Hall, 1976.
4. Hewett, M.D., Guidance and Control Systems Course (Class Notes), 1983.
5. Roskam, J., Airplane Flight Dynamics and Automatic Flight Controls, Roskam Aviation and Engineering Corp., 1979.

INITIAL DISTRIBUTION LIST

	No.	Copies
1. Defense Technical Information Center Cameron Station Alexandria, Virginia 22314	2	
2. Library, Code 0142 Naval Postgraduate School Monterey, California 93943	2	
3. Dr. Marle D. Hewett F. E. Textron, Inc. 2485 McCabe Way Irvine, California 92714	2	
4. CDR Barton P. Anderson, USN Naval Air Rework Facility Naval Air Station Pensacola, Florida 32508	2	

210330

Thesis

A4446 Anderson

c.1

An investigation into
the control limitations
of a bank to turn mis-
sile in the terminal
homing phase.

210030

Thesis

A4446 Anderson

c.1

An investigation into
the control limitations
of a bank to turn mis-
sile in the terminal
homing phase.

thesA4446

An investigation into the control limita



3 2768 001 91473 2

DUDLEY KNOX LIBRARY